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Origin of mechanical strain sensitivity of pentacene thin-film transistors

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ABSTRACT

We report on bending strain-induced changes of the charge carrier mobility in pentacene organic thin-film transistors employing a combined investigation of morphological, structural, and electrical properties. The observed drain current variations are reversible if the deformation is below 2%. The morphology and structure of the active pentacene layer is investigated by scanning force microscopy and specular synchrotron X-ray diffraction, which show that bending-stress causes morphological rather than structural changes, modifying essentially the lateral spacing between individual pentacene crystallites. In addition, for deformations >2% the rupture of source and drain gold electrodes is observed. In contrast to the metal electrodes, the modification of the organic layer remains reversible for deformations up to 10%, which suggests the use of soft and flexible electrodes such as graphene or conducting polymers to be beneficial for future strain sensing devices.

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45 1. Introduction

Thin films of conjugated organic molecules are subject 46 of intense research due to their applicability in novel 47 (opto-)electronic devices, including organic thin-film tran-48 sistors (OTFTs). Pentacene (PEN) is the prototypical hole-49 conducting material with notably high charge carrier 50 51 mobilities of up to $5.5 \text{ cm}^2/\text{V} \text{ s}$ [1–3] in p-type OTFTs. One key advantage of organic electronic devices is the pos-52 sibility to produce flexible all-organic OTFTs with the func-53 tional organic semiconductor films deposited on flexible 54 plastic foils like Mylar[®] or polyethylenetherephthalate 55 (PET) as substrate [4]. Through their intrinsic flexibility, 56 57 OTFTs can be applied as mechanical strain-sensing devices [5,6] exhibiting significant advantages over conventional 58

Q2 * Corresponding authors. Tel.: +49 1786905049 (V. Scenev). *E-mail addresses*: vscenev@aol.com (V. Scenev), rabe@physik. hu-berlin.de (J.P. Rabe). types of sensors: they can be processed under ambient 59 conditions and are generally inexpensive to fabricate 60 [4–11]. For sensing strain, reversible changes in the electri-61 cal characteristics of OTFTs were employed, including 62 drain current, charge carrier mobility, threshold voltage, 63 and contact resistance for deformations up to 1-2% 64 [5,6,9,12,13]. In particular, the reported changes in mobil-65 ity were proposed to be due to morphological changes of 66 the PEN layers under mechanical strain and/or the activa-67 tion of trap states in the PEN/electrode interface region 68 [5,6,9,14,15]. However, up to now there has been no direct 69 experimental evidence to support these suggestions. In or-70 der to enable targeted research for improving current 71 OTFTs for future reliable sensing applications, further 72 experimental work is needed to complete the microscopic 73 picture of strain-impact on OTFT performance. Here we re-74 port a comprehensive electrical characterization of flexible 75 OTFT devices under applied bending-stress, relating the 76 device characteristics to morphological and structural 77

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ARTICLE IN PRESS V. Scenev et al./Organic Electronics xxx (2013) xxx-xxx

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78 properties of the active layer, as determined by a combination of scanning force microscopy (SFM) and specular X-79 ray diffraction (XRD). We identify the deterioration of the 80 81 metal electrodes to be responsible for irreversibilities in 82 the device characteristics, while the observed modifica-83 tions of the active organic layer remain reversible for 84 deformations up to 10%, which suggests using soft organic

85 electrodes for future improved sensing applications.

2. Experimental 86

OTFTs were fabricated on 200 µm thin and flexible 87 88 polyethylenetherephthalate (PET) substrates. A gold layer was vacuum-deposited on the substrates as gate electrode. 89 Polyvinylalcohol (PVA) with ammonium dichromate (AD) 90 salt (cross-linking agent) was deposited from water solu-91 tion as gate dielectric by spin-coating and subsequent 92 93 UV-curing for cross-linking. Gold source and drain electrodes (Fig. 1a) were patterned by thermal deposition 94 95 through a shadow mask. Pentacene (PEN) was used as organic semiconductor. PEN films were evaporated at a base 96 97 pressure $<10^{-7}$ mbar; the film thickness and the deposition 98 rate (0.5 nm/min) were monitored by a quartz crystal microbalance placed next to the sample; the device is 99 sketched in Fig. 1a. A special apparatus for defined bending 100 of the OTFT (Fig. 1c) was developed to be suitable for use in 101 102 both SFM and specular XRD experiments. XRD measurements were carried out at the beamline W1 at DESY-103 HASYLAB (Hamburg, Germany) with a primary beam en-104 ergy of 10.5 keV, using the bending apparatus (Fig. 1c) as 105 106 sample holder for in situ experiments, and a standard setup 107 (PVA samples fixed planar on a Si wafer) for reference measurements. The electrical and morphological charac-108 terization of the PEN layers under deformation was carried 109 out in situ under ambient conditions. For electrical charac-110 terization a Keithlev 2636A sourcemeter was used. The 111 surface topography was imaged with SFM (Nano Wizard, 112 JPK instruments). The PEN film strain was calculated with 113 the model of beam buckling (Fig. 1b), which allows to cal-114 culate the film strain, ε , directly from the bending radius 115 [16], as demonstrated before [9,17]. The bending radius 116 was calculated taking into account the homogeneous 117 bending of the PET foil. This setup allowed to strain PEN 118 films up to 10%, with the upper limit defined by the small-119 est accessible radius of curvature and the thickness of the 120 PET substrate. All electrical device characterization, XRD 121 and SFM measurements, were carried out under ambient 122 conditions. 123

3. Results

Transfer curves (i.e., drain current (I_D) versus gate volt-125 age $(V_{\rm C})$ characteristics) of the devices were recorded for 126 different degrees of strain. The bending-stress was released 127 after acquiring transfer characteristic for a particular strain 128 in order to verify the reversibility of the process (i.e., if the 129 current recovers to the initial value). We find, as expected 130 [9], a decrease in drain current as function of device defor-131 mation (Fig. 2a). For deformations of up to 1.7%, straining 132 of the device causes reversible variations of the transfer 133 curves. Starting from 1.7% I_D does not recover to the initial 134 value of the pristine device upon bending-stress relief. 135 Transfer characteristics exhibit a pronounced hysteresis 136 with the hysteresis loop-area increasing with increasing 137





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