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Interfacial optimization of fiber-reinforced hydrogel composites for soft fibrous tissue applications

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ABSTRACT

Meniscal tears are the most common orthopedic injuries to the human body, yet the current treatment of choice is a partial meniscectomy, which is known to lead to joint degeneration and osteoarthritis. As a result, there is a significant clinical need to develop materials capable of restoring function to the meniscus following an injury. Fiber-reinforced hydrogel composites are particularly suited for replicating the mechanical function of native fibrous tissues due to their ability to mimic the native anisotropic property distribution present. A critical issue with these materials, however, is the potential for the fiber-matrix interfacial properties to severely limit composite performance. In this work, the interfacial properties of an ultra-high-molecular-weight polyethylene (UHMWPE) fiber-reinforced poly(vinyl alcohol) (PVA) hydrogel are studied. A novel chemical grafting technique, confirmed using X-ray photoelectron spectroscopy, is used to improve UHMWPE-PVA interfacial adhesion. Interfacial shear strength is quantified using fiber pull-out tests. Results indicate significantly improved fiber-hydrogel interfacial adhesion after chemical grafting, where chemically grafted samples have an interfacial shear strength of 256.4 ± 64.3 kPa compared to 11.5 ± 2.9 kPa for untreated samples. Additionally, scanning electron microscopy of fiber surfaces after fiber pull-out reveal cohesive failure within the hydrogel matrix for treated fiber samples, indicating that the UHMWPE-PVA interface has been successfully optimized. Lastly, inter-fiber spacing is observed to have a significant effect on interfacial adhesion. Fibers spaced further apart have significantly higher interfacial shear strengths, which is critical to consider when optimizing composite design. The results in this study are applicable in developing similar chemical grafting techniques and optimizing fiber-matrix interfacial properties for other hydrogel-based composite systems.

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50 51 1. Introduction

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Physically cross-linked poly(vinyl alcohol) (PVA) hydrogels are extremely biocompatible [1], possess viscoelastic properties similar to articular [2,3] and meniscal cartilage [4], and do not 54 55 exhibit any wear, even after millions of cycles [5]. As a result, PVA hydrogels have been investigated extensively for articular cartilage applications [2,6]. Poor properties in tension, however, limit the actual use of this material, especially for stronger fibrous tissues similar to the meniscus, ligaments and tendons. 59

One method to enhance the mechanical properties of polymer 60 61 networks is through the incorporation of various additives, such 62 as fibers [7,8] and particles [9], the latter including nanoparticles 63 such as clays [10] and nanotubes [11]. Fiber-reinforced composites 64 offer the advantage of easily imparting anisotropic properties to

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the material. More importantly, for biomedical applications, cues can be taken from nature to guide composite designs, including fiber layout and orientation, that mimic the native fiber structure of human tissue (e.g. the orientation of collagen fibers in the meniscus [12,13]).

We have previously shown that fibrous reinforcement of PVA hydrogels successfully increased the tensile modulus from 0.23 MPa without any reinforcement to 260 MPa after reinforcement with ultrahigh-molecular-weight polyethylene (UHMWPE) fibers [14], achieving a modulus range similar to that reported in the literature for the native meniscus [15]. UHMWPE fibers were chosen due to their biocompatibility, high strength, high tensile modulus and fatigue resistance [16]. These characteristics are essential in order to withstand the high stresses that occur within joints during movement [17]. The inert and hydrophobic nature of UHMWPE fibers, however, presents a challenge regarding composite processing and ultimate material properties due to poor fiber wettability and interfacial adhesion.

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83 Oxygen plasma surface modification of polyethylene fibers is a 84 common approach to increase interfacial adhesion [18-21]. 85 Furthermore, the presence of oxygen-containing functional groups 86 on fiber surfaces after plasma treatment allows for chemical 87 grafting of specific functional groups onto the fiber surfaces. We have developed a novel PVA grafting technique to increase interfa-88 89 cial adhesion at the UHMWPE-PVA interface by first activating 90 fiber surfaces with oxygen plasma and then chemically grafting PVA onto the fiber surfaces using an aldehyde linkage. PVA-grafted 91 UHMWPE fibers were then physically cross-linked into the 92 93 hydrogel network [22].

In this work, the impact of PVA fiber grafting on composite 94 interfacial properties and biocompatibility was evaluated in order 95 96 to guide future composite design parameters toward soft fibrous 97 tissue applications. Interfacial shear strength was calculated using 98 fiber pull-out tests as a quantitative measure of interfacial adhesion. Interfacial shear strength was determined with and 99 100 without PVA grafting and as a function of inter-fiber spacing. Scanning electron microscopy (SEM) was used to determine 101 the mode of failure after fiber pull-out. The biocompatibility of 102 103 PVA-grafted UHMWPE fiber mats was confirmed using a cell-based 104 in vitro cytotoxicity test.

105 2. Materials and methods

106 2.1. PVA hydrogel synthesis

PVA (>99% hydrolyzed) with a molecular weight of 89,000-107 108 98,000 g mol⁻¹ and poly(vinyl pyrrolidone) (PVP) with a molecular 109 weight of 40,000 g mol⁻¹ were obtained from Sigma Aldrich (St Louis, MO). PVP was added in small amounts to the hydrogel 110 111 formulation to improve network stability through interchain 112 hydrogen bonding [23]. Polymer solutions were prepared by mix-113 ing 20 wt.% polymer, composed of 99 wt.% PVA and 1 wt.% PVP, 114 in deionized water. The container was sealed and autoclaved at 115 121 °C for 2–4 h to ensure complete dissolution of PVA. Polymer 116 solutions were poured into individual cylindrical vials either 117 without fibers (for shear testing) or with fibers (for fiber pull-out 118 testing). Freeze-thawed samples were subjected to 21 h of freezing 119 at -20 °C and 3 h of thawing at room temperature for five cycles.

120 2.2. PVA shear strength

121PVA hydrogels were evaluated in shear, to determine the upper122limit for interfacial shear strength. Cylindrical hydrogel samples,123prepared as described previously, were ~ 12 mm in diameter124(n = 5). To prevent water evaporation prior to testing, hydrogel125samples were kept in their sealed vials until immediately before126testing. PVA samples were held in place using a two-piece plastic

in-house designed apparatus shown in Fig. 1a. Each plastic piece 127 had a 12 mm diameter indentation. The hydrogels were inserted 128 into the apparatus such that the plastic surfaces for both pieces 129 touched each other. Tensile grips were used to secure the plastic 130 surfaces in place. Testing was performed using an Instron Materials 131 Testing System Series 4442 (Norwood, MA) with a 500 N load cell 132 at a constant cross-head speed, 10 mm min⁻¹, perpendicular to the 133 hydrogel's axial axis. Testing conditions were in air at room 134 temperature and performed until failure. A free-moving metal ring 135 was placed around the two pieces to constrain movement of the 136 plastic to the testing direction. Shear strength, τ_{max} , shear, was 137 calculated as maximum load over cross-sectional hydrogel area 138 according to Eq. (1), where F_{max} is load at failure and r is hydrogel 139 radius. 140 141

$$\tau_{\max,shear} = \frac{F_{\max}}{\pi r^2} \tag{1}$$

UHMWPE fibers with a fiber diameter of $\sim 25 \ \mu m$ were obtained145from Fiber Materials, Inc. (Biddeford, ME). Fibers were obtained146under the trade name Spectra® 1000 in plain weave style 945 with147a denier of 215 and reported fiber strength and modulus of 3.25148and 113 GPa, respectively. Single UHMWPE fibers were manually149separated from fiber bundles in the weave.150

2.4. Scanning electron microscopy

Scanning electron microscopy (SEM; Model FEI/Phillips XL30)152was used to image UHMWPE fiber surfaces. Samples were carbon153coated to prevent charging. Low beam energy, 3 kV, was used to154prevent sample destruction during imaging.155

2.5. X-ray photoelectron spectroscopy

X-ray photoelectron spectroscopy (XPS) spectra were collected 157 using a Physical Electronics PHI VersaProbe 5000 with a scanning 158 monochromatic source from an Al anode. Charging of samples 159 during testing was prevented via a dual beam charge neutraliza-160 tion system. Survey XPS spectra were acquired at 100 W with the 161 following parameters: pass energy of 117.4 eV, range between 0 162 to 1000 eV, step size of 0.5 eV and dwell time of 20 ms. High 163 resolution spectra were also collected of the elemental C1s peak 164 using the high power mode at 100 W with the following parame-165 ters: pass energy of 23.5 eV, range between 278 to 298 eV, step size 166 of 0.2 eV and dwell time of 50 ms. Observed shifts due to charge 167 overcompensation were corrected by shifting the C1s peak to 168 285.0 eV. Deconvolution of the high resolution C1s peak was 169 performed using CasaXPS processing software. The binding energy 170



Fig. 1. (a) Shear testing experimental set-up. Hydrogel is shown in pink with blue arrows indicating direction of testing. Inset shows three-dimension view of sample. (b) Failure was confirmed to occur in shear. (c) Typical force vs. extension curve for PVA hydrogels loaded in shear.

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