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# A novel concept for non-linear multidisciplinary aerodynamic design optimization

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#### ARTICLE INFO

ABSTRACT

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Entropy generation Aerodynamic shape optimization Wing box Evolutionary algorithm Entropy based design A fundamental approach is presented here in order to define a comprehensive property that overwhelms the limitations of existing aerodynamic design/optimization practice. A novel parameter is derived extending the loss model accounted by the second law of thermodynamics. The given approach attempts to quantitatively relate the finite-time thermodynamic irreversibilities associated with a particular shape class of a body across a flow field. It is then studied analytically by applications in external and internal aerodynamics. Further, the physical behavior of the function is explored using a case study for aero-structural optimization along with other physical quantities with established behavior (Multi-Disciplinary-Optimization). A baseline model of aerodynamically twisted wing profile entailing NACA 1412 and NACA 621112 airfoils is optimized using Elite member selection based Multi-Objective Genetic Algorithm (MOGA). The proposed function is proven to be more computationally economical and comprehensive for optimization.

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#### 1. Introduction

The multi-disciplinary nature and complexity of aerospace systems make them uniquely challenging. Their numerical modeling/analysis and optimization are computationally expensive and exclusively selective to the area of investigation. Real-world aerospace systems encounter majorly two problems: Multiverse objectives and highly complex and diverse design space. Over past few decades various direct and inverse optimization techniques have particularly found utility in development of optimized aerodynamic shapes like wing/blade geometry. The flagship practices for optimization of aerospace systems are based on multiple-shape/topology optimization, exclusively modified/hybrid algorithms or a combination of both. Apart from numerical parameterization, selection of objective or cost function is a defining step for the accuracy and efficacy of the analysis. However, the major concerns over the selection of the objective function are: specificity in representation of domain, computational cost against the comprehensively and primordially its dependence on the knowledge and experience of the researcher.

The choice of parameterization is dependent upon the nature/complexity and scope of the design/analysis. The simplest parameterization schemes include utilizing point cloud method, which is confined to lower order complexity resulted by increase

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in number of parameters in design space proportional to the complexity of formulation. A report published by Melin [1] projects a detailed discussion on comparison of parameterized airfoil based point cloud airfoils. A 'super element' based wing aero-structural optimization was conducted by Kuntjoro et al. [2]. Their analysis included a leading edge circular approximation and generation of separate pressure & suction surfaces using a polynomial representation in terms of meridian and tangential coordinates. To effectively reduce the computational time, Davari et al. [3] proposed to build a simple model from free form polynomials by controlling the camber and thickness of wind turbine blade sections only. One of the most popular parameterization scheme used in analysis was proposed by Sobieczky [4,5], known as PARSEC method which utilized 11 geometric characteristics of airfoil as control parameters. The upper and lower surface of the airfoil can be separately generated by using this method. Since, PARSEC method was particularly developed for airfoil shape generation, it limits the possibility of different airfoil shapes at the leading edge and does not guarantee a physically acceptable trailing edge, as discussed by Castonguay and Nadarajah [6].

The use of Bezier curves for parameterization has also been widely studied [8–10]. A notable multi-disciplinary and multiobjective study was conducted by Toivanen et al. [11] for aeroelectromagnetic optimization which used Bezier curves to represent upper and lower surface with 9 control points each. Subsequently, Dersken and Rogalsky [12], proposed a PARSEC-Bezier interaction based parameterization scheme. It was particularly de-

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signed to reduce the non-linear interactions of parameters and 2 create a direct link to objective function and reduce the computa-3 tional time. Gardner and Selig [7], found the optimal airfoil shapes 4 through manipulation of velocity distribution using normal/hybrid 5 genetic algorithm. Based on preset criteria, the airfoil geometry 6 was generated using an inverse method from velocity distribution 7 parameters for candidate airfoils. They showed that using design 8 variables defining velocity distribution in inverse method can pro-9 foundly enhance the performance of the airfoil shape optimization 10 genetic algorithm. A detailed analysis of present evolutionary algo-11 rithms was conducted by Zitzler [13]. The main focus of the study 12 was to study the sensitivity of the Pareto-front on the shape of the 13 objective function & use of weight function in the domain. He also 14 indicated that the use of 'weighing function' cannot generate all 15 Pareto solution to the non-convex surfaces.

16 A multi-point shape optimization technique was utilized by 17 Montanelli [14], for design of turbomachinery blades. He used a 18 discrete adjoint method using Non Uniform Relational B-Splines 19 (NURBS) parameterization to generate the coordinate control 20 space. His study includes the use of 'weights' as per their im-21 portance to the analysis and then combine them to define a sin-22 gle objective function for analysis. Straathof [15] also discussed 23 some recent parameterization techniques in his proposal of a novel 24 method using B-splines. It is to notice that though NURBS provide 25 a compact and intuitive geometric representation, it's the com-26 plexity in their definition and resolution to which a geometry can 27 be replicated in different computational environment. A more ef-28 ficient and utilitarian concept was proposed by Kulfan [16] for 29 Computational Fluid Dynamics (CFD) analysis. She compiled a list 30 of desirable features for geometric representations and introduced 31 Class-Shape-Transformation (CST technique). The technique uses a 32 combination of specific shape and class functions resulting in dif-33 ferent surface design space. The method will be further discussed 34 in current analysis in subsequent sections. A detailed survey of 35 shape parameterization techniques was published by Samareh [17] 36 from NASA which acts a very helpful source for elements of topol-37 ogy optimization.

38 Since last two decades, the concept of exergy based design opti-39 mization analysis has been widely used for multi-level and multi-40 disciplinary aerospace system and component designs. The main 41 advantage for the popularity of exergy based analysis is their abil-42 ity of application in geometrically complex systems. One of the 43 early work for using exergy method in aerospace systems is de-44 rived from Paulus and Gaggioli [18]. They used 'exergy of lift' for 45 calculations, based on the idea of the energy delivered to and by 46 the wing. The objective of the study was to successfully use exergy 47 and plot the 'Exergy flow diagram' of the aircraft for all modes 48 of flight (i.e., take-off, cruise, landing) based on various aircraft 49 components. Alabi and Ladeinde [19,20], utilized the CFD based 50 exergy calculations for the design of a complete aircraft systems 51 (Boeing B747-200 aircraft). They carried out physical decomposi-52 tion of the overall system was done for multi-level identification 53 of airframe subsystems. Similarly, Li et al. [21] used exergy method 54 for aerodynamic designs using a 2D and 3D wing geometry under 55 turbulent flow conditions. They used 3rd order NURBS parameter-56 ization scheme for increasing Cl/Cd ratio and reduce volumetric 57 entropy production rate using Genetic algorithm.

58 It can be evidently understood that a particular shape of a de-59 vise (wing/blade) affects its aerodynamic characteristics and other 60 features like its weight, modal response etc. Thus, the irreversibil-61 ities like viscous and thermal dissipation produced in the domain 62 of interest by the specific body (shape) is a very effective signature 63 of the devise for analysis. Exergetic losses associated with a flow 64 field is directly proportionate to the losses and the useful work 65 lost by the fluid. Thermal dissipative forces play a significant part 66 in aero-turbomechanic analysis, where a combination of thermal

and viscous dissipative forces is considered to include the stagnation losses and losses incurred to the pressure gradients in flow field.

Bejan calculated the effects of wing shape on viscous dissipation (first term) and thermal dissipation (second term) produced in a system (eqn. (1)). For external flows over a typical wing, placed in a laminar flow field velocity of U, temperature T, W is the wing span length, body temperature  $T_w$ , q'' as heat transfer rate from body and surface area A, the local entropy production rate (irreversibilities) can be estimated as [22]

$$S_g \frac{kT^2}{q'^2 W} = 1.456 \Pr^{-\frac{1}{3}} R e_L^{-\frac{1}{2}} + 0.664 \frac{U^2 \mu kT}{q'^2} R e_L^{\frac{1}{2}}$$
(1)

Though, the local entropy production is considerably effective tool in representing the physical system and account for losses, but it lacks on account of representing the multi-disciplinary nature of the system. As in, for aero-structural or aero-electromagnetic optimization, it will treat the wing shape as a black body, hence the other relevant factors like internal structure etc. cannot be accounted for. Therefore, in order to include all the physical aspects new optimization function needs to be defined, to make the analysis comprehensive & computationally economical. Also, as per designer prospective the shape should be conveniently parameterized and controlled in optimization process. Hence the new function should also extend this ability to approximate various classes of geometrical shapes.

#### **2.** Derivation and study of parameter $(\pi_s)$

Let us assume a generic aerodynamic body moving across a flow regime. The entropic losses (irreversibilities) incurred in the flow are influenced by the thermo-physical state of the medium and the specific shape of the body. As we know that every system is associated with some specific form of energy, we can use the intrinsic energy form (Q') for an analysis. The choice of the energy form is of prime importance here, which is further illustrated. Also, the rate of work losses associated in such an aerodynamic system can be calculated using Guoy–Stodola theorem [23]

$$\dot{W}_{lost} = T\dot{S}_g = T\left(\dot{S}_g = \frac{k}{T^2}\left(\nabla^2 T\right) + \frac{\mu}{T}(\emptyset)\right)$$
(2)

such that  $\frac{k}{T^2}(\nabla^2 T)$ , represents the conductive effects for thermal interaction across the flow field and  $\frac{\mu}{T}(\emptyset)$  is equivalent to the viscous forces acting on the body placed in a temperature field (*T*). It can be noted here that  $S_g$  is always positive whenever there are velocity and thermal gradients present in any fluid flow domain. Thus, for any aerodynamic system we can identify

$$\dot{W}_{lost} \propto Q', A, \mu$$
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and Q' is the intrinsic form of associated energy, A is area associated with the loss generation and  $\mu$  is the thermo-physical property of the medium. Using Buckingham- $\pi$  theorem [24,25], let us consider

$$\dot{W} = \emptyset(Q', A, \mu) = \emptyset(Q')^{a}(A)^{b}(\mu)^{c}$$

$$\begin{bmatrix} ML^{-1}T^{-2} \end{bmatrix} = \emptyset[L^{2}T^{-2}]^{a}[ML^{-1}T^{-1}]^{b}[L^{2}]^{c}$$
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Comparing, we get a = 1, b = 1, c = -1. Thus we can define

$$T\dot{S} = \emptyset \frac{Q'\mu}{A}$$
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For simplicity, let  $\emptyset = 1/\pi_s$ , rearranging we get

$$\pi_s = \left(\frac{Q'}{\dot{W}}\right) \left(\frac{\mu}{A}\right) \tag{3}$$

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