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The design of electrode for partial discharge location simulation in oil insulated power transformer and the application of AE method

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Abstract

This paper presents the design of electrode for PD-location simulation in oil insulated power transformer and the application of Acoustic Emission (AE) method. The purpose of this design is to make a simple PD signal simulation and to save the time of experiment. The design must take into account the electric field stress at the electrodes (anode) that will cause PD. The electrodes were designed as 2 types. The first is a conventional electrode expected to make a high nonuniform field. The second electrode was designed as insulation layer and transformer coil to generate higher nonuniform field and expected to cause PD easily. Electrodes were simulated to determine the maximum of electric field by installing in the transformer model. Then, the electrodes are installed in the transformer model to make the real test by supplying high voltage to the electrodes to generate PD signal. From the measurement results of PD-location in the power transformer model according to AE and TDOA method found that, the first electrode has uncertain PD-location measurement results. Moreover, it take so long time of any experiment to obtain PD-signal and sometimes become critical breakdown as a result to damage measurement device. While the PD-location detection results from the second electrode found that it can be easily simulated PD signal. The PD-location result has a better precision or has statistical data to detect PD-location explicitly. Therefore, this special designed electrode could be applied for PD detection study in power transformer or other electrical equipment as well.

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1. Introduction

Several years ago, so many researches had tried to present many methods about the partial discharge detection and location in power transformer. The benefit of PD localization in power transformer is the possibility to estimate the severity of the occurred problem inside power transformer. The known information of PD detection and its location can be further used for determining the proper action whether to do maintenance or immediate repair. Some research report has presented the simulation method, location detection and experiment study¹⁻³. Some research report has presented the design of electrode in their experiment^{4,5}or some report has tried to simulate the real transformer model^{6,5}. For my last 3 years' experience about the study on location of acoustic emission partial discharge detection in transformers, I have found that, one of the difficulty about the experiment is the electrode design. If one want to study about the PD-location, one need to energize the PD signal at the desire position and desire time. This paper will present the alternative how to design the electrode for PD-location simulation in oil insulated power transformer. The calculation and simulation of electric field in transformer model have been managed first and then the PD-location experiment with the application of AE method has been used to prove the accuracy.

2. Transformer model and Electrode Design

As in Fig. 1, the transformer model for PD-location simulation has been designed. The 3 adjustable electrodes have been put into the tank together with transformer oil fill. The top electrode (Anode) has designed into 2 models as in Fig. 2 (a) and (b). The top electrode No.1 is as copper with sharp ended rod shape. It is conventional rod electrode and expect that it would give highly non-uniform field. The top electrode No.2 is also the same as the top electrode No.1 addition with ring laminated at the ended rod. The reason to design the top electrode No.2 is expect that, it would give very high non-uniform field at this point and easy to simulate the PD-signal. The bottom plate electrode is as cathode with rogowski profile.

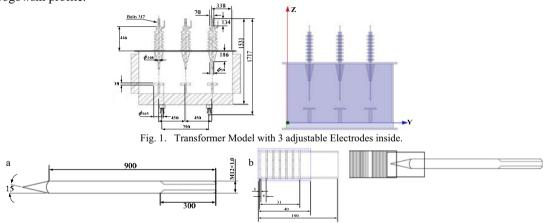


Fig. 2. (a) Top electrode No.1 (b) Top electrode No.2

2.1. Field Utilization Factor

For top electrode No.1, it could be calculated the field utilization factor (η^*) according to equation $(1) - (3)^8$. If the radius (r) is constant designed, the field utilization factor of any distance (S) could be calculated and the maximum electric field at the ended rod could be known for specific breakdown voltage (U_b).

$$\eta^* = \frac{1}{f} = \frac{E_{mean}}{E_{max}} \tag{1}$$

$$E_{mean} = U_b / S \tag{2}$$

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