



Full Length Article

Apparent gas permeability in an organic-rich shale reservoir

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HIGHLIGHTS

- New gas permeability models for organic and inorganic pores were built.
- Effective stress, phase behavior and multiple transport mechanisms were considered.
- Effects of real gas, stress, and adsorption on gas transport were discussed.

ARTICLE INFO

Article history:

Received 22 January 2016

Received in revised form 16 April 2016

Accepted 4 May 2016

Available online 21 May 2016

Keywords:

Shale gas

Transport mechanism

Gas apparent permeability

Organic pores

Inorganic pores

ABSTRACT

Accurate models of gas transport in shale gas reservoirs must consider complex gas transport mechanisms and phase behavior in nanopores, as well as different pore types. The gas transport mechanisms in shale gas reservoirs include viscous flow, Knudsen diffusion, surface diffusion, adsorption and desorption. In this study, a unified model of nanopore gas transport in shale gas reservoirs is presented. Gas storage patterns are different in organic pores and inorganic pores. Therefore, we develop two fully coupled apparent permeability models to describe gas transport in organic pores and inorganic pores separately. The apparent permeability model of organic pores considers the gas transport mechanisms of viscous flow, Knudsen diffusion, surface diffusion, adsorption and desorption. The apparent permeability model of inorganic pores considers the gas transport mechanisms of viscous flow and Knudsen diffusion. In both models, stress dependence, real gas effects and phase behavior are taken into account. Then, the influences of pore pressure, effective stress, real gas effects, pore radius, phase behaviors and transport properties on apparent gas permeabilities in organic pores and inorganic pores are analyzed based on the proposed models.

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1. Introduction

With the rapid decline in conventional reserves, unconventional resources such as tight gas and shale gas reservoirs have played an increasingly important role in the North American energy industry in recent years and have gradually become a key component of the world energy supply. In shale gas reservoirs, gas is stored in organic pores and inorganic pores with nm-scale pore size and extremely low matrix intrinsic permeability. Zou et al. [1] reported pore sizes in shale gas reservoirs ranging from 1 to 200 nm and shale matrix intrinsic permeabilities ranging from 10^{-9} to $10^{-3} \times 10^{-15} \text{ m}^2$ [2,3]. Organic pores are usually smaller than 10 nm in diameter [3–5]. For macro-scale numerical simulations and productivity forecasts, existing multi-continuum medium

models [6] are divided into inorganic matrix and organic matrix components; however, gas transport differences in the two different matrices are often neglected. The consequences of neglecting this difference indicate that apparent gas permeability in shale nanopores should be studied based on different pore types.

The size of shale nanopores approaches the molecular mean free path. Therefore, the continuity assumption becomes invalid [7,8]. Knudsen number is defined as the ratio of the molecular mean free path to the average pore diameter. At different Knudsen numbers, the corresponding gas flow regime differs, as is shown in Fig. 1. Zheng et al. [9,10] derived a fractal model for gas diffusivity in porous media using fractal theory and an analytical expression for gas permeability in dual-porosity media. A fractal predictive model of the gas slippage factor and gas permeability in porous media with low permeability in the slip flow regime was proposed by Zheng et al. [11] based on the combination of bulk diffusion and Knudsen diffusion. Zheng et al. [12] studied the effective gas

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Nomenclature

| | | | |
|----------------------|---|--------------------------|--|
| a | vdw energy parameter ($\text{Pa dm}^6/\text{mol}^2$) | $r_{\text{eff_stress}}$ | effective hydraulic radius in consideration of stress dependence (m) |
| b | vdw energy parameter (dm^3/mol) | $r_{\text{eff_in}}$ | effective hydraulic radius in inorganic pores (m) |
| C_{max} | maximum adsorbed gas concentration (mol/m^3) | T_c | critical temperature (K) |
| d_m | gas molecular diameter (m) | T_{pr} | pseudo reduced temperature |
| D_{s0} | surface diffusion coefficient when gas coverage is zero (m^2/s) | V_L | Langmuir volume (m^3/kg) |
| D_s | surface diffusion coefficient (m^2/s) | V_m | molar volume of gas (m^3) |
| $H(1 - \kappa)$ | Heaviside function (dimensionless) | Z | gas compressibility factor (dimensionless) |
| ΔH | isosteric adsorption heat at the gas coverage of “0” (J/mol) | α | rarefaction coefficient (dimensionless) |
| k_0 | permeability at zero effective stress (μm^2) | β | slip coefficient (dimensionless) |
| k_B | Boltzmann constant (J/K) | σ_{eff} | effective stress on the matrix (Pa) |
| k_m | matrix permeability in Gangi’s model (μm^2) | σ | Lennard-Jones size parameter (m) |
| k_{ins} | intrinsic permeability (μm^2) | ρ_s | rock density (kg/m^3) |
| Kn | Knudsen number (dimensionless) | Φ | porosity (dimensionless) |
| k_{free} | free gas transport permeability (μm^2) | $\Phi_{\text{O_or}}$ | initial porosity in organic matrix (dimensionless) |
| k_{surface} | surface diffusion permeability (μm^2) | $\Phi_{\text{O_in}}$ | initial porosity in inorganic matrix (dimensionless) |
| $k_{\text{app_or}}$ | organic pores apparent permeability (μm^2) | ε | Lennard-Jones energy parameter (dimensionless) |
| $k_{\text{app_in}}$ | inorganic pores apparent permeability (μm^2) | θ_i | gas coverage of ideal gas (dimensionless) |
| M_g | gas molecular weight (g/mol) | θ | gas coverage of real gas (dimensionless) |
| m | associated with the surface roughness of pores | μ | viscosity (Pa s) |
| P_c | critical pressure (Pa) | λ | mean free path length of molecules (m) |
| p | pore pressure (Pa) | ρ_s | rock density (kg/m^3) |
| p_1 | effective stress when pores are closed completely (Pa) | κ | ratio of the rate constant for blockage to the rate constant for forward migration (dimensionless) |
| p_c | confining pressure (Pa) | κ_b | rate constant for blockage (m/s) in surface diffusion |
| p_L | Langmuir pressure (Pa) | κ_m | rate constant for forward migration in surface diffusion |
| P_{pr} | pseudo reduced pressure | τ | tortuosity (dimensionless) |
| r | pore radius (m) | | |
| r_0 | initial effective hydraulic radius (m) | | |
| r_c | critical radius (m) | | |

diffusion coefficient in dry porous media with a fractal-like tree network. Beskok and Karniadakis [13] and Civan et al. [5,14,15] developed apparent permeability models based on the Knudsen number regime. Apparent permeability models based on superposition of Knudsen diffusion and slip flow were developed by Javadpour et al. [16–20]. Ma et al. built a pore network model for simulating gas flow in micro- and nano-porous materials [21] based on the Javadpour model [17]. Additional studies have analyzed viscous flow generated from collisions between gas molecules and Knudsen diffusion due to collisions between gas molecules and pore walls [22,23] (as shown in Fig. 2). Of these two mechanisms (viscous flow and Knudsen diffusion), the dominant mechanism depends on the pore scale of the porous media. When the pore diameters are very large compared to the mean free path of gas molecules, the probability of collisions between molecules is much higher than that of collisions between molecules and pore walls. Thus, gas transport is mainly governed by viscous flow due

to collisions between molecules and is less influenced by Knudsen diffusion. As the pore diameters decrease, reaching the same order of the mean free path of gas molecules, the collisions between molecules and pore walls become more important, with gas transport mainly governed by Knudsen diffusion.

Javadpour et al. [16] described gas flow in nanopores using a diffusive transport regime with a Knudsen diffusion coefficient and negligible viscous effects. He later [17] presented a formulation for gas flow in mudrock nanopores based on linear superposition of Knudsen diffusion and viscous flow using the Maxwell theory. Based on the Javadpour model [17], Azom and Javadpour [24] proposed a gas transmission model for real gas in nanopores. Additionally, the effect of wall roughness on Knudsen diffusion in nanopores was considered by Darabi et al. [18]. However, the Javadpour [17] model includes one empirical coefficient known as the tangential momentum accommodation coefficient (TMAC). An accurate value of TMAC is hard to define for different shale

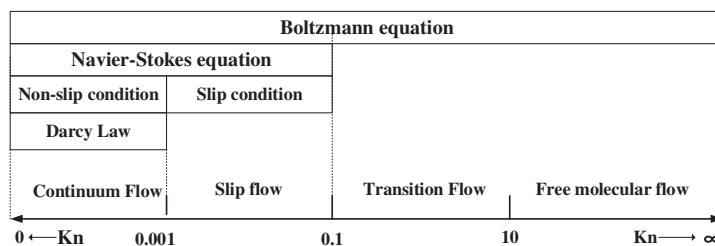


Fig. 1. Transition of flow regimes based on the Knudsen number.

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