



# Adsorption breakthrough and cycling stability of carbon dioxide separation from CO<sub>2</sub>/N<sub>2</sub>/H<sub>2</sub>O mixture under ambient conditions using 13X and Mg-MOF-74

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## HIGHLIGHTS

- Adsorption separation of CO<sub>2</sub> from dry and humid CO<sub>2</sub>/N<sub>2</sub> mixture is carried out under ambient conditions.
- Experimentally validated model is applied by a user-defined-function in ANSYS Fluent.
- 13X and Mg-MOF-74 are tested for breakthrough and cyclic CO<sub>2</sub> separations.
- Dehydration process before CO<sub>2</sub> adsorption processes is strongly recommended.
- Cycling separation is recommended to be used instead of breakthrough tests.

## ARTICLE INFO

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## ABSTRACT

Carbon dioxide and storage is an efficient method to reduce the emitted CO<sub>2</sub> from the burning of fossil fuels. Zeolite-based materials are conventional adsorbents used to adsorb some gasses involving carbon dioxide. Mg-MOF-74 is an eminent reticular material among adsorbents due to its good CO<sub>2</sub> capacity at low pressures (10–20 kPa). In this study, an experimentally validated model is used to report the H<sub>2</sub>O effect on CO<sub>2</sub> separation using 13X and Mg-MOF-74 under ambient conditions. A computational model has been developed using ANSYS Fluent program linked by user-define-function (written in C). The adsorption breakthrough results show that a humid CO<sub>2</sub>/N<sub>2</sub> mixture, under 300 K, 86% RH, 101.3 kPa, could slightly reduce the CO<sub>2</sub> adsorption capacity by about 0.05% and 6% for 13X and Mg-MOF-74, respectively (at CO<sub>2</sub> adsorption breakthrough saturation). Regardless of these reductions, Mg-MOF-74 has better adsorption capacity, even under humid ambient conditions, by about 5.77 mmol/g in a comparison to 2.27 mmol/g for 13X, respectively.

Cycling stability over more than 90 cycles is also simulated; and shows that, a dehydration process is recommended to be carried out before the CO<sub>2</sub> separation process for efficient energy consumption and sustainable adsorbents. The total recyclable amounts of adsorbed CO<sub>2</sub> are about 0.94 and 3.07 mmol/g for 13X and Mg-MOF-74, respectively, under 101.3 kPa adsorption, 2 kPa desorption, 86% relative humidity, and 298 K. The cyclic CO<sub>2</sub> separation is found to be a robust method more than the breakthrough separation to evaluate the real adsorption capacities.

## 1. Introduction

CO<sub>2</sub> separation by the adsorption technologies is growing vastly. The utmost advantage of the adsorption separation processes is the simplicity of adsorbent regeneration by means of heat, vacuum or both [1]. Carbon- and zeolite-based adsorbents are well-known materials exploited for the CO<sub>2</sub> separation. In particular, zeolite-based adsorbents show better CO<sub>2</sub> uptakes than activated carbons under lower operating

pressures (10–20 kPa) such as NaY, 13X [2], and CNT/13X [3], whereas carbon-based adsorbents are preferred under high pressures (CO<sub>2</sub> adsorptive storage pressures > 5 bar) [4]. Metal-organic frameworks (MOFs) are a new class of novel adsorbents [5]. Specifically, MOF-74 (e.g., MOF-74(Ni, Co) [6] and MOF-74(Mg) [7]) shows a good CO<sub>2</sub> adsorption capacity and CO<sub>2</sub> over N<sub>2</sub> selectivity. Quantitatively, Mg-MOF-74 was tested to have the highest CO<sub>2</sub> adsorptive capacity under low-pressure conditions (350 mg/g at 298 K and 1 bar) [7].

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**Nomenclature**

$C$	molar concentration of gas, mol/m <sup>3</sup>
$C_p$	specific heat capacity, J/kg·K
$D, d$	bed diameter, particle-size, m
$D_{disp}$	coefficient of gas dispersion, m <sup>2</sup> /s
$E_g$	energy of gas-phase, J/m <sup>3</sup>
$E_s$	energy of solid-phase, J/m <sup>3</sup>
$h$	enthalpy, J/kg
$h_{ext}$	coefficient of heat transfer at outer bed surface, W/m <sup>2</sup> ·K
$h_{int}$	coefficient of heat transfer at internal bed surface, W/m <sup>2</sup> ·K
$\Delta H$	adsorption heat, J/mol
$\vec{g}$	acceleration vector of gravity, m/s <sup>2</sup>
$\vec{J}$	flux due to diffusion, kg/m <sup>2</sup> ·s
$K_o$	constant in Toth equation, 1/Pa
$K_{eq}$	constant in Toth equation, 1/Pa
$k$	thermal conductivity, W/m·K
$k_L$	time constant of LDF, 1/s
$M$	mass weight, kg/mol
$n$	constant in Toth equation
$q$	actual adsorbed gas, mmol/g
$q^*$	equilibrium adsorbed gas, mmol/g
$q_m$	capacity limit, mmol/g
$Q_F$	inlet flow rate, m <sup>3</sup> /s
$P$	pressure, Pa
$R$	universal gas constant, J/mol·K
$r$	radius, m
$Re$	Reynolds number
$t$	time, s

$T$	operating temperature, K
$\vec{\tau}$	stress tensor, N/m <sup>2</sup>
$y$	weight fraction
$\vec{v}$	velocity, m/s

**Greek letters**

$\rho$	gas density, kg/m <sup>3</sup>
$\varepsilon$	porosity of adsorbent bed
$\gamma$	heat capacity ratio
$\varepsilon$	thermal emissivity
$\mu$	dynamic viscosity, Pa·s
$\eta$	vacuum pump efficiency
$\sigma$	Stefan Boltzmann coefficient, W/m <sup>2</sup> ·K <sup>4</sup>
$\tau$	tortuosity

**Subscripts**

eff	effective
p	particle
max	maximum
min	minimum
pore	pore of adsorbent
$i$	species index of gas
$g$	gas
$s$	standard conditions
$0$	inlet, saturation
$w$	wall

**1.1. CO<sub>2</sub> separation under humid conditions**

Many studies have been conducted on developing water-stable adsorbents to be used in the CO<sub>2</sub> capture processes [8]. Some materials showed a significant reduction in the CO<sub>2</sub> adsorption in the presence of water while others were stable. It is found that CO<sub>2</sub> recovery was minimized by 22% using 13X under 95% RH, 30 °C, and 1.2 bar [9]. However, 13X has been tested and showed an excellent stability under humid conditions [10]. The structural stability tests under humid conditions (298 K and RH < 90%) showed that HKUST-1, Mg-MOF-74, and UiO-66 (–NH<sub>2</sub>) retained a good structuration while DMOF-1, DMOF-1-NH<sub>2</sub>, and UCM-1 were not stable and completely lost their crystallinity [11]. A negligible drop in CO<sub>2</sub> uptake was observed by testing HKUST-1 and Ni/DOBDC under humid conditions [12]. MOF-841 was, also, reported as a water and cycling stable adsorbent [13].

Despite the high CO<sub>2</sub> uptake of Mg-MOF-74, the presence of H<sub>2</sub>O reduced the CO<sub>2</sub> capture capacity, unlike some MOFs such as HKUST-1 and MIL-101(Cr) [14]. For example, at 1 bar and 298 K, about 8.4 mmol/g CO<sub>2</sub> could be adsorbed by dry Mg-MOF-74; while under hydration of 6.5% and 13%, about 6.7 mmol/g and 5.4 mmol/g CO<sub>2</sub> could be adsorbed, respectively [14]. It is also reported that Mg-MOF-74 has higher H<sub>2</sub>O hydrophilicity (593 mL/g at 298 K and 1 bar) than zeolite [15]. The reduction of CO<sub>2</sub> uptake at 373 K, 9% RH, and 101.3 kPa was addressed to be about 47% using Mg-MOF-74 [16].

The functionalization of MOFs by amine groups showed a higher CO<sub>2</sub> uptake under H<sub>2</sub>O presence than those under dry conditions [17]. Amine-impregnated silicic acid composite was introduced as a candidate adsorbent for CO<sub>2</sub> separation having a CO<sub>2</sub> uptake of 4.54 mmol/g at 25 °C under 10 vol% CO<sub>2</sub> and 10 vol% H<sub>2</sub>O [18]. Polyethyleneimine (PEI)-impregnated millimeter-sized mesoporous carbon spheres (MCSs) showed an excellent stability for CO<sub>2</sub> capture in the presence of H<sub>2</sub>O [19]. KFUPM-1 (polymer-adsorbent treated by amine-group) showed a higher cyclic stability and CO<sub>2</sub> uptake under the presence of water vapor [20]. About 0.75 cyclic CO<sub>2</sub> uptake was achieved using CaO/

MgO (calcium-based adsorbent) under real conditions [21]. Recently, some adsorbents were proposed to be water-stable for CO<sub>2</sub> post-combustion such as dmpn-Mg<sub>2</sub>(dobpdc) [22], NbOFFIVE-1-Ni [10], nHept-2-Mg<sub>2</sub>(pc-dobpdc) [23], IRMOF-74-III-(CH<sub>2</sub>NH<sub>2</sub>)<sub>2</sub> [24], and ZIF-300 [25]. Notwithstanding that some MOFs exhibit water and thermal stability, there are many challenges for such adsorbents to be applicable to commercial and real-world; e.g., combining high CO<sub>2</sub> capacity with high CO<sub>2</sub>/N<sub>2</sub> selectivity in the presence of humidity [8].

**1.2. Energy consumption by carbon capture processes**

The energy penalties due to the separation of CO<sub>2</sub> in power plants were estimated in the literature. The cost of avoiding CO<sub>2</sub>, for amine scrubbing plant integrated with natural gas combined cycles, was evaluated to be between \$82.6 and \$121.8 per tonne of CO<sub>2</sub> [26]. Bicarbonate-forming solvents could also be used for carbon capture with CO<sub>2</sub> avoid energy about 0.27 kWh/kg CO<sub>2</sub> [27]. The average annual CO<sub>2</sub> emission rate for the integrated gasification combined cycle (IGCC) integrated with membrane CO<sub>2</sub> capture, was at 89 kg CO<sub>2</sub>/MWh [28]. Analogous to thermodynamic cycles, the carbon pump theory was used for investigating thermodynamics and energy consumption of the TSA process [29]. Incorporating secondary materials (such as CNT) with MOFs could increase the CO<sub>2</sub> uptake and decrease the regeneration energy; it is found that the CO<sub>2</sub> uptake increased by 36% for MIL-101(Cr) [30] and about 8% for Mg-MOF-74 [31].

Among different CO<sub>2</sub> separation technologies, the electric adsorption separation process was addressed to be economically infeasible for CO<sub>2</sub> capture [32]. The effect of water vapor on the CO<sub>2</sub> separation using activated carbon (coconut shell Acticarb GC1200) was small, but it has a high impact on the power consumption (~35%) of vacuum swing adsorption process [33]. The energy consumption of CO<sub>2</sub>-loaded aqueous amine solution using Al<sub>2</sub>O<sub>3</sub>/HZSM-5 bifunctional catalysts was found to be less than a catalyst-free test by 23.3–34.2% [34]. For separating CO<sub>2</sub> from the atmospheric air, the energy consumption was

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