



A practical approach to calculate the detailed spatial distribution of the heat transfer fluid temperature in thermosolar supporting boilers



L. Valiño*, R. Mustata, J. Barroso

LIFTEC/CSIC-Universidad de Zaragoza, María de Luna 10, 50018, Zaragoza, Spain

ARTICLE INFO

Article history:

Received 29 January 2015

Received in revised form

19 May 2015

Accepted 21 May 2015

Available online 14 July 2015

Keywords:

HTF oil

Solar thermal

Natural gas boiler

Zonal method

ABSTRACT

Temperature of the oil used as the Heat Transfer Fluid (HTF) in power supporting natural gas boilers is the most critical factor due to the proximity of its degradation point to the working regime. Detailed predictions through Computational Fluid Dynamics (CFD) calculations are too expensive in both time and resources. This paper deals with an alternate, substantially more economical procedure to obtain the detailed temperature distribution inside the circulating oil in such kind of furnaces. The proposed approach consists in limiting the detailed CFD calculations for the critical part of the coils situated closer to the flame in the lower part of the furnace, where oil temperature is higher, with appropriate boundary conditions obtained from an ad hoc zonal calculation of the furnace.

© 2015 Elsevier B.V. All rights reserved.

1. Introduction

In order to achieve economical profitable performances, modern, state-of-the-art HTF oils (Therminol-1 and Technical, 2008) used in power plants usually reach an operating temperature close to 400 °C point. When the solar radiation is weak, the oil coming out from the solar heating system enters the boiler with some temperature increase, but still needing more heat to reach the correct process temperature. At those times, thermal support boilers provide the extra energy needed to heat the HTF up to the right temperature, see e.g. (Baharoon et al., 2015) and (Muñoz et al., 2009).

These boilers are of the family of water-tube (also known as water-wall) boilers, with thermal oil which circulates in the arranged tubes covering the inside part of the furnace wall instead of water. In contrast to the water-wall boilers, HTF oil does not change phase as it circulates. Having also more heat capacity, it effectively captures the heat from the flame and burnt gases inside the combustion chamber until reaching the above mentioned working temperature close to 400 °C. Also, for a cleaner process, those furnaces are feeded with natural gas, as fuel. Out of the available types of water-tube boiler, the helically-coiled ones are a popular choice due to their particular thermo-hydraulic aspects, and efforts are

made in developing calculation codes that can assist in the design phase, see (Sogni and Chiesa, 2014).

Unfortunately HTF oils are not stable when their temperature exceeds a certain limit, for the particular case studied, 400 °C in the core of the flow and 425 °C in the boundary layer (film temperature). These are values close to the working temperature, which makes the right thermal balance of the system a critical issue. Once the critical temperature is overpassed, the oil degrades and may decompose in other volatile lighter oils and form solid particles, by cracking. This causes a loss of the system performance, as those volatile oils are not suitable for heat transfer, effectively reducing the thermal carrier capacity, and eventually leading to accidents by coil rupture: the deposition of the solid material on the interior part of the oil tubes prevents a proper heat transfer, and finally damages the outer part of the tube exposed to the high radiation zone in the flame chamber.

To achieve a detailed assessment of the thermal behaviour of the HTF oil, in the present paper a combined approach is proposed. It is acknowledged that the area where detailed CFD is needed is restricted to the coils facing the combustion chamber in the lower part of the furnace, where its temperature is higher and the radiation is more intense. As the oil has a high thermal capacity and its flow is turbulent, it is therefore able to smooth local variation of thermal magnitudes, so there is not need of a detailed description of boundary conditions. A coarse although properly provided description would suffice. Taking this fact into account, a general zonal method is used to predict the behaviour of the furnace in a

* Corresponding author.

E-mail address: valino@litec.csic.es (L. Valiño).

Nomenclature

q_v	Volumetric power in furnace	k_{g1}	Global heat transfer coefficient in the first stage
V_F	Furnace volume	L_{s2}	Outside coil length
\dot{Q}_{g1i}	Heat given off by gas in the first stage to inside coil	L_{si}	Inside coil length
$\overline{\Delta T}_{log1i}$	Ave. Log. Temp. in the first stage for inside coil	M	Relative height of maximum temperature zone
α_{g1}	Local heat transfer coefficient in the first stage	m_l	Furnace volume fraction occupied by the luminous flame
α_{g2}	Local heat transfer coefficient in the second stage	N_{si}	Inside coil number
\dot{Q}_i	Release heat in surface i	N_{s2}	Outside coil number
\dot{Q}_T	Total power delivery by the fuel	p	Total pressure in furnace
\dot{Q}_{aAH}	Heat absorbed by air in air heater	p_g	Triatomic gas partial pressure in furnace
\dot{Q}_{loss2}	Conduction loss heat in outside coil	Pr_{g1}	Prandtl number in the first stage
\dot{Q}_{lossAH}	Conduction loss heat in air heater	Pr_{g2}	Prandtl number in the second stage
\dot{Q}_{oilIn_d}	Heat absorbed by oil in inside coil	q_5	Heat loss due to conduction
\dot{Q}_{oilOut_d}	Heat absorbed by oil in outside coil	Q_{air}	Sensible heat of air
\dot{Q}_u	Useful power in the boiler	Q_d	Available heat
\dot{Q}_{g1}	Heat released by gas in the first stage	Q_{fuel}	Sensible heat of fuel
\dot{Q}_{g2}	Heat released by gas in the second stage	Q_{Furn}	Total heat entering the furnace
\dot{Q}_{gF}	Heat given off by gas in furnace	Q_F	Total heat entering the furnace
η	Thermal efficiency	q_2	Heat loss due to exhaust gas
λ_{g1}	Gas conductivity in the first stage	Q_{g1o}	Heat released by gas in the first stage to outside coil
λ_{g2}	Gas conductivity in the second stage	Q_{gAH}	Heat released by gas in air heater
ν_{g1}	Gas viscosity in the first stage	r_G	Triatomic gas fraction at the furnace
ν_{g2}	Gas viscosity in the second stage	S_H	Effective thickness of the furnace volume
$\overline{\Delta T}_{log2}$	Ave. Log. Temp. in the second stage	t_{airOut}	Hot air temperature
$\overline{\Delta T}_{log1o}$	Ave. Log. Temp. in the first stage for outside coil	T_a	Adiabatic flame temperature
$\overline{\Delta T}_{logAH}$	Ave. Log. Temp. in air heater	t_{gEsc}	Exhaust gas temperature
\overline{C}_F	Average specific heat of gases in the furnace	t_a	Adiabatic temperature
\overline{C}_F	Average specific heat of gases in the furnace	t_{airOut}	Hot air temperature
Ψ_F	Wall thermal effectiveness	t_{exit}	Assumed gas temperature at the exit of boiler
LHV	Low heating value	$t_{F,exit}$	Gas temperature at furnace exit
φ_{coil2}	Thermal effectiveness coefficient for second stage	t_{gexit}	Gas temperature at the exit of boiler
φ_{coil1}	Thermal effectiveness coefficient for first stage	t_{oilInt}	Oil temperature at the exit of inside coil (intermediate oil temperature)
a_F	Thermal emission of the furnace	t_{oilInt}^*	Design temperature at the exit of indoor coil (intermediate oil temperature)
a_F	Thermal emission of the furnace	t_{oilOut}	Outlet oil temperature
a_{flam_l}	Thermal emission of the luminous flame	t_{oilOut}^*	Design outlet oil temperature
A_{g1}	Gas flow area in the first stage	$t_{oil, in}$	Inlet oil temperature
A_{g2}	Gas flow area in the second stage	t_{ref}	Reference temperature
ALFA	Air excess coefficient in exhaust gas	t_{gs1}	Gas temperature at the exit of inside coil
ALFA ₂	Air excess coefficient in outside coil	t_{gs2}	Gas temperature at the exit of outside coil
B	Volumetric flow rate	t_{gs2}	Gas temperature at the exit of outside coil
D	Mass flow rate	t_{gsF}	Gas temperature at furnace exit
D_{nom}	Nominal mass flow rate	t_{air}	Cold air temperature
d_{air}	Cold air moisture	t_{fuel}	Fuel gas temperature
d_{fuel}	Fuel gas moisture	V_{g1}	Gas velocity in the first stage
D_{nom}	Oil mass flow rate (nominal)	V_{g2}	Gas velocity in the second stage
d_{se}	Outside coil diameter	\dot{Q}_u	Useful power produced by the boiler
d_{si}	Inside coil diameter	η	Efficiency
F_{AH}	Air heater area	Ψ_F	Wall thermal effectiveness in furnace
F_F	Furnace heat transfer surface a	AirL _{AHn}	Air leakage in the air heater
F_{g1i}	Inside coil heat transfer area	B	Fuel gas volumetric flow rate (STP)
F_{g2}	Outside coil heat transfer area	D_F	Furnace diameter
F_F	Furnace heat transfer surface	D	Oil mass flow rate
F_{g1i}	Inside coil heat transfer area	h_F	Furnace height
F_{g2i}	Outside coil heat transfer area	k_{g2}	Global heat transfer coefficient in the second stage
F_{AH}	Air heater area	m_l	Furnace volume fraction occupied by luminous flame
H_{CA}	Cold air antalphy	M	Relative height of the maximum temperature zone
H_{eg}	Exhaust gas antalphy	q_2	Exhaust gas loss
k_c	Attenuating coefficients of free carbon	q_5	Conduction loss heat
k_g	Attenuating coefficients of a triatomic gas	Q_d	Total heat introduced by fuel to the furnace
k_i	Global heat transfer coefficient for surface i	LHV	Fuel low heating value
k_{Ca}	Global heat transfer coefficient in air heater	AirL _{2n}	Air leakage in the second stage of economizer
		ALFA _F	Air excess coefficient in furnace

Download English Version:

<https://daneshyari.com/en/article/1757565>

Download Persian Version:

<https://daneshyari.com/article/1757565>

[Daneshyari.com](https://daneshyari.com)