



Short communication

In-situ characterization of the uncrimping process of arterial collagen fibers using two-photon confocal microscopy and digital image correlation

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ARTICLE INFO

Article history:

Accepted 12 August 2013

Keywords:

Adventitia

Digital image correlation

Two-photon excitation microscopy

Deformation

Arterial mechanics

ABSTRACT

Uncrimping of collagen fibers in the arterial wall is an integral process in regulating the macro-level mechanical response of arteries. Uncrimping of collagen fibers leads to a gradual, but significant strain-stiffening response of the artery at physiological pressures and prevents overdilatation at elevated pressures. In this study, we imaged adventitial collagen fibers from fresh primate arteries using two-photon excitation microscopy while subjecting the arteries to physiological inflation pressures and axial stretches. The imaging focal plane was fixed at a constant radial location in the adventitial wall by adjusting the focal distance as the arteries inflated, allowing for the continuous monitoring of the uncrimping process of a single region of collagen fibers. Digital image correlation was then applied to the sequential images to assess and correlate the local displacements to manual traces of selected reference fibers and their engagements. We found that the collagen fibers of interest became fully engaged at a luminal pressure of 20 mmHg, this was then followed by rotation of these fibers as the bulk artery continued to dilate. This technique helps to further the understanding of the uncrimping process of collagen fibers under physiological loads, which can aid in the development of more accurate microstructural constitutive models.

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1. Introduction

Collagen fibers (CFs) are considered the primary load-bearing constituent in the arterial wall. The high tensile strength of CFs and their abundance, particularly in the adventitia, provide structural support and prevent the overdilatation of the arterial wall at elevated blood pressures (Holzapfel et al., 2000). However, at sub-physiological pressures, CFs are undulated or crimped, and therefore present minimal resistance to loading. As the arterial wall dilates with increasing luminal pressure, the undulated CFs uncrimp and become engaged (i.e. straightened), and this process results in a significant strain-stiffening response of the wall (Cox, 1978). The uncrimping process of CFs is an integral component of the non-linear mechanical response of arteries. The kinematics of the uncrimping is complex and not well understood, and a better understanding of this process can help in the formulation of more physiologically relevant microstructurally-motivated constitutive models (Cacho et al., 2007, Gasser et al., 2012).

This study presents a proof-of-concept utilizing digital image correlation (DIC) and two-photon excitation microscopy (TPEM) techniques to characterize the uncrimping process of adventitial CFs in the cylindrical configuration of arteries subjected to physiological pressures and axial stretches. The second harmonic generation (SHG) signals of the CFs were used as natural stochastic patterns for the DIC analysis. The uncrimping process in each artery was assessed across a fixed area and radial location, thus allowing for the continuous tracking of the same group of CFs across the entire pressure-loading regime. We found that the sampled CFs became fully uncrimped and engaged prior to the onset of significant strain-stiffening in the wall. This result was in agreement with manual traces of selected individual fibers in the same region of interest. Lastly, we characterized the mean displacement directions of the CFs with loading.

2. Methods

2.1. Mechanical testing

Two common carotid arteries (one right and one left) were harvested from two healthy non-human primates (rhesus macaques) during necropsy. The ages of the

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animals and the traction-free geometries of the respective arteries are provided in Table 1.

The arteries were flushed immediately with saline and transported on iced saline to the laboratory. Adherent perivascular tissues were carefully removed by sharp dissection and the arteries were cannulated on a cylindrical biaxial mechanical testing device; similar devices are described in detail elsewhere (Gleason et al., 2004, Zaucha et al., 2009). The arteries were subjected to cyclic, quasi-static constant rate pressurizations between 0 and 120 mmHg at fixed axial lengths while their outer diameters and axial forces were recorded in-line. During testing, the arteries were continuously submerged in a Ca^{2+} and Mg^{2+} -free Dulbecco's phosphate-buffered saline (DPBS, Corning Cellgro) bath maintained at 37 °C. Axial lengths were incrementally increased and the arteries were preconditioned at each increment by several pressurization cycles to achieve repeatable pressure–diameter curves. Based on established methods, the axial lengths in which the axial forces ceased to vary with pressure was deemed to be the in-vivo axial lengths of the arteries (Van Loon, 1977). Once this configuration was established, the arteries were transferred to a secondary cylindrical biaxial device designed to fit on an inverted multi-photon confocal microscope (LSM 510 META NLO, Zeiss) for TPEM analysis of the CFs.

Table 1
Specimen age and traction-free geometries of arteries used in this study.

	Type	Age	Outer Diameter	Wall Thickness	Length
Artery 1	RCCA	7 yr	3.10 mm	0.46 mm	13.0 mm
Artery 2	LCCA	2 yr	2.74 mm	0.58 mm	19.6 mm

RCCA: Right Common Carotid Artery, LCCA: Left Common Carotid Artery

2.2. Multiphoton imaging

The arteries were axially stretched prior to imaging to their pre-determined in-vivo axial lengths and preconditioned again with several pressurization cycles to ensure repeatability. The arteries were then pressurized from 0 mmHg in a stepwise manner by 5 mmHg increments to 50 mmHg and then by 10 mmHg increments to 120 mmHg. This pressurization scheme was implemented to ensure small deformations needed to perform the DIC analysis. At each pressure increment, the arteries were excited with an 800 nm laser and the SHG signals of the CFs were collected through a 380–420 nm bandpass filter using a 20 × objective (Wan et al., 2010). Each frame was averaged 16 times to maximize the resolution. To maintain the same region of interest, the focal plane of the microscope objective was fixed at a single radial location through manual adjustments of the focal distance as the arteries inflated. CFs in the focal plane that could be uniquely tracked by visual observation throughout the entire pressurization ramp were used as references for the manual adjustments. Several areas on the arteries were sampled prior to the final imaging sequence in order to identify an appropriate set of reference CFs; the final regions of interest were located approximately in the center of the arteries at a depth of 20–30 μm into the arterial wall.

2.3. DIC analysis

DIC was performed between sequential images using a modified open source algorithm (OpenPIV) in MATLAB (Taylor et al., 2010). The algorithm was tested on a representative pair of identical SHG images of CFs in which one of the images was translated by 30 pixel at 45°. Furthermore, the percent engagement of three reference fibers in artery 1 was measured by manually tracing the fiber lengths using ImageJ (National Institute of Health), see Fig. 1A, B. The engagement percentage was defined as the percent ratio of the fiber's chord length (straight line end-to-end) to total length, thus 100% engagement denoted a fully engaged,

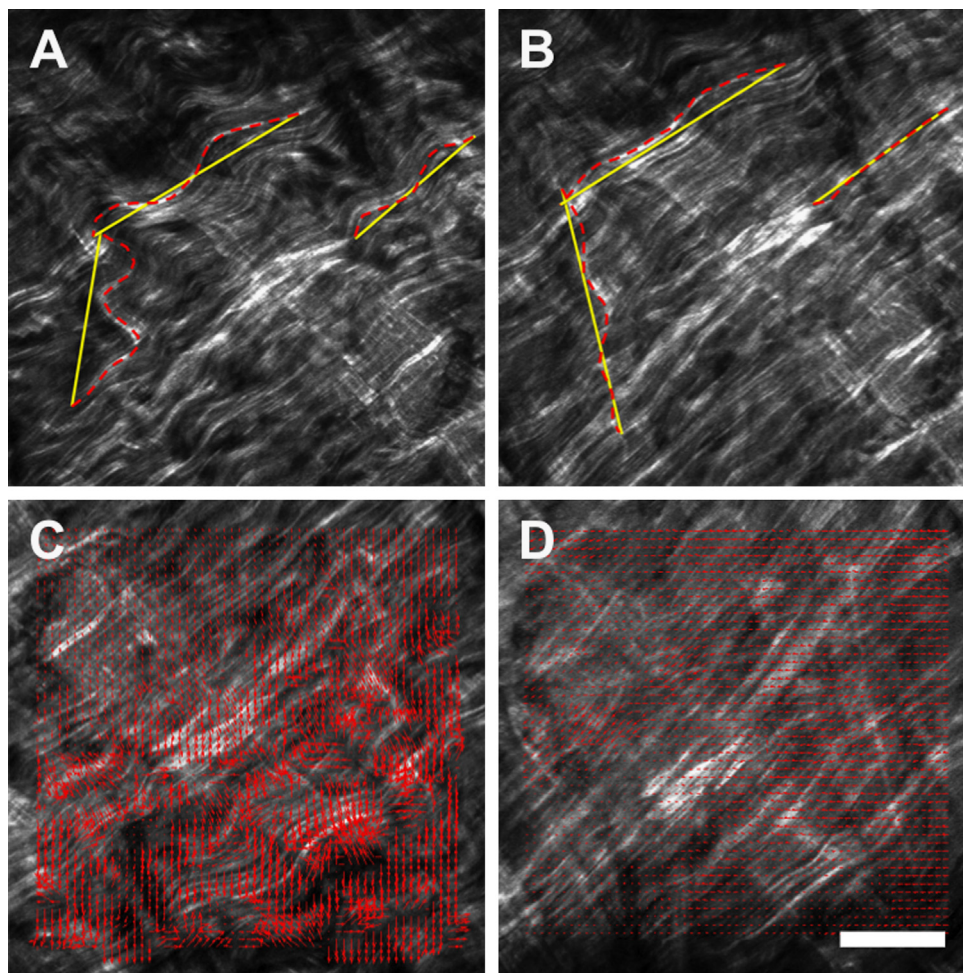


Fig. 1. Three reference fibers manually traced at low pressure (A) and high pressure (B). Dashed lines denote the total fiber lengths while solid lines are the chord lengths. The engagements of the fibers were calculated as percent ratios of these two lengths. Corresponding DIC displacement vectors for low (C) and high pressures (D). Note that the displacement magnitudes decreased significantly for the high pressure. White scale bar \approx 100 μm.

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