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Time-dependent bladder tissue regeneration using bilayer bladder acellular matrix graft-silk fibroin scaffolds in a rat bladder augmentation

model

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ABSTRACT

With advances in tissue engineering, various synthetic and natural biomaterials have been widely used in tissue regeneration of the urinary bladder in rat models. However, reconstructive procedures remain insufficient due to the lack of appropriate scaffolding, which should provide a waterproof barrier function and support the needs of various cell types. To address these problems, we have developed a bilayer scaffold comprising a porous network (silk fibroin [SF]) and an underlying natural acellular matrix (bladder acellular matrix graft [BAMG]) and evaluated its feasibility and potential for bladder regeneration in a rat bladder augmentation model. Histological (hematoxylin and eosin and Masson's trichrome staining) and immunohistochemical analyses demonstrated that the bilayer BAMG-SF scaffold promoted smooth muscle, blood vessel, and nerve regeneration in a time-dependent manner. At 12 weeks after implantation, bladders reconstructed with the BAMG-SF matrix displayed superior structural and functional properties without significant local tissue responses or systemic toxicity. These results demonstrated that the bilayer BAMG-SF scaffold may be a promising scaffold with good biocompatibility for bladder regeneration in the rat bladder augmentation model.

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47 **1. Introduction**

48 Various congenital and acquired urinary tract diseases, such as bladder exstrophy, bladder cancer, and neurogenic bladder dys-49 function, require bladder reconstruction [1]. Currently, bladder 50 reconstruction is still one of the greatest surgical challenges in 51 the field of urology. While enterocystoplasty is still considered 52 53 the gold standard and has played a major role in bladder reconstruction for decades [2], it is associated with a series of complica-54 tions, such as recurrent urinary tract infections, electrolyte 55 imbalance, urinary incontinence, perforation and urolithiasis, 56 severely impacting the quality of life of patients [3]. 57

Tissue engineering (TE) approaches provide a potential strategy to minimize these consequences and have great promise for bladder repair and reconstruction [4,5]. In recent studies, different types of scaffolds, constructed mainly from naturally derived materials and synthetic polymers, are used widely for bladder reconstruction [6,7]. Bladder acellular matrix grafts (BAMGs) are intact collagen-based xenogenetic biomaterials derived from pigs that are prepared using rigorous techniques to remove all cells [8]. Moreover, BAMGs exhibit good biocompatibility and support tissue regeneration [9], and several studies have indicated that BAMG is a suitable scaffold for bladder reconstruction [6,10,11]. In addition, BAMGs have also been shown to prevent permeation of luminal contents into the abdominal cavity [12]. Although multilayered urothelial tissues have been shown to be generated by implantation of a simple BAMG scaffold in the bladder, these dense and smooth BAMGs cannot promote satisfactory smooth muscle regeneration, vessel formation, and nerve tissue regeneration, particularly for seeding cells or host tissue penetration into the scaffold [10,13]. Silk fibroin (SF) is a unique natural fibrous protein

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that has a unique array of properties, including high structural
strength and elasticity, diverse processing plasticity, and tunable
biodegradability [14]. Unfortunately, the simple and compact SF
structure is not easily degraded and increases the risk of urinary
stones [15,16].

82 The ideal scaffold for the regeneration of the urinary bladder 83 must fulfill specific requirements pertaining to three-dimensional 84 (3-D) architecture, microenvironmental needs of the various types of cells in the bladder wall, barrier function, and structural integ-85 86 rity of the bladder [17]. To reach this goal, we have developed a 87 bilayer scaffold by adding SF directly on the BAMG and lyophilizing 88 the sample, resulting in the SF-dependent generation of an internal interconnected porous architecture; this structure was then shown 89 90 to increase the extent of degradation and infiltration of host blad-91 der tissue [16]. We believe that this bilayer BAMG-SF scaffold may 92 represent a novel promising biomaterial for bladder 93 reconstruction.

94 Therefore, in the present study, we examined the feasibility of 95 the bilayer BAMG-SF scaffold for bladder reconstruction in rats. The morphological features of the bilayer scaffold were character-96 97 ized by scanning electron microscopy (SEM), and biological perfor-98 mance of the bilayer scaffold was analyzed at 2, 4, and 12 weeks 99 after implantation into the rat bladder. Furthermore, we also eval-100 uated the extent of SF scaffold degradation in vivo, inflammatory 101 responses, and systemic safety.

102 2. Materials and methods

103 2.1. Fabrication of bladder acellular matrix grafts (BAMG)

104 All animal procedures were approved by the Institutional 105 Animal Care and Use Committee of the Affiliated 9th People's 106 Hospital of Shanghai Jiao Tong University School of Medicine. 107 Porcine bladder tissues were harvested from 3-month-old pigs 108 and rinsed with phosphate-buffered saline (PBS; pH 7.2-7.4) to 109 remove blood. The bladder samples were then transported in ice-cold PBS to the laboratory immediately. Fat tissues and fascia 110 around the urinary bladder were removed with scissors. The 111 112 urothelium, muscle, and serosal layers were grossly removed by 113 surgical delamination and washed in distilled water in a stirring flask (200 rpm) for 48 h at 4 °C, followed by treatment with 114 0.03% trypsin for 1 h. The bladders were then soaked for 7 days 115 116 at 37 °C in 0.2% Triton X-100 (Sigma, St. Louis, MO, USA) and 117 0.1% (v/v) ammonium hydroxide. The solution was refreshed every 118 day. The resulting matrix was washed with distilled water for 119 2 days at 4 °C and sterilized with 75% ethanol. The complete elim-120 ination of cellular nuclei in the BAMG was confirmed by histolog-121 ical evaluation and quantification of residual DNA content.

122 2.2. Evaluation of the decellularization efficacy

123 The BAMG were fixed in 10% buffered formalin, dehydrated, and embedded in paraffin. For histological examinations, sections 124 125 (5 mm) of the BAMG were deparaffinized and stained with H&E and Masson's trichrome stainings to evaluate the cellular nucleus 126 127 and ECM components. The total DNA in freeze-dried native porcine 128 bladders and BAMG was extracted using a DNA isolation kit for tis-129 sues (Roche Applied Sciences). The samples were weighed, finely 130 minced using scissors, and digested with RNase and proteinase K. 131 The remaining DNA was collected and quantified using the Quant-iT[™] PicoGreen[®] dsDNA Assay Kit according to the manufac-132 133 turer's protocol. The fluorescence of test solution was measured on 134 a fluorescence microplate reader (excitation, 480 nm; emission, 135 520 nm; Thermo Scientific Multiskan FC). The amount of DNA in 136 the native porcine bladders and BAMG was quantified against a

DNA standard curve and expressed as μ g/mg dry weight of the test samples. We randomly and respectively selected 6 native porcine bladders and BAMGs to carry out the DNA content assay. All the evaluations were repeated 3 times. 140

2.3. Fabrication of the bilayer BAMG-SF scaffold

The bilayer BAMG-SF scaffold was composed of 3-D porous SF 142 and BAMG. First, the BAMG was washed with deionized water 10 143 times to remove the alcohol component, which could negatively 144 affect the adhesion of SF on the BAMG. Then, the BAMG was 145 trimmed into $15 \text{ mm} \times 15 \text{ mm}$ square pieces and placed in a pre-146 pared rectangular casting vessel (bottom: $15 \text{ mm} \times 15 \text{ mm}$), where 147 the muscle layer surface of the BAMG is directly exposed to the SF 148 solution. Preparation of silk fibroin solution and fabrication of 149 highly interconnected porous silk fibroin scaffolds following the 150 procedure described previously [18,19]. Next, 300 µL of SF solution 151 (2% w/v) was slowly poured into the vessel. The whole material 152 was transferred to the refrigerator and frozen at -20 °C for 2 days. 153 The frozen composite was then lyophilized to remove the water 154 and the other solvents to form a porous SF scaffold. Finally, the 155 scaffolds were dried at room temperature under vacuum for 156 2 days, which were then sterilized in 75% ethanol, rinsed in PBS, 157 and subjected to surgical procedures described below. 158

2.4. SEM

Structural analysis of the matrix prior to implantation was per-160 formed by SEM in order to gain insights into the scaffold surface 161 morphology, interfiber space, and thickness. The samples were fro-162 zen with liquid nitrogen, cut into small pieces, and vacuum dried 163 overnight. The samples were then sputter-coated (Balzers Union 164 07120/135, Germany) with 10 nm of platinum/gold, and the 165 images were recorded with a JEOL 6360 LV microscope (Tokyo, 166 Japan) at 20-25 kV with different magnifications. The average scaf-167 fold thickness was measured at random sites through the analysis 168 of cross-section, top-view, and bottom-view SEM images. 169

2.5. Mechanical testing

Uniaxial tensile tests were performed as previously described 171 [16] on an Instron5542 testing frame (Norwood, MA, USA) 172 equipped with a 1000 N capacity load cell and Biopuls pneumatic 173 clamps. We randomly selected 6 pieces of BAMGs to evaluate the 174 mechanical testing. The bilayer BAMG-SF (N = 6) were trimmed 175 into rectangular strips (40 mm \times 10 mm) and hydrated in PBS for 176 at least 24 h to reach a swelling equilibrium prior to testing. Each 177 material was cut into a dog-bone shape before testing. Test sam-178 ples were submerged in a temperature-controlled testing con-179 tainer (Biopuls) filled with PBS (37 °C). Tensile testing was 180 performed by clamping each prepared specimen into a custom fab-181 ricated tensile tester with a 50-N load cell. The displacement con-182 trol mode with a crosshead displacement rate of 10 mm/min was 183 used. The initial elastic modulus (EM), ultimate tensile strength 184 (UTS), and % elongation to failure (ETF) were calculated from 185 stress/strain plots. The EM was calculated using a least squares 186 fit within the linear elastic region. The UTS was determined as 187 the highest stress value attained during the test, and the %ETF 188 was the last data point before the load decreased by more than 189 10%. Data were presented as the mean ± standard deviation. 190

2.6. Animals

Biomaterials were evaluated in a bladder augmentation model192using adult male Sprague Dawley rats (8 weeks old) following193IACUC-approved protocols, as previously described [20]. The194

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