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# Ultimate strength of composite ships' hull girders in the presence of composite superstructures



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#### ARTICLE INFO

#### ABSTRACT

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#### 1. Introduction

Laminated composites can be used in different structures in the fields of aerospace, marine and civil engineering. These sorts of composites are generally assemblies of some layers of fibrous composite materials, which can be joined together with the aid of adhesives or resins, in order to provide required engineering properties, including in-plane stiffness, bending stiffness, strength, and coefficient of thermal expansion. It should be emphasised that different structural arrangements of laminated composites including single-skin, stiffened skin and sandwich panels are used in the engineering structures. Application of such materials in ship structures dates back to the late 1970s. Initially, small boats and ships' topsides were being built of such composite materials. Over the time, usage of the composite materials in ship construction continued to grow and in recent years, some longer vessels like frigates and passenger ships are made of laminated composite materials.

Having larger composite ships in length necessitates assessment of their ultimate bending strength in the early stages of structural design. In most of the steel ships, there is no superstructure in the amidships region and thus, the effect of superstructure on the ultimate strength of the ship is negligible. However, composite superstructures are often fitted in the amidships of the composite ships. This leads to the significant contribution of

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and also the results of finite element analysis. Also, a set of composite ships having different lengths of superstructure is generated and analysed. Efficiency of the composite superstructure in contribution to the ultimate bending strength of the composite ships is finally evaluated. © 2016 Elsevier Ltd. All rights reserved.

An extended formulation of the Coupled Beam Theory (CBT) developed by the authors is employed in

order to calculate the ultimate strength of composite ships taking into account of the effect of the su-

perstructure. A nonlinear finite element method is applied for solving the equilibrium equations. Be-

haviour of the stiffened composite panels in tension and compression is modelled by using progressive

failure method. Both hull and superstructure of the ship are modelled using beam elements. Connection

between beam elements representing hull and superstructure is made using specially developed spring

box elements. Accuracy of the extended method is demonstrated using an available experimental result

the composite superstructure in the bending strength of the composite ship.

The ultimate strength of steel ships has been widely investigated by many researchers around the world. Caldwell [1] was the first who estimated the ultimate strength of steel ships employing the fully plastic bending theory of the beams. However, he did not consider the reduction in the load-carrying capacity of structural members after they attain their corresponding ultimate strengths. Smith [2] proposed an approach for calculation of the ultimate strength of the ships. He first divided the ship's cross section into different unstiffened/stiffened plate panels, and then performed a progressive collapse analysis under bending on it assuming that the cross section remains plane after bending and each of the panels behaves according to its corresponding average stress-average strain relationship. Finite element method was applied by Smith [2] in order to obtain the average stress-average strain relationships for unstiffened/stiffened panels. Other researchers made some attempts for derivation of the average stress-average strain relationships for ships' unstiffened /stiffened plate panels subject to in-plane compression alone or in combination with other loads using analytical approaches. Among them, reference may be made to the work of Khedmati [3].

In all of above-mentioned research studies, the ultimate strength of the ships is calculated by ignoring the effect of the superstructure. On the other hand, the available theoretical methods to estimate the ultimate strength of the ship's hull with a superstructure are mostly based on the simple beam theory or two-beam theory. Mackney and Rose [4] have studied the effect of the superstructure on the longitudinal strength of a ship both







Nomenclature		$M_0$	Ultimate bending strength of the ship without any superstructure
A;	Cross-sectional area of the <i>i</i> -th beam	Ni	Axial force of the <i>i</i> -th beam
Å	Constant Matrix	$N_i[x]$	Shape functions
В	Diagonal matrix containing the singular values	$p_{ii}$	Transverse (vertical) distributed forces between the <i>i</i> -
B	Constant Matrix	- IJ	th and <i>j</i> -th beams
– C::	Bending moment lever on the <i>i</i> -th beam due to the	$Q_i$	Shear force of the <i>i</i> -th beam
-1)	shearing $^{i}$ shearing $^{i}$ between the <i>i</i> -th and <i>i</i> -th beams	$q_i$	External force of the <i>i</i> -th beam
	$=\{0, i=i\}$	$\hat{R}_1$	Residual
d <sub>a</sub>	Distance between the upper fibre of the beam to the	$R_2$	Residual
IK	reference line	S <sub>ii</sub>	Longitudinal distributed shear forces between the <i>i</i> -th
D	Constant Matrix	5	and <i>j</i> -th beams
е	Distance between the lower fibre of the beam to the	R <sub>12</sub>	Shear strength in plane 12
' IJ	reference line	$T_{ii}$	Shear stiffness between the <i>i</i> -th and <i>j</i> -th beams
$E_{i}^{t}$	Tangential modulus of the <i>i</i> -th panel or slope of the	Ů	Square and orthogonal matrix
l	mean stress-mean strain curve of the <i>i</i> -th panel	u <sub>i</sub>	Axial displacement of the <i>i</i> -th beam
EA;	Axial stiffness of the <i>i</i> -th beam	$u_i^*$	Approximate axial displacement of the <i>i</i> -th beam
$EA_{i}^{t}$	Tangent axial stiffness = $\sum E_i^t A_i$	$u_i^i$	Normal degree of freedom of <i>j</i> -th node from <i>i</i> -th beam
EA <sup>;</sup>	EA value for <i>i</i> -th node of <i>i</i> -th beam	Ň	Square and orthogonal matrix
EI;	Bending stiffness of <i>i</i> -th beam	$v_i^M$	Transverse displacement of the <i>i</i> -th beam due to the
$EI_{i}^{t}$	Tangent bending stiffness = $\sum E_i^t A_i z_i^2$		bending
EI, <sup>j</sup>	EA value for <i>j</i> -th node of <i>i</i> -th beam	$v_i$	Total transverse displacement for the <i>i</i> -th beam
ΕΧ <sub>i</sub>	Value which modifies the internal forces if the re-	$v_i^{M*}$	Approximate transverse displacement of the <i>i</i> -th
	ference line differs from the centroid of the cross-		beam due to the bending
	section	$v_j^i$	Vertical degree of freedom of j-th node from i-th beam
$EX_i^t$	Tangent modifier of the forces = $\sum E_i^t A_i z_i$	$X_i$	First sectional moment of area of the <i>i</i> -th beam
EX <sup>j</sup>	EX value for <i>j</i> -th node of <i>i</i> -th beam	$X_T$	Tension strength in direction 1
$H_i$	Effective Height of the <i>i</i> -th beam	$X_C$	Compression strength in direction 1
I <sub>i</sub>	Sectional moment of inertia of the <i>i</i> -th beam	$Y_T$	Tension strength in direction 2
$k_{mi}^i$	Stiffness matrix elements of <i>i</i> -th beam	$Y_C$	Compression strength in direction 2
k <sub>EAi</sub>	Constant	$X_{S}$	Nodal displacement vector of system
k <sub>EIi</sub>	Constant	z <sub>i</sub>	Distance of the <i>i</i> -th panel to the reference line
k <sub>EXi</sub>	Constant	$\delta_{ij}^{u}$	Relative axial displacement
Κ	Global stiffness matrix of system	$\delta_{ij}^{\nu}$	Relative transverse displacement
$k_{ij}(x)$	Vertical stiffness between the <i>i</i> -th and <i>j</i> -th beams	$\gamma_s$	Coefficient of efficiency of the superstructure or su-
L	Length of hull		perstructure effectiveness coefficient
Ls	Length of superstructure	$\sigma_1$	Normal stress in direction 1
$M_i$	Bending moment of the <i>i</i> -th beam	$\sigma_2$	Normal stress in direction 2
$M_{x}$	Ultimate bending strength of the ship under	$\tau_{12}$	Shear stress in plane 12
	consideration	$\theta_j^\iota$	Tangential degree of freedom of j-th node from i-th
<i>M</i> <sub>100</sub>	Ultimate bending strength of the ship with a super- structure of 100 percent efficiency		beam

experimentally and numerically. The simple beam theory and finite element method were applied in their study, while they ignored the effect of the connection between the hull and superstructure. Naar et al. [5] proposed a new approach called Coupled Beams Method (CBM) to evaluate hull girder response of passenger ships. This method is based on the assumption that the global bending response of a modern passenger ship can be estimated with the help of beams coupled to each other by distributed longitudinal and vertical springs. To solve the governed equations, Naar et al. [5] proposed an analytical method that was only applicable when the superstructure is as long as the ship's hull.

Very few publications can be found in the literature addressing the issue of ultimate strength of composite ships. Chen et al. [6] were the first who tried to estimate the ultimate strength of composite ships. They proposed a simple analytical method for calculating the ultimate strength of composite vessels. In their method, the behaviour of composite panels was formulated with a simple formula. Chen and Soares [7] extended the above-mentioned method for calculating the ultimate strength of composite ships under bending moment. Two types of the failure modes were considered in their study; the panel buckling as well as fracture of the composite materials. Later, Chen and Soares [8] estimated the reliability of composite ships under bending moment, using the first method proposed by Chen et al. [6]. To calculate the reliability of the reinforced plate buckling failure, the failure of the first layer of the reinforcing plate and the ultimate failure of the reinforced plate were considered. Finally, Chen and Soares [9] used Smith's method, which is a conventional approach and capable of calculating bending moment-curvature curves, in order to calculate the ultimate strength of composite vessels.

Application of the composite materials to the construction of long ships is still a relatively new and growing subject, which needs more research to be performed on assessment of the ultimate strength of these types of the ships. Besides, most of the previous studies do not take into account of the effect of the superstructure on the ultimate strength of the ships.

As it is understood from the above-mentioned review, ultimate strength of the ships taking the superstructure's effect into account have been studied in many aspects, the most of which are only devoted to the linear elastic material behaviours. Download English Version:

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