

#### **Research Paper**

# Sensor for monitoring rice grain sieve losses in combine harvesters



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Keywords: Rice Grain sieve loss Impact behaviour Discrete element method Field test Grain sieve losses are important parameters to judge the performance of cleaning shoes in combine harvesters. To keep grain sieve loss within acceptable limits, an impact-type piezoelectric sensor was developed for real-time monitoring. Rice grain and short straw particle models were established according to their physical properties, and discrete element method (DEM) simulations were carried out to understand their collision behaviour with the sensor. The influence of grain shape, straw length and impact angle on variations of the maximum normal contact force and force rise-time were analysed in detail. Differences in normal collision force, and force rise-time occurred which lead to corresponding differences in signal frequency and voltage amplitude. A signal processing circuit, which mainly consisted of a band-pass filter circuit and a voltage comparator circuit, was designed to discriminate for full grains. Field tests results indicated that measurement errors recorded by the sensor and checked against manually measurements were <4.48%.

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#### 1. Introduction

Combine harvesters operate all over the world, harvesting different crops under different environmental conditions. They have functions which cover the entire harvesting process that can be divided into cutting, threshing, separating, cleaning and storing. Cleaning process, refer to the final separation of grain from material other than grain (MOG), which is influenced by a wide range of parameters including crop yield, climate, threshing and cleaning settings (Craessaerts, De Baerdemaeker, Missotten, & Saeys, 2010; Craessaerts, Saeys, Missotten, & Baerdemaeker, 2010). Grain sieve loss, which is influenced by a wide range of parameters such as design, operating conditions as well as crop properties, is an important parameter to judge the performance of the cleaning shoe. In China, evaluation of grain sieve losses mainly relies on manual labour, using a canvas to collect all mixed material at the exhaust port, then filtering out the grains from MOG by a re-cleaner, weighing them and then calculating the absolute sieve loss. This value can be used for benchmarking, but it cannot be used for system control because it cannot be obtained real-time. With the advances in sensors and automation in recent years, researchers have proposed many sensors for use with combine harvesters to extract real-time information from the working process (Craessaerts, Saeys, Missotten & De Baerdemaeker, 2008; Omid, Lashgari, & Mobli, 2010; Reyns, Missotten, Ramon, & Baerdemaeker,

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grain impact force rise-time, us

N	om	len	cla	atu	ire

		t-2	straw impact force rise-time us
a,b	semi-axis lengths of ellipsoid, m	τ.	curie temperature. °C
С	equivalent capacitance, F	Tr <sub>o</sub>	relative permittivity
Ca	capacitance in piezoelectric ceramics, F	II	voltage amplitude V
Cc	cable capacitor, F		unit vector of rotating shaft
Ci	input capacitance, F		voctor of particle velocity $m c^{-1}$
d <sub>31</sub> , d <sub>33</sub>	piezoelectric constant, PC/N	v	$rac{1}{2}$
е	coefficient of restitution	0 <sub>n</sub>	$r_{10}$
$E^*$	effective Young's modulus, MPa	<i>U</i> <sub>n1</sub>	grain normal velocity, in s
E <sub>1</sub>	Young's modulus of grain, MPa	0 <sub>n2</sub>	straw normal velocity, in s
E <sub>2</sub>	Young's modulus of sensor, MPa	$\mathbf{v}_{ au}$	tangential velocity, m s
F <sub>n</sub>	normal contact force, N	$v_{\tau 1}$	grain tangential velocity, m s <sup>-1</sup>
F <sub>n max</sub>	maximum normal impact force, N	$v_{\tau 2}$	straw tangential velocity, m s
F <sub>n1 max</sub>	grain maximum normal impact force, N	Un	normal relative velocity, m s
$F_{n2}$ max	straw maximum normal impact force, N	$v_{\tau}^{rer}$	tangential relative velocity, m s <sup>-1</sup>
$F_{\tau}$	tangential contact force, N	$\delta_{n}$	normal overlaps, m
$F_{\tau 1 \text{ max}}$	grain tangential contact force, N	$\delta_{n1}$	grain normal overlaps, m
$F_{\tau 2} \max$	straw tangential contact force, N	$\delta_{n2}$	straw normal overlaps, m
F <sup>d</sup>	normal damping force, N	$\delta_{ au}$	tangential overlaps, m
F <sup>d</sup>	tangential damping force. N	$\delta_{ au 1}$	grain tangential overlaps, m
τ g	gravitational acceleration. m $s^{-2}$	$\delta_{\tau 2}$	straw tangential overlaps, m
G*	effective shear modulus. MPa	α	normal overlap, m
G1	shear modulus of seed. MPa	$\alpha_{\max}$	maximum normal overlap, m
G <sub>2</sub>	shear modulus of sensor. MPa	$\alpha_y$	yield overlap, m
K22	electromechanical coupling coefficient	γ	aspect ratio
I	moment of inertia. kg m <sup>2</sup>	Vout	collision output voltage, V
m	mass of grain, g	V <sub>out1</sub>	grain collision output voltage, V
m*	equivalent mass. g	V <sub>out2</sub>	straw collision output voltage, V
n	contact normal vector	$\nu_1$	Poisson's ratio of output material
n.	contact pressure MPa	$\nu_2$	Poisson's ratio of plate
Р р.,	vield pressure MPa	$\theta_1$	grain impact angle, (°)
Py O	mechanical quality factor	$\theta_2$	straw impact angle, (°)
Qm r	loss grains ratio	$\eta_1$	grain peak force ratio
R	rotating radius of particle m	$\eta_2$	straw peak force ratio
R. R.	radii of principal curvature m	ω	rotational velocity, rad $s^{-1}$
$\mathbb{R}^*$	mean effective radius m	$ ho_{ m m}$	density, g cm $^{-3}$
R.	input resistance O	DEM	discrete element method
t.	collision time s	MCU	microcontroller unit
t:.	grain collision time s	MOG	material other than grain
41 t.	straw collision time s	PVDF	polyvinylidene fluoride
+	force rise time c		
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2002), either by monitoring machine settings (e.g. driving speed, fan speed, upper and lower sieve opening) (Mcgechan, 1982), machine load (e.g. feed-rate, torque drum, engine load and grain mass flow) (Loghavi, Ehsani, & Reeder, 2008) or by measuring field-related parameters (e.g. moisture content of grain, machine lateral and longitudinal inclination) (Craessaerts, De Baerdemaeker et al., 2010; Craessaerts, Saeys et al., 2010; Lenaerts, Missotten, De Baerdemaeker, & Saeys, 2012; Mouazen, Anthonis, & Saeys, 2004). Some researchers also have engaged in grain sieve loss auto-detection technology (Hiregoudar, Udhaykumar, Ramappa, Shreshta, & Medaet, 2011) and many advanced combine harvesters have grain sieve loss monitoring sensors installed (Eldredge, 1985; Liu and Leonard, 1993; Zhou, Zhang, Liu, & Yuan, 2010; Gao, Zhang, Yu, & Li, 2011; Li, 2006; Ni, Mao, & Tian, 2011; Osselaere, 1985). To date, a measure was found for monitoring grain loss by quantifying grain impacts during a fixed interval based on piezoelectric effect. However, the combine harvesters produced in Europe and North America are mainly used for harvesting crops, such as wheat, bean and oil-seed rape. Rice, one of the most important crops in China, is very different in its physical properties to these crops and there is therefore a need to develop a signal processing circuit to accurately discriminate rice grain loss from MOG.

The surface of grain sieve loss monitoring sensors usually consists of a rigid plate. Different materials collide with the plate causing differences in the frequency and force of the collision. The impact behaviour of grains and MOGs with the plate is therefore a critical step for designing a signal processing circuit for real-time monitoring. In recent years, Download English Version:

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