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Numerical investigation of ultrasound reflection and backscatter measurements in cancellous bone on various receiving areas

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ABSTRACT

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In this study, new ultrasound reflection and backscatter measurements in cancellous bone using a membrane-type hydrophone are proposed. A membrane hydrophone made of a piezoelectric polymer film mounted on an annular frame allows an incident ultrasound wave to pass through its aperture because it has no backing material. Therefore, in measurements using the membrane hydrophone, the receiving area could be located independently from the transmitting area. In addition, the size and shape of the receiving area, which corresponded to those of the electrode deposited on the piezoelectric film, could be arranged in various ways. To investigate the validity of the proposed measurements, before bench-top experiments, the reflected and backscattered waves from cancellous bone were numerically simulated using a finite-difference time-domain method. The reflection and backscatter parameters in the cancellous bone were derived. The simulated results suggested that appropriate receiving areas for the reflection and backscatter measurements could exist and that the proposed measurements could be more effective for evaluating bone properties than conventional measurements.

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39 1. Introduction

40 Various ultrasound measurements in bone have been studied to establish accurate and precise quantitative ultrasound (QUS) tech-41 42 niques for clinical assessment of bone quality [1–4]. Among these, 43 ultrasound reflection and backscatter measurements in cancellous bone have been attempted [4-6] because of their easy applicability 44 to skeletal sites where through-transmission measurements are 45 46 difficult. The reflected and backscattered waves are generally 47 received using only one transducer that acts as both transmitter and receiver in pulse-echo mode. Thus, the sizes, shapes, and loca-48 tions of the transmitting and receiving areas must be the same; 49 50 however, independent arrangement of the receiving area is desir-51 able to effectively detect the wave characteristics associated with 52 the bone properties.

53 In this study, new reflection and backscatter measurements in cancellous bone are proposed in which a membrane-type hydro-54 phone is inserted between the ultrasound transmitter and the 55 56 bone. The membrane hydrophone is composed of a piezoelectric 57 polymer film and an annular frame without a backing material, 58 which allows an incident ultrasound wave to pass through its aperture [7,8]. The advantage of the technique is that when the 59 60 membrane hydrophone is used, the receiving area can be easily

0041-624X/\$ - see front matter © 2013 Elsevier B.V. All rights reserved. http://dx.doi.org/10.1016/j.ultras.2013.09.017 changed, which was the advantage in the proposed measurements. It is difficult to verify an ultrasound measurement in bone because an immense number of experiments are required owing to the variability in bone structure. Numerical simulations are helpful as a surrogate for experiments [9,10]. Thus, by using a finite-difference time-domain (FDTD) method [11–14], the reflected and backscattered waves from the cancellous bone were numerically simulated for various receiving areas. The correlations of the reflection and backscatter parameters with the structural parameters of the cancellous bone—specifically the porosity and mean intercept lengths (MILs) [15] of the trabecular elements and pore spaces—were investigated to demonstrate that the dependences of QUS parameters on bone properties can change with the receiving areas.

2. Ultrasound measurements using a membrane hydrophone

2.1. Membrane hydrophone

Piezoelectric polymer films such as poly(vinylidene fluoride) 76 are a suitable piezoelectric material for an ultrasound receiver in 77 water (namely hydrophone) because their acoustic impedances 78 are relatively close to the impedance of water. Hydrophones made 79 of piezoelectric films can be classified into two types: needle-type 80 [16] and membrane-type [7,8]. The former is composed of the pie-81 zoelectric film and a cylindrical backing material, and the latter is 82 composed of the film and an annular frame. A schematic of the 83

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84 construction of the membrane hydrophone is shown in Fig. 1. In 85 the case of the general construction in Fig. 1(a), circular and linear 86 electrodes are deposited on the piezoelectric film. The circular electrodes on either surface overlap, but the linear electrodes are 87 separated. Therefore, an incident ultrasound wave can be received 88 89 only in the circular area, which corresponds to the receiving area. In a membrane hydrophone, various receiving areas can be easily 90 91 realized by changing the overlapping area of the electrodes, as in the annular area in Fig. 1(b). Moreover, as shown in Fig. 1, no mate-92 93 rial exists on the back of the receiving area.

2.2. Measurement of reflected and backscattered waves 94

95 Fig. 2 illustrates the method of measuring the reflected and backscattered ultrasound waves from cancellous bone using the 96 97 membrane hydrophone. The hydrophone was arranged between 98 the needle-type ultrasound transmitter and the cancellous bone 99 in water. Because the acoustic impedance of the hydrophone's pie-100 zoelectric film was close to that of water, the transmitted ultrasound wave could pass through the film and arrive at the 101 cancellous bone. The reflected and backscattered waves from the 102 bone were received by the membrane hydrophone. 103

If the inner diameter of the annular frame mounting the piezo-104 105 electric film is sufficiently larger than the diameter of the ultra-



Fig. 1. Schematic construction of membrane hydrophones with (a) circular and (b) annular receiving areas.



Fig. 2. Method of measuring reflected and backscattered ultrasound waves from cancellous bone using a membrane hydrophone.

sound beam, the membrane hydrophone cannot significantly 106 disturb the ultrasound field. The half-width 2θ of the ultrasound 107 beam (wavelength: λ) transmitted from a circular flat surface 108 (diameter: $2a_t$) is approximated as 109 110

$$2\theta \approx 2 \arcsin\left(0.705 \frac{\lambda}{a_t}\right),$$
 (1) 112

and the beam diameter $2a_b$ at a distance *d* from the transmitter is 113 calculated as

$$2a_b \approx 2d \tan \theta. \tag{2}$$
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For example, for λ = 1.48 mm at a frequency of 1 MHz in water, $2a_t = 10$ mm, and d = 40 mm, the calculated $2a_b$ is approximately 17.1 mm; thus, an inner diameter of 20 mm is adequate for the annular frame. Practically, a smaller inner diameter is acceptable because a focused transmitter is generally used in QUS apparatuses for bone assessment.

3. Numerical simulations of reflection and backscatter measurements

3.1. Simulation model

Three-dimensional (3D) FDTD simulations of reflection and back-127 scatter measurements using the membrane hydrophone were per-128 formed using self-made FDTD software [14]. The simple 129 simulation model was constructed with consideration of in vitro 130 experiments, which will be performed for comparison between 131 the experimental and simulated results in the future. A cross-sec-132 tional view of the simulation model is shown in Fig. 3. This model 133 had a spatial interval of 57 µm and consisted of cancellous bone 134 and water regions, whose dimensions were $5.016 \times 6.84 \times$ 135 6.84 mm³ (88 \times 120 \times 120 points) and 7.98 \times 6.84 \times 6.84 mm³ 136 $(140 \times 120 \times 120 \text{ points})$, respectively. In Fig. 3, the x-direction cor-137 responds to the direction of ultrasound transmission, and the y-z138 plane corresponds to the cancellous bone surface. 139

The transmitting area with a rigid backing material had a circu-140 lar concave shape with a diameter of 5.7 mm (100 points), which 141 was set at the center of the y-z plane at x = 0 mm at a distance 142 of 7.98 mm (140 points) from the cancellous bone surface. The fo-143 cal distance was 10.488 mm (184 points), which corresponded to 144 the focal point 2.508 mm (44 points) inside of the cancellous bone. 145 The transmitted waveform was a single sinusoid at 1.0 MHz multi-146 plied by a Hanning window (note that the center frequency was 147 shifted to approximately 1.25 MHz owing to the window). Its time 148 interval was 4 ns. At x = 0, 1.995, 3.99, and 5.016 mm (0, 35, 70, and 149 88 points) from the transmitting area [7.98, 5.985, 3.99, and 150 2.964 mm (140, 105, 70, and 52 points) from the cancellous bone 151

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