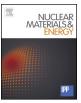
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# First-principles calculations of interaction between solutes and dislocations in tungsten



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<i>Keywords:</i> Solution softening Transmutation products Dislocation First-principles Tungsten alloys	Changes in mechanical properties due to transmutation products (Re and Os) in W alloys is a central issue for plasma-facing materials in fusion reactors. We conducted density functional theory calculations to investigate the effect of Re, Os, and other 5d solutes on core structure and motion of screw dislocations associated with plastic deformation. Ir, Pt, Au, and Hg solutes show strong attractive interactions with screw dislocations, causing solution strengthening by the pinning mechanism. On the other hand, Hf, Ta, and Re cause softening by facilitating dislocation motion around solutes. This prediction corresponds well with the experimental observation of softening behavior in W-Re alloys.

#### 1. Introduction

Tungsten (W) is a potential candidate for plasma-facing materials in fusion reactors due to its high melting point and thermal conductivity, as well as its high resistance to neutron sputtering [1-8]. Structural materials exposed to high deuterium and tritium fluxes under 14 MeV neutron irradiation, which releases significant amounts of transmutation products such as hydrogen and helium, experience degradation of their physical and mechanical properties [9-11]. The relationship between trapping of transmutation gas products and surface damage has been widely investigated [12–15]. The other important aspect of neutron irradiation in fusion reactors is the transmutation products of W [16]. Neutron irradiation produces increasing amounts of 5d metals such as rhenium (Re) and osmium (Os) with increasing fluxes, where Re is initially produced and then Os is created from Re. The stability of these transmutation products is a central issue when W alloys are used in fusion reactors, since fusion products may alter the mechanical properties of structural materials. The changes in mechanical properties, such as hardness and microstructure, due to irradiation have been examined for pure W, W-Re, W-Os, and W-Re-Os alloys [17], and clear differences were found between Re and Os in terms of the effect of irradiation hardening. Hardness decreases with Re content up to 10 mass% for low-dose neutron irradiation (below 1.54 dpa), while it increases linearly with the total concentration of Re and Os at higher doses [18], where precipitation nucleated by the irradiation contributes directly to the hardness. More recently, the local distribution of Re in W-Re and W-Re-Ta alloys under irradiation has been investigated using atom probe tomography, revealing that Re clustering tends to occur in these alloys [19]. On the other hand, it has long been known that Re solutes in W alloys cause solution softening [20–23], and that this softening behavior depends on both temperature and alloy composition. In particular, W-Re alloys exhibit a strong ductilization tendency at low temperatures (below 300 K) and low solution concentrations (about 10 at.%) [21], which is thought to be due to the effect of Re solutes on the double kink nucleation process [22]. The effects of individual transmutation solutes on mechanical properties, as well as the formation of radiation defects such as voids and radiation-induced precipitation (RIP), are therefore of great importance for W alloys under neutron irradiation.

We have so far carried out first-principles and kinetic Monte Carlo calculations to investigate the formation of radiation defects such as RIP in W alloys [24–26]. The formation and motion of W-Re and W-Os pairs in perfect crystals and some mixed dumbbell structures provide an insight into the effect of these elements on radiation defect formation. It is also important to understand solid solution strengthening and softening behavior in W, since W is intrinsically brittle. Regarding the effect of individual solutes on mechanical properties, the solution softening observed at low temperatures was found to be common to various body-centered cubic (BCC) metals [27]. Screw dislocation motion is a fundamental plastic deformation mechanism in BCC metals, and therefore

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the fundamental properties of dislocation motion associated with the core structure in W [28] and the effect of Re solutes on dislocation core structure [29–33] were investigated by density functional theory (DFT) calculations, where some sophisticated models were proposed. The stress-dependent interaction energy and migration process of Re in W alloys was investigated using DFT and kinetic Monte Carlo calculations [32], and softening effect was investigated by DFT and theoretical models in cooperation with the interaction between solute and a screw dislocation [33]. However, the energy barrier for dislocation motion should be considered as well as the interaction energy. In the present study, we construct a dipole configuration of screw dislocations in a periodic cell and investigate in detail the effects of Re and other 5*d* solutes on the interaction motion through DFT calculations.

#### 2. Analysis method

The introduction of dislocations into our periodic cell was accomplished by applying a continuum linear elastic theory solution for a periodic dislocation dipole array [34] in BCC W with lattice constant  $a_0 = 3.1715$  Å. We can effectively solve for the distortion field in the periodic cell using a Fourier series, where the elastic energy can be expressed in Fourier space associated with elastic constants. The distortion field was then chosen to minimize the total elastic energy, subject to the topological constraints imposed by the dislocations. The displacement field can be obtained via line integrals. The displacement field of dislocation dipole in a 135-atom supercell was then obtained. In the present study, screw dislocation core with the Burgers vector 1/ 2 < 111 > was considered. The position of dislocation and solutes were shown in Fig. 1, where the core structure of the screw dislocation dipole was visualized using a differential displacement (DD) map [35]. The unit cell vector of the supercell for a dislocation quadrupolar is  $y = 2.5a_0[11\overline{2}] + 4.5a_0[\overline{1}10] + (a_0/4)[111],$  $x = 5a_0[11\overline{2}],$ and  $z = (a_0/2)[111]$ . We used two- and six-layer supercell models along the z direction with a total of 270 and 810 atoms, respectively to confirm the convergence of the size along the direction, and two solutes were introduced near each side of the dipole's dislocation cores. The interaction energy between the 5d solutes and the screw dislocation dipole was then evaluated. First-principles electronic structure calculations were carried out within the DFT framework using the Vienna Ab-initio Simulation Package (VASP) [36,37], with the Perdew-Burke-Ernzerhof generalized gradient approximation exchange-correlation density functional [38]. The Brillouin-zone k-point samplings were chosen using the Monkhorst-Pack algorithm [39], where  $1 \times 1 \times 9$  and  $1 \times 1 \times 3$  k-point samples along x, y, and z directions were used for structural relaxation of two- and six-layer models, respectively. We used a plane-wave energy cutoff of 400 eV, with a first-order Methfessel-Paxton scheme employing a smearing parameter of 0.1 eV. We ensured that the total energy converged to within  $10^{-6}$  eV for all

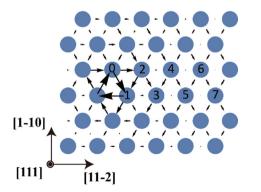


Fig. 1. The relative position of dislocation core and solutes, where the differential displacement vector is used to visualize the dislocation core.

calculations. The relaxed configurations were obtained by the conjugate gradient method, and the search was terminated when the force on all atoms had reduced to 0.02 eV/Å. The energy barrier and saddle point during dislocation motion for pure W were evaluated by the nudged elastic band (NEB) method with nine replica images [40].

#### 3. Results and discussion

We first evaluated the interaction energy between the 5d solutes and the screw dislocation without atomic relaxation to understand the general features of the interaction, with the solutes being substituted at sites 0 to 7 according to Fig. 1. Fig. 2 shows the effect of the relative position (or distance) between the solutes and the dipole on the interaction energy for each solute, where the relative position of dislocation core is unchanged to constrain the dislocation motion influenced by high solute concentration. The interaction energy is defined as the energy difference between site 0 and furthest site from dislocation core. Strong attractive interactions were observed with the screw dislocation in iridium (Ir), platinum (Pt), gold (Au), and mercury (Hg), while hafnium (Hf), tantalum (Ta), and Re had relatively weak interactions and Os was in the middle. In addition, we found that the effective range of the interaction for most of the solutes was up to the 3rd nearest neighbor in the (111) plane, with little difference between the different solute types.

We then evaluated the actual interaction energy, considering atomic relaxation, for 1st nearest neighbor configuration (sites 0 and 1). Fig. 3(a) shows the interaction energies between all 5d solutes and a screw dislocation per a solute, where the solute is supposed to be substituted in every 2b units along the dislocation line. For confirmation of the convergence of the supercell size, we calculated the interaction energy only when each solute is substituted at site 0 using 6b unit supercell as shown in Table 1 and found that 2b unit reproduces the tendency well. The trends and absolute values are approximately the same as the ones calculated using unrelaxed configurations, indicating that the electronic interaction primarily determines the interaction energy. As discussed about d-band filling for bcc transition metals [41], the electronic interaction plays a significant role in the interaction energy in case of screw dislocation because there is no volumetric strain component unlike edge dislocations. Ir, Pt, Au, and Hg showed strong attractive interactions with the screw dislocation, resulting in solid solution hardening via the pinning mechanism. In addition, after atomic relaxation, the 3rd nearest neighbor configuration (site 3) for these solutes converged to the 1st nearest neighbor configuration (associated with site 1) due to the short-range strong attractive interaction with high solute concentration. On the other hand, since the interactions with Hf, Ta, and Re were not so strong, the dislocation did not move even when these solutes were substituted in 2nd nearest neighbor configuration. These results suggest that Hf, Ta, and Re at least do not induce solution strengthening.

Fig. 3(b) shows the relaxed core structures around typical Re, Os, and Au solutes, visualized by DD maps. We found that weakly-interacting solutes, such as Re, did not change the core structure, while those with attractive interactions, such as Au, causes reconstruction of the core structure, that is, the stable easy-core changes into a split core by the presence of these solutes. We should note, however, that this change of core structure is caused by high solute concentration and therefore, the interaction energy would be overestimated. There is still difficulty in simulating dilute alloys due to the computational cost though larger atomic models along dislocation line should be used.

The energy barrier to kink nucleation is important when discussing the effect of solutes on plastic deformation. The kink nucleation rate is expressed as the thermally activated process, which is associated with the external stress and the solute concentration as follows [42]: Download English Version:

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