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Expansion development planning of thermocracking-based bitumen upgrading plant under uncertainty



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ABSTRACT

Expansion development of upgrading plants is an important decision to make for the oil sands industry. In this paper, we propose a multistage stochastic expansion development method to tackle uncertain synthetic crude oil (*SCO*) and *CO*₂ tax prices. The linear decision rule based technique is applied to solve the proposed stochastic optimization model. Various analyses are conducted based on optimization results: (i) effects of the uncertainty set size, (ii) comparison of solutions for selected pessimistic, realistic, and optimistic scenarios, (iii) effects of different operating modes for an upgrading plant, and (iv) cost distribution. Results of this work demonstrate that the stochastic model provides a more flexible, economical, and robust solution negligibly compared to the *SCO* price. Finally, expansion development of the studied upgrading plant is economically beneficial even at the current market state.

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1. Introduction

Crude oil is the global dominant energy source and the reliance of the world economy on it is expected to continue for a long time. It is estimated that the worldwide demand of crude oil will reach 111 million barrels per day by 2040, and approximately 25% of it will be contributed by North America, including Canada and the United States (World Oil Outlook, 2014). Due to the increasing scarcity of conventional oil reserves, oil industries and governments are interested in unconventional oil resources. Note that oil reserves that cannot be accessed using conventional drilling techniques are referred as unconventional oil. These reserves (e.g., tight oil, oil shale and bitumen) need novel methods for extraction (Demirbas et al., 2017; Wang et al., 2016). After Saudi Arabia and Venezuela, Canada has the third largest oil reserves with proven 168 billion barrels (Woynillowicz et al., 2005). Furthermore, nearly 97% of total Canadian oil reserves are in the form of oil sands, which are mainly distributed in the Athabasca, Cold Lake, and Peace River areas in northern Alberta (Woynillowicz et al., 2005).

Unconventional oil production in Canada is continuously increasing. The oil sands bitumen production in Alberta is projected to reach 3.8 million barrels per day by 2022, which will be two times the production as of 2012 (Lazzaroni et al., 2016). While oil

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https://doi.org/10.1016/j.compchemeng.2018.01.007 0098-1354/© 2018 Elsevier Ltd. All rights reserved. price fluctuation affects profitability of the oil sands industry, important issue is how to adjust production and expansion planning under an uncertain market environment. Another major concern for the continuous development of the oil sands industry is the environmental management. Sustainable development with minimum environmental conservation is a concern of Alberta provincial and Canadian federal governments. To follow the international agreements (the United Nations Framework and Kyoto protocol), Canada is committed to mitigating its greenhouse gas (GHG) emissions. In Alberta, a carbon tax of \$15 per tonne of CO₂ was enacted in 2007 for the first time (Fact Sheet: Carbon Pricing Around the World, 2012). Recently, it was increased to \$20 and \$30 per tonne of CO₂ in 2016 and 2017 (Alberta Boosts Carbon Tax, 2015; Carbon Levy and Rebates, 2017). It is expected that the carbon tax rate will be increased; however, the exact future tax level is unknown. As it can be seen, the further development of the oil sands industry is accompanied with uncertainties in both the unpredictable oil price and changing environmental policies. Studying the development and expansion planning under uncertainties currently seems essential for the oil sands industry.

The uncertainty issue has received attention in various design and planning problems. The strategic planning of a bioethanolsugar supply chain was studied under demand uncertainty (Kostin et al., 2012). A two-stage multi-scenario mixed-integer linear stochastic programming approach was proposed, and a decomposition technique was applied to solve it based on the sample average approximation technique. It was further shown that the stochastic model lead to more robust solution compared to

Nomenclature		$\underline{\Omega}^{M}$	upper bound for the inlet to the upgrading plant $\left(\frac{tonne}{br}\right)$
Acronyms		QQ	lower bound for perceptile of capacity usage (%)
ARMA A	uto Regressive Moving Average	<u>Step</u>	lower bound for percentile of capacity usage (%)
DP D	Deterministic Problem	$\underline{\Sigma}_{p}^{r}$	lower bound for percentile of each product in n-
	biluent Recovery	V - V	nal blend (%)
al E	lectricity	$\underline{\Omega}_{p}^{\Lambda}, \Omega_{p}^{X}$	lower and upper bounds for expansion capacity
			(bpd)
GHG G	GreenHouse Gas	an	gradient of linear capital cost equation
HGO H	leavy Gas Oil	ASCO	constant coefficients vector of reformulated
<i>HGOHT</i> H	leavy Gas Oil HydroTreater		ARMA model at year t
ht H	leat	h	intercept of linear capital cost equation (M^{c})
HT H	lydroTreater	Dp DSCO	constant coefficients scalar of reformulated APMA
LDR L	inear Decision Rule	D _t	
LGO L	ight Gas Oil		model at year t
LGOHT L	ight Gas Oil HydroTreater	d	depreciation time (yr)
NPH N	Janhtha	h	the coefficients vector of general uncertainty set
	Japhtha HydroTreater	ir	annual real debt interest rate (%)
	lapinina nyuloneatei	OT	operating time (<i>hr</i>)
	iet Piesent value	P_t	truncate matrix at year t
SAGD S	team-assisted gravity Drainage	r	discount rate (%)
SCO S	ynthetic Crude Oil	UC1	unit conversion from cubic meter per hour into
SOR S	team-Oil-Ratio		harrel per day (^{bpd})
SP S	tochastic Problem		$\frac{m^3}{hr}$
st S	team	UC ₂	unit conversion from \$ to M\$ $(\frac{MS}{2})$
TC T	hermocracker	W	coefficient matrix of general uncertainty set
		7.	$1 \qquad \alpha \alpha$ guantile of standard normal distribution
Indices and sets		$z_{1-\alpha}$	I – a quantile of standard normal distribution
$n \in \mathcal{D}$ set of operating units		Decision	variables
$p \in P$ S	at of utilities	Λ	variable stemmed from dual counterpart of inequal-
$u \in \mathcal{U}$ So	et of time newinds		ity constraint
$l \in I$ so	et of time periods	CCAPEX	capital cost investment of year t (M\$)
$\mathcal{C} \in \mathcal{C}$ So	et of products	V _n t	binary capacity expansion decision for process n in
\mathcal{MP} SI	ubset of mixer-type units (NPHHT, LGOHT, HGOHT)	1 p, t	the year t
SP SI	ubset of splitter-type units (<i>DR</i> , <i>TC</i>)	миН2	mass flow rate of budrogen in budrotreater n at year
\mathcal{PC} SI	ubset of matching between product and associated	IVI p,t	tonne
h	ydrotreater		$t\left(\frac{totne}{hr}\right)$
		$M_{p,c,t}^{out}$	mass flow rate of outlet product <i>c</i> from splitter <i>p</i> at
Parameters			year $t \left(\frac{tonne}{hr}\right)$
α	significance level	M ⁱⁿ	mass flow rate of inlet to splitter <i>p</i> at year t (tonne)
α^{yield}	vield coefficient of splitter-type units	MHTout	mass flow rate of outlet from hydrotreater n at year
H_2	hadre and manipulation of the state of the s	lv1 p,t	(tonne)
α_p^2	hydrogen requirement coefficients $\left(\frac{conte}{m^3}\right)$	110	$t\left(\frac{tonte}{hr}\right)$
α_p^{HI}	yield coefficient of mixers	$M_{p,t}^{H2}$	mass flow rate of hydrogen in hydrotreater p at year
$\beta_{p, u}$	energy requirements coefficient $\left(\frac{energy}{tonne}\right)$		$t\left(\frac{tonne}{hr}\right)$
γ^{CO_2}	carbon tax economic coefficient $\left(\frac{\$}{100000000000000000000000000000000000$	MSCO	total mass flow rate of SCO at year t (tonne)
Ritumen	$Conne CO_2$	E .	energy consumption of utility u at year t (energy)
γ_{r}^{bhumen}	Bitumen price $\left(\frac{s}{bbl}\right)$	$L_{u, t}$	capacity expansion of process n to be installed in
γ_u^E	energy requirements economic coefficients	Λ <i>p</i> , <i>t</i>	capacity expansion of process p to be instance in
	$\left(\frac{s}{energy}\right)$		
ν^{H_2}	hydrogen requirement economic coefficients	<i>Qp</i> , <i>t</i>	total capacity of process p in period t (bpd)
,	$\left(\frac{\$}{1}\right)$		
V MAINEX	maintenance economic coefficient		
, SCO	SCO price $\left(\frac{\$}{2}\right)$	the determ	ninistic model. The strategic investment planning of a
γ Γ	a scalar to control the uncertainty set size	multi-prod	uct, multi-period supply chain problem was investi-
sE	a scalar to control the uncertainty set size	gated (Oliv	reira et al., 2013). To address the demand uncertainty,
o_u	tonne CO ₂	a two-stag	e mixed-integer linear stochastic programming model
	$\left(\frac{\cos(\log 2\sigma_2)}{\operatorname{energy}}\right)$	with risk	consideration was taken into account to reduce the
δ^{H_2}	GHG emission coefficient of Hydrogen $\left(\frac{\text{tonne CO}_2}{\text{tonne}}\right)$	chances of	very large objective function values during minimiza-
δsco	GHG emission coefficient of SCO production	tion A tw	vo-stage mixed-integer linear stochastic programming
	$\left(\frac{\text{tonne CO}_2}{2}\right)$	was applie	d for the expansion planning of electricity generation
6+	uncertainties for SCO price	mas applied for the expansion planning of electricity generation	
~. 7.	uncertainties for CO_{-} tay price	piques (real combustion turbing publication combined and	
5 t A	ARMA ARMA model coefficients	inques (coal, compusition turpine, nuclear, compined cycle and	
0 q	density (tonne)	wind generator) were considered. The load and wind availabilities	
ρ_p	$\frac{1}{m^3}$	were the uncertain parameters which were defined as independent	
φ_p	AKIVIA AKIVIA model coefficients	and identically distributed random variables. Environmental regu-	
$\Omega_t^{investment}$	capital investment limitation corresponding to	lations (ind	cluding carbon tax and a renewable portfolio standard)
	period t (M\$)	were impo	sed on the model as well. This model was solved us-

ing the L-shaped method based on the Monte Carlo simulation.

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