

Contents lists available at ScienceDirect

Energy Conversion and Management



journal homepage: www.elsevier.com/locate/enconman

Thermodynamic balancing of the regeneration process in a novel liquid desiccant cooling/desalination system



M.A. Ahmed, Naef A.A. Qasem, Syed M. Zubair*, P. Gandhidasan, Haitham M. Bahaidarah

Mechanical Engineering Department, KFUPM Box # 1474, King Fahd University of Petroleum & Minerals, Dhahran 31261, Saudi Arabia

balancing of the regeneration process in a hybrid liquid desiccant cooling/
incing technique is investigated by adding a single extraction between the
his technique is considered as a potential method to reduce energy con- term performance, dramatically. The mathematical procedure to model the h is outlined to study the effect of extraction on the hybrid system per- single extraction and without extraction (zero extraction), is analyzed in eration, local enthalpy losses, the coefficient of performance, and proper that at enthalpy pinch of 20 kL per kg of dry air single extraction system

water per hour as a by-product compared to 94.2 kg per hour for the zero extraction system.

1. Introduction

In coastal areas, there are extreme seasonal variations in temperature and humidity over the course of year; this is why air conditioning is a necessity in these areas. About 70% of produced energy is consumed by air conditioning in these regions. In general, the energy consumption by buildings represents 30–40% of the world's primary energy consumption [1]. In addition, freshwater is turning into a scarce resource in many regions around the world. Population expanding causes an increase in consumption of freshwater, especially in the stressed regions. The mankind is facing a water shortage, with demand expected to surpass supply by 40% in 2030 [2]. Therefore, water purification methods in conjunction with conservation efforts are needed in places where the natural resources of potable water are diminishing [3].

For these reasons, many places are facing two major problems that affect the existence and comfort of its population. These problems are due to high-energy demand and water scarcity. Therefore, cost-effective and environmentally friendly cooling and desalination techniques become an essential requirement. These techniques should be able to effectively utilize waste heat, renewable energy, etc. The desiccant-based hybrid cooling/desalination system [4] can help in solving some of the increasing energy demand [5]. The desiccant-based hybrid system does not use ozone-depleting refrigerants which makes it eco-friendly [6].

Desiccant-based systems for cooling and desalination purposes were

investigated in the literature. Hybrid solar still with a desiccant regeneration and desalination of saline water were studied by Modi and Shukla [7]. Su et al. [8] proposed a hybridization between the liquid desiccant dehumidification and solar-powered absorption refrigeration system for cooling and water production. Yang et al. [9] suggested a new method for regenerating liquid desiccant in a cooling system using photovoltaic (PV) capacitive deionization. Kabeel et al. [10] studied an indirect evaporative air cooler with baffles integrated with HDH desalination system. The hybrid system was powered by air and water solar thermal collectors. The liquid desiccant cooling systems were reviewed by Abdel-Salam and Simonson [11]. Moreover, solar-powered absorption chillers involving liquid desiccant cooling systems have been recently reviewed by Shirazi et al. [12]. A novel desiccant system hybridized with HDH for a zero-brine discharge is introduced by Ahmed et al. [13].

Tue et al. [14] introduced a novel desiccant-enhanced direct expansion heat pump, with a coefficient of performance (COP) more than 6. A novel hybrid liquid desiccant cooling/desalination system has been proposed [4] by adding a condenser between the humidifier and regenerator chambers. The benefit of adding a condenser was to recover the heat of outlet scavenging air from the regenerator. This resulted in improving the system performance by 11.25%. Besides the heat recovery, the moisture content in the recirculated air was condensed leading to about 86.4 kg/h freshwater.

* Corresponding author.

E-mail address: smzubair@kfupm.edu.sa (S.M. Zubair).

https://doi.org/10.1016/j.enconman.2018.09.012

Received 1 May 2018; Received in revised form 2 September 2018; Accepted 3 September 2018 0196-8904/ © 2018 Elsevier Ltd. All rights reserved.

Nomenclature		ω «	humidity ratio $(kg_{H_{2O}} kg_{da}^{-1})$	
Acronyms				
		Subscripts		
COP	coefficient of performance	1		
HDH	humidification dehumidification	1, 2,	desiccant solution stream state points	
HCR	heat capacity ratio	a, b,	air stream state points	
NEG	normalized entropy generation	ave	average	
		bot	bottom	
Symbols		da	dry air	
		ex	extraction point	
c_p	specific heat capacity at constant pressure $(kJ kg^{-1} K^{-1})$	f	dehumidifier	
h	specific enthalpy at a component terminal (kJ kg ⁻¹)	gen	generated	
h^*	specific enthalpy in term of dry air mass flow rate	ht	heater	
	$(kJ kg_{da}^{-1})$	hx	heat exchanger	
Ĥ	total enthalpy rate (kW)	i	inlet	
h_{fg}	latent heat of vaporization $(kJ kg^{-1})$	id	ideal	
т	slope of humidifier and dehumidifier line ($CkJ^{-1}kg_{da}$)	max	maximum	
'n	mass flow rate (kg s ^{-1})	min	minimum	
m_r	desiccant-to-air mass flow rate ratio (–)	n	condenser	
MRR	moisture removal rate $(kg s^{-1})$	0	outlet	
Q	heat input rate (kW)	opt	optimum	
RR	recovery ratio (–)	pw	freshwater	
S	specific entropy $(kJ kg^{-1} K^{-1})$	r	regenerator	
S	total entropy (kW K ⁻¹)	S	desiccant	
T	temperature (°C)	sol	solution	
c 1		st	strong concentration	
Greek		tan'	correspondent point at humidifier line to the tangent point	
	11.00		at air curve	
Δ	difference	tan	tangent point at air curve	
3	effectiveness (-)	W	weak concentration	
Ψ	entnaipy pinch (kJ kg _{da})			
Ş	desiccant solution concentration $(kg_s kg_{sol}^{-1})$			

The aforementioned studies were conducted to improve cooling/ desalination systems. Moreover, some efforts suggested an implementation of the balancing principle to improve the system performance by minimizing entropy generation. Thiel et al. [15] have studied irreversibility by drawing a clear distinction between the finite mean driving force of a transport process and its variation with the spatial distribution. Narayan et al. [16] studied the effect of thermal balancing using extraction technique on the performance of HDH desalibnation systems. Notably, the thermal balancing principle has been applied to systems that involve heat and mass exchangers. In particular, it was successfully tested to improve the performance of HDH systems via some mass extractions between the system humidifier and dehumidifier. Chehayeb et al. [17] have broadened the concept of single extraction that was proposed earlier by Narayan et al. [16] to the multiple air extractions and injections, in order to thermodynamically balance the HDH system. Miller and Lienhard [18] introduced enthalpy rates to balance the HDH system components by extracting water or air from one component and injecting into the other.

Müller–Holst [19] proposed an extraction HDH system by varying the ratio of water-to-air mass flow rate continuously, thereby decreasing the stream-to-stream temperature difference to achieve thermal balancing. Another novel approach for thermodynamic balancing was presented by Zamen et al. [20] by proposing a multi-stage HDH system. They introduced a new performance parameter, called "temperature pinch". Schlickum [21] patented a three-stage HDH system, in which the liquid stream was connected in series while the air stream was separately recirculated for each stage. Hou [22] reported a two-stage solar multi-effect HDH system. Different designs for a closedair open-water HDH system with and without extractions are investigated by Elmutasim et al. [23]. Brendel [24] invented an HDH system that is driven by forced convection. In which, water is extracted at several points from the dehumidifier and injected into the humidifier to provide thermal balancing. Thiel and Lienhard [25] have shown that it is required to consider both the concentration and temperature profiles in order to optimize heat and mass exchangers (HME). Younis et al. [26] have also studied extracting air from two points in the humidifier and injected into the dehumidifier. The enthalpy-temperature diagram is frequently used to demonstrate the impact of extraction on HDH systems [20], whereas the temperature pinch approach was used earlier [27] to evaluate a system maximum performance.

Narayan et al. [28] have investigated thermodynamic balancing in HDH system by extracting and injecting water or air from the dehumidifier into the humidifier or the other way around. Mistry et al. [29] reported that reducing entropy production results in maximizing the performance of HDH performance. Miller and Lienhard [18] investigated the impact of extraction on balancing the enthalpy profiles in HDH systems. McGovern et al. [27] reported a 300% increase in HDH performance by incorporating a single water extraction. They also found that the recovery ratio enhancement was from 7% to 11%. Analogous to temperature pinch, Narayan et al. [16] presented en-thalpy pinch approach to balance HME, wherein both temperature and concentration profiles are considered. Through experimentation, Narayan et al. [30] reported a 54% increase in the performance of an HDH system by using a single air extraction.

Noticeably, the literature has focused on HDH for carrying out the thermal balancing principle. There is no study on the effect of extraction technique in liquid desiccant cooling systems. This is because, applying extraction is not possible in the conventional liquid desiccant cooling systems due to the lack of condenser in such systems, unlike the Download English Version:

https://daneshyari.com/en/article/10148936

Download Persian Version:

https://daneshyari.com/article/10148936

Daneshyari.com