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Synthesis and optimisation of an integrated water and membrane network framework with multiple electrodialysis regenerators



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ABSTRACT

The shrinking supplies of freshwater globally, coupled with strict environmental regulations, have driven the manufacturing industry towards sustainable water management for the minimisation of freshwater intake and wastewater generation. By using process integration and its enabling tools, this work considers the synthesis of an optimal water network with multiple regeneration capabilities. Development of the proposed framework is achieved by embedding a subnetwork of detailed electrodialysis models within a water network. Based on a superstructure and fixed flowrate, the optimisation problem is formulated as an MINLP model and solved in GAMS/DICOPT. To demonstrate the applicability of the proposed mathematical model a literature case study on a pulp and paper plant is presented and the results indicate a potential of 12% savings in freshwater intake, 16% reduction in wastewater generated and a 14% saving in the total annualised cost for the entire network.

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1. Introduction

Sustainability of human activities, primarily production and consumption, has been of growing concern in the process industry. Among the sustainability mega-forces, water scarcity has risen to the top of the corporate agenda for most entities in the industrial sector. On average, the manufacturing industry consumes about 22% of the total freshwater available globally and about 90% of this is disposed of as wastewater (Sachidnanda and Rahimifard, 2012). In the face of these dire estimates, a number of industries are taking measures to become stewards of this vital resource through sustainable water management. This suggests the need to methodically and efficiently run operations such that profitability is maximised without exceeding the ecological capabilities that support these operations (El-Halwagi, 2012).

Process integration is a powerful and effective framework for sustainable design that emphasises the unity of a process because of the strong interactions that exist between the different unit operations (El-Halwagi, 2012). With regards to the minimisation of freshwater intake and wastewater generation, process integration has presented enabling tools for sustainable water network design such as water recycle, reuse as well as regeneration-recycle and regeneration-reuse. Optimisation of water networks has become a vital instrument of sustainability as it allows for the realisation of

http://dx.doi.org/10.1016/j.compchemeng.2015.11.005 0098-1354/© 2015 Elsevier Ltd. All rights reserved. the full benefits, both economic and environmental, of using the aforementioned enabling tools.

The two optimisation approaches that remain irrefutable are the insight-based 'pinch' approach and mathematical programming. Most of the early work reported on water network optimisation was insight-based, which being graphically-based, focused on flowrate targeting and network design methods. Wang and Smith (1994) proposed the first graphical-based solution with a fixed load framework, to synthesise a single contaminant water network that had regeneration capabilities. Over the years, the technique has been refined and modified to extend its applicability to various systems found in the real world (Tan et al., 2007). Noteworthy is that these graphical methods offer low computation expense but are limited to mass transfer based operations and grassroots design purposes (Bandyopadhyay and Cormos, 2008; Tan et al., 2009).

Mathematical programming techniques involve the development of models based on mathematical relations that describe the system under analysis and the application of rigorous algorithms to obtain solutions. Early work on mathematical optimisation was reported by Takama et al. (1980) who used a superstructre based approach to address a water allocation planning problem for a refinery. Further work on the technique became more prominent much later, as researchers realised its capability of treating rigorous, large-scale, complex systems, which pinch analysis is incapable of handling (Tan et al., 2009). This includes the work by Quesada and Grossmann (1995) and Karuppiah and Grossmann (2006) who tackled an integrated water network problem using global optimisation approaches. Similar works that adopt mass and property

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Nomen	nclature	0.	source flowrate
Sets			
I	$\{i i = water sources\}$	$Q_{j,r}^{n}$	nowrate from source, j to regenerator, r
	$\{i i = water sinks\}$	$Q_{j,i}^s$	flowrate from source, j to sink, i
R	$\{r r = regenerators\}$	$Q_{r,r'}^{x}$	recycle from diluate stream to regenerator feed
, n		$Q_{r,r'}^{y}$	recycle from concentrate stream to regenerator feed
Parame	oters	O^{b}	sink <i>i</i> flowrate requirements
IR.	liquid recovery for regenerator r	FW/	freshwater flowrate
F	Faraday constant	100	wastewater flowrate
1	cell width	C^{f}	regeneration feed concentration for regenerator r
7	valence	C_r	regeneration recurconcentration for regenerator, r
aLCD	ICD constant	C _r ^s	concentration of feed concentrate stream for regen-
hLCD	ICD constant	CCT	erator, r
↓ tr	conversion factor	Cr	concentration of recycling concentrate for regener-
	current utilisation	CIW	ator, r
5	spacer shadow factor	C_r^w	concentration of concentrate waste stream for
α 2	spacer shadow factor	cdil	regenerator, r
0	total mombrane registance		diluate contaminant concentration
ρ	volume factor		concentrate contaminant concentration
p	oguivalent conductance	S _r	maximum allowable regenerator concentration
	colution viscosity	C_j	source concentration of
μ	solution viscosity	C_i^0	maximum allowable sink concentration
η	cofety factor	RR _r	removal ratio for regenerator, r
E Lel	Safety factor	Integer	variables
Lmb	cost of membrane	N _r	number of cell pairs per regenerator, r
CFW	freehwater cost		number of een pane per regenerator,
CWW		Binary	variahle
	wastewater treatment cost		$\int 1 - if regenerator r exists$
n 4	maximum equipment me	$y_r^{ED} =$	$0 \leftarrow \text{otherwise}$
1ª	operating time per year		$\left(\begin{array}{c} 0 \leftarrow \text{otherwise} \\ 1 \text{wise} \\ \end{array} \right)$
p a	parameter for carbon steel piping	d	$1 \leftarrow \text{piping exists between regenerator dilute and}$
q	parameter for carbon steel piping	$y_{r,i}^a =$	$\begin{cases} sink, i \\ c \\$
m	niterest rate per year		$(0 \leftarrow \text{otherwise})$
v DS	pipe linear velocity		$1 \leftarrow$ piping exists between regenerator concentrate
$D_{j,i}^{\varepsilon}$	Mannatian distance between source, j and sink i	$y_{r,i}^c =$	and sink, i
$D_{r,i}^d$	Manhattan distance between regenerator, r and		$(0 \leftarrow \text{otherwise})$
	sink, i		$\int 1 \leftarrow \text{recycle exists from regenerator diluate to}$
$D_{r,r'}^{y}$	Manhattan distance between regenerators r and r'	$y_{r,r'}^{x} =$	{ regenerator, <i>r</i>
D_{i}^{k}	Manhattan distance between source, <i>j</i> and regener-		$(0 \leftarrow \text{otherwise})$
<i>J</i> , <i>I</i>	ator, r		$\int 1 \leftarrow$ recycle exists from regenerator concentrate to
		$y_{r,r'}^{y} =$	{ regenerator, <i>r</i>
Contini	Continuous variables		$(0 \leftarrow \text{otherwise})$
<i>TAC</i> _r	total annualised cost for regenerator, r.		(1 ← piping exists between source, <i>j</i> and
Ar	membrane area required by regenerator <i>r</i> .	$y_{i,r}^k =$	{ regenerator, <i>r</i>
E_r^{spec}	specific desalination energy required by regenerator	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	$0 \leftarrow \text{otherwise}$
	<i>r</i> .		$\int 1 \leftarrow \text{piping exists between source. } i \text{ and sink. } i$
E_r^{pump}	specific pumping energy required by regenerator r.	$y_{j,i}^s =$	$0 \leftarrow \text{otherwise}$
I _r	electric current required by regenerator <i>r</i> .		
Lr	stack length		
vr	linear flow velocity, at stage s		
Ur	voltage applied	integratio	n frameworks by Ponce-Ortega et al. (2010) and Khor
ΔP_r	pressure drop across the regenerator	et al. (201	1) to mention a few, have also been done using powerful
Q_r^f	regenerator feed flowrate	mathemat	tical programing tools.
R _r	recovery rate for regenerator, r	Within	water networks, regeneration allows for the partial
Sr	splitting rate for regenerator, r	treatment	of wastewater before being recycled or reused. To date.
Q_r^{dil}	final diluate stream flowrate of regenerator, r	membran	e-based technology emerges as one of the most sustain-
Q_r^p	diluate stream flowrate for regenerator, r	able conte	enders for regeneration mainly because of its competency
Q_r^w	concentrate stream flowrate for regenerator, r	to treat wastewater in single-step processes at competitive costs	
Qr	concentrate stream recycle flowrate for regenerator,	(Strathma	nn, 2010; Rangaiah and Wei. 2010). An interesting obser-
	r	vation is	that for most of the work done on water-regeneration
Q_r^r	recycle stream flowrate for regenerator, r	network of	optimisation so far, the technologies of choice. number
Qrcon	final concentrate flowrate for regenerator, r	of regener	ration units, arrangement of the regeneration train and
Q_r^d	diluate flowrate to sink, <i>i</i>	regenerat	ion design parameters are not set as decision variables:
0^{c}	concentrate flowrate to sink. i	rather the	y are assumed to be known (Rangaiah and Wei, 2010)
Y,1	· · · · · · · · · · · · · · · · · · ·	1	

Additionally, the complexity of regenerator design has forced a

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