



Calibration of the Weibull stress scale parameter, σ_u , using the Master Curve

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Abstract

This work proposes that the Weibull stress scale parameter, σ_u , increases with temperature to reflect the increasing microscale toughness of ferritic steels caused by local events that include plastic shielding of microcracks, microcrack blunting, and microcrack arrest. The Weibull modulus, m , then characterizes the temperature invariant, random distribution of microcrack sizes in the material. Direct calibration of σ_u values at temperatures over the DBT region requires extensive sets of fracture toughness values. A more practical approach developed here utilizes the so-called Master Curve standardized in ASTM Test Method E1921-02 to provide the needed temperature vs. toughness dependence for a material using a minimum number of fracture tests conducted at one temperature. The calibration procedure then selects σ_u values that force the Weibull stress model to predict the Master Curve temperature dependence of K_{Ic} values for the material. At temperatures in mid-to-upper transition, the process becomes more complex as fracture test specimens undergo gradual constraint loss and the idealized conditions of high-constraint, small-scale yielding assumed in E1921-02 gradually degenerate. The paper develops the σ_u calibration process to incorporate these effects in addition to consideration of threshold toughness effects and the testing of fracture specimens with varying crack-front lengths. Initial illustrations of the calibration process for simpler conditions, i.e. IT crack-front lengths, use the temperature dependent flow properties and a range of toughness levels for an A533B pressure vessel steel. Then using the extensive fracture toughness data sets for an A508 pressure vessel steel generated recently by Faleskog et al. [Engng. Fract. Mech., in press], the paper concludes with calibrations of both m and σ_u over the DBT region and assessments of the Master Curve calibration approach developed here.

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Nomenclature

B	thickness
B_{xT}	thickness for an xT size specimen ($B = x$ in.)
B_{1T}	thickness for an 1T size specimen ($B = 1$ in., 25.4 mm)
\mathcal{C}	material constant relating Weibull stress to J -integral
$\overline{\mathcal{C}}$	material constant relating Weibull stress to K_J
E	elastic modulus
E_T	hardening modulus
H	height of compact tension specimen
J	value of J -integral
J_{avg}	through-thickness average of J -integral
J_c	value of J -integral at cleavage fracture
$J_{c(\text{limit})}$	limiting value of J_c
K_c	microcrack toughness
K_I	mode I stress intensity factor
K_J	plane-strain conversion of J
K_{J_c}	plane-strain conversion of J_c
$K_{J_c}^{(xT)}$	plane-strain conversion of J_c for an xT size specimen
$K_{J_c}^{\text{SSY}(1T)}$	plane-strain conversion of J_c for small-scale yielding conditions at 1T thickness
$K_{J_c(\text{med})}$	median value ($P_f = 0.5$) of K_{J_c}
K_{min}	threshold or minimum fracture toughness
K_0	toughness scale parameter ($P_f = 0.632$)
$K_0^{(1T)}$	toughness scale parameter ($P_f = 0.632$) for a 1T size specimen
M	non-dimensional deformation, $M = b\sigma_0/J$
$M^{(xT)}$	non-dimensional deformation for an xT size specimen
M_{min}	non-dimensional deformation based on K_{min}
$M_{\text{min}}^{(xT)}$	non-dimensional deformation for an xT size specimen based on K_{min}
N	total number of fracture specimens in a given data set
\mathcal{L}	length-scale parameter
P_f	cumulative probability of failure
R	outer radius of boundary layer model
R_p	radius of plastic zone
θ	temperature
$\bar{\theta}$	specific test temperature
T_0	reference temperature
T_σ	magnitude of T -stress
V	volume of the fracture process zone
V_0	reference volume
\overline{V}_0	alternate reference volume
W	width of fracture specimen
Y	microcrack geometry factor
(x, y, z)	Cartesian coordinate system with origin at initial crack-front location
(u, v, w)	displacement components in (x, y, z)
a	crack length

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