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# $\mathrm{CO}_{\mathrm{x}}$ free hydrogen production through water-gas shift reaction in different hybrid multifunctional reactors



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#### HIGHLIGHTS

# G R A P H I C A L A B S T R A C T

- Experimental WGS study in different reactor configurations: TR, MR, SER and SEMR.
- H<sub>2</sub> and/or CO<sub>2</sub> separation from the reaction zone intensifies the process.
- The equilibrium is completely shifted allowing to obtain two ultra-pure H<sub>2</sub> streams in the SEMR.
- Using steam during regeneration enhances the hydrotalcite working sorption capacity.

# ARTICLE INFO

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# ABSTRACT

High-purity  $H_2$  production from the water-gas shift (WGS) reaction was assessed. Since the WGS is limited by the equilibrium, different reactor types that allow to extract one or more products from the reaction medium, namely membrane reactor (MR; for  $H_2$  separation), sorption-enhanced reactor (SER; for CO<sub>2</sub> capture) and sorption-enhanced membrane reactor (SEMR; for simultaneous CO<sub>2</sub> and  $H_2$  removal), were used and compared with fixed-bed traditional reactor (TR). Experimental results were obtained with commercial materials, namely WGS Cu-based catalyst and K-doped hydrotalcite for CO<sub>2</sub> capture. Additionally, in the MR and SEMR, a self-supported Pd-Ag membrane for separating  $H_2$  selectively from the reaction zone was used.

Experimental tests were performed at different temperatures and pressures, and the results obtained were compared with those predicted by theoretical simulations at the thermodynamic equilibrium. Moreover, in the case of SER, different methods for the hydrotalcite regeneration and the evaluation of its working sorption capacity under cycling conditions were also assessed. Not all sorbed  $CO_2$  can be desorbed under dry conditions (pure nitrogen purging stream); however, if steam is used during the regeneration step, all sites can be effectively regenerated, allowing to have a stable working sorption capacity. Concerning the performance of the different hybrid reactors tested, i.e. MR, SER and SEMR, it was found that all are able of overcoming the TR limitations, with performances reaching conversion above the equilibrium for the feed composition. Nonetheless, only the SER and SEMR configurations allow to obtain high-purity H<sub>2</sub> in all reactor exiting streams under the operating conditions herein assessed.

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#### 1. Introduction

Hydrogen is recognized as an emerging new energy carrier due to its waste-free combustion, and high energy mass density [1]. It can be used not only as raw material in the chemical and petrochemical industrial sectors, but also in fuel cells and internal combustion engines without  $CO_2$  emissions [2,3].

Hydrogen is produced from both renewable and non-renewable resources through diverse processes such as methane steam reforming, coal gasification, water electrolysis or biomass gasification [4]. Currently, methane steam reforming is the most widely route used to produce hydrogen at industrial scale [5]. The steam reforming stage, which produce syngas (a mixture of CO and H<sub>2</sub>), is followed by two successive water-gas shift (WGS, Eq. (1)) reaction steps to maximize the conversion of CO [6]. Such reaction finds application in several industrial processes [7].

$$CO + H_2 O = H_2 + CO_2 \quad \Delta H_{298}^0 = -41 \cdot kJ \, mol^{-1}$$
(1)

As the WGS is an equilibrium-limited reaction, apart from  $H_2$  and  $CO_2$  there are other chemical species (CO and  $H_2O$ ) at the end of this reaction step, i.e. at the reactors' outlet.

Carbon monoxide is a poison both to several catalytic processes employed in fuels production and to anode catalysts currently used in polymer electrolyte membrane fuel cells (PEMFCs) [8,9], and so purification of the reformate gas prior to use is required. Thus, to obtain hydrogen with the required purity, a final pressure swing adsorption (PSA) unit is often required [10,11]. PSA reportedly produces high purity H<sub>2</sub>, up to 99.9%, but the H<sub>2</sub> recovery is about 75–90% since part of the H<sub>2</sub> recovered is used to regenerate the adsorbent [11–13].

Alternatively, a sorption-enhanced reactor (SER) has been proposed as an effective approach to high-purity  $H_2$  production with low concentration of CO, by shifting the thermodynamic equilibrium of the WGS reaction towards  $H_2$  generation by *in-situ* removing CO<sub>2</sub> through adsorption. Nevertheless, the main disadvantage of the SER is that the CO<sub>2</sub> sorbent gets saturated at some point and then regeneration is needed. For obtaining cyclic operation, at least two parallel reactors are needed: while one is producing  $H_2$ , the other is being regenerated, i.e., CO<sub>2</sub> is being removed from the sorbent with an inert gas. This approach is similar to the one used in other cyclic adsorption processes like PSA [11,14].

Different sorbents like hydrotalcites [15–17], CaO-based materials [18,19], MgO-based materials [20–22], lithium zirconates [23–25] and lithium silicates [26,27] have been reported in the literature as  $CO_2$  sorbents for SERs technologies. It is expected, from a good  $CO_2$ -selective sorbent, to have a high  $CO_2$  sorption capacity and selectivity at moderate temperatures, effective regeneration at moderate temperatures, good hydrothermal and mechanical stability and low cost. Since one of the goals in this work is to perform experiments at relatively low temperatures (300–350 °C), a hydrotalcite sorbent was used. It displays high  $CO_2$  equilibrium capacity and fast sorption kinetics, good regeneration and has a great stability [15,28,29]. Moreover, the fact that the  $CO_2$  capacity of hydrotalcites is strongly enhanced in the presence of steam makes them an even better sorbent for use in the WGS process, where water is a reactant [30].

Besides the CO<sub>2</sub> sorption-enhanced process, palladium based membrane reactors (MRs) have also shown to be promising for overcoming equilibrium limitations in reversible reactions like the WGS, yielding high-purity streams of H<sub>2</sub> with low concentration of CO [31,32]. This is reached by shifting the thermodynamic equilibrium of the reaction toward H<sub>2</sub> generation by in-situ removing H<sub>2</sub> through permeation. Pd-based membranes are currently the most promising for high-purity H<sub>2</sub> production in MRs, especially Pd alloys (e.g. Pd–Ag) that are less sensitive than pure Pd to embrittlement (caused by the presence of H<sub>2</sub> at temperatures below 300 °C and pressures below 2 MPa) and poisoning (caused by contact with CO, for example) [33–36]. Tosti *et al.*  [37] demonstrated that self-supported dense Pd–Ag (with 23–25 wt.% of Ag) tubular membranes with finger-type configuration are highly durable and reliable since they allowed to attain complete  $H_2$  selectivity and no failures were observed after long time of thermal and hydrogenation cycles. These characteristics, together with high permeability, make such membranes very promising for high-pure  $H_2$  production. Due to these reasons, in this work one of such membranes was used.

The WGS reaction has been identified as one of the processes wherein both H<sub>2</sub> yield and purity can be improved by using either a MR [38–40] or a SER [17,41,42]. To apply this technology with the simultaneous removal of both products, it is necessary to use a H<sub>2</sub>-selective membrane and a CO<sub>2</sub>-selective sorbent, in a hybrid sorptionenhanced membrane reactor (SEMR). This reactor has several advantages: (i) the reaction and purification of the generated stream can be performed in a single unit; (ii) it allows decreasing the necessary Pd-Ag membrane area, compared to a MR, which is important due to its price; and (iii) high-purity H<sub>2</sub> can be directly produced with simultaneous CO<sub>2</sub> capture [11].

This work aims at comparing the performance of different reactor types (for the low temperature WGS reaction) including a traditional fixed-bed reactor (TR) and hybrid reactors, namely MR, SER and SEMR. In a previous work [11] we have studied the WGS reaction in a SEMR, but in this case, a longer Pd-Ag membrane and higher temperatures of reaction were employed, allowing to reach improved hydrogen recoveries. Moreover, comparison between obtained experimental values and simulated thermodynamic limits are now addressed, along with the assessment of the hydrotalcite working sorption capacity during reaction tests.

# 2. Experimental

# 2.1. Reactor types and materials

Fig. 1 shows a conceptual scheme of the different reactors studied. The sorption-enhanced reactor (SER) is similar to the fixed-bed traditional reactor (TR) with the difference that in such reactor the catalyst is mixed with the  $CO_2$  sorbent for removing the  $CO_2$  as it is being formed, shifting the reaction toward the products. In the case of a membrane reactor (MR) or a SEMR, the perm-selective membrane divides the reactor into the reaction and the permeate zones; hydrogen selectively permeates the membrane from the reaction zone (retentate) to the permeate side due to hydrogen partial pressure gradient across the membrane. Such driving force can be increased using an inert sweep gas flow (e.g. He, N<sub>2</sub>, steam, etc.) or by (vacuum) pumping in the permeate side.

The reaction experiments were carried out with a commercial Cubased WGS catalyst manufactured by Johnson Matthey (Ref. HIFUEL230), which requires operating temperatures between 200 and 350 °C. In the case of the SER and SEMR, a K-promoted hydrotalcite (MG30-K) supplied by Sasol was used as well. More details about MG30-K can be found elsewhere [11].

# 2.2. Experimental set-up

The fixed-bed and sorption-enhanced reactors consist of a stainless steel tube with a length of 120 mm and 10 mm o.d., which was loaded with the Cu-based catalyst (355 <  $\emptyset$  < 550 µm) diluted with glass beads (Sigma Aldrich 212–300 µm) in the case of the TR, and mixed with the MG30-K hydrotalcite (355 <  $\emptyset$  < 550 µm) in the SER. Along the bed 2 thermocouples were placed at 40 and 80 mm from the inlet.

The MR and SEMR consist of two tubes with different diameters (cf. Figs. 1c and d); the tube with lower diameter is the self-supported Pd-Ag membrane (with 23–25 wt.% of Ag – length of 120 mm, 10 mm o.d. and 150  $\mu$ m of wall thickness), which was welded at both ends to steel tubes to form the permeator tube. The steel tube of higher diameter is where the sweep gas goes in, as it flows in the annular section,

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