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# Transfers from Earth to Earth–Moon L<sub>3</sub> halo orbits using accelerated manifolds

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### Abstract

This paper is concerned with two-impulse transfers from Earth to Earth–Moon  $L_3$  halo orbits. After an orbit injection maneuver from an Earth orbit, a spacecraft travels on a ballistic accelerated manifold trajectory to a position intersection with a halo orbit where an orbit injection maneuver is executed. Although many types of transfers are located, our primary concern is transfers that require either a low transfer time of flight or a small orbit injection maneuver. Several families of transfers lie along the edge of a time of flight/injection maneuver Pareto Front. These families share similar characteristics and are shown to be an extension of a transfer that utilizes a stable invariant manifold. The quickest family of transfers to  $L_3$  can be completed in 28.5–33 days with an injection maneuver of 61.75–130 m/s, with shorter duration transfers requiring a larger injection maneuver. The family of transfers with the smallest injection maneuvers given a duration limit of 140 days required 13.45 m/s.

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## 1. Introduction

The dynamics of spacecraft on libration point orbits (LPOs) and their associated invariant manifolds present many interesting opportunities for mission design. In the last four decades, missions such as ISEE-3, Herschel Space Observatory, Genesis, and ARTEMIS have traveled to and operated in LPOs about the collinear points  $L_1$  and  $L_2$  in the Earth–Moon and Sun–Earth systems. These missions have a diverse array of objectives; studying the Universe by the light of the far-infrared and submillimeter portions of the spectrum, observing and entrapping solar wind particles and returning them to Earth, and analyzing the effect of the Sun's radiation at our Moon.

points  $L_1$  and  $L_2$ . However, there has been an increased interest in orbits about Earth–Moon  $L_3$  due to their advantageous geometry. For example, many orbits at  $L_3$  have the ability to view almost 50% of the Earth's surface. It has recently been shown that a constellation of three spacecraft (two in Earth–Moon  $L_3$  LPOs and one in an  $L_1$  LPO) can provide almost complete visibility of the Earth's surface (Davis et al., 2013). This constellation could also provide continuous coverage of geosynchronous regions. Orbits at  $L_3$  are relatively stable and would likely require minimal station-keeping (Parker et al., 2014). Furthermore, satellites traveling to an  $L_3$  orbit require substantially less fuel than those traveling to geostationary orbit.

Presently, missions have only orbited the libration

In the past, invariant manifolds have been used to construct transfers from Earth to LPOs in both the Sun–Earth (SE) system, e.g., Genesis (Lo et al., 2001) and the Earth– Moon (EM) system, e.g., ARTEMIS (Broschart et al.,

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2009). There are many examples in literature of methods to build these transfer trajectories (Howell et al., 1994; Koon et al., 2000; Parker and Born, 2008).

#### 1.1. Trajectories to Sun–Earth L<sub>3</sub> orbits

Designing a trajectory to the vicinity of Sun–Earth  $L_3$  is particularly challenging since the region lies on the opposite side of the Sun as the Earth with almost the same Sun–Earth distance. One suggested transfer method is to use invariant manifold trajectories associated with  $L_3$ LPOs. However, the invariant manifolds of  $L_3$  Lyapunov orbits may take thousands of years to leave the vicinity of  $L_3$ , never closely approach Earth, and are thus impractical for mission design (Hou et al., 2008).

Another suggested approach is to utilize the unstable invariant manifolds of  $L_1$  and  $L_2$  LPOs since they travel close to Earth and to the vicinity of  $L_3$ . These transfers require over nine years of transfer time. Tantardini compared several methods for reaching  $L_3$  orbits (Tantardini, 2009). Bi-elliptic transfers, transfers using patched conics with gravity assists, and transfers utilizing low-thrust were modeled using the two-body problem. Following the work done by Hou et al., transfers using invariant manifolds associated with Lyapunov orbits about  $L_1$  and  $L_2$  were also explored (Tantardini et al., 2010).

#### 1.2. Trajectories to Earth–Moon $L_3$ orbits

Recently, Larsen et al. modeled transfers from a 300 km low Earth orbit (LEO) to the EM L<sub>3</sub> point by employing the exterior stable manifold of L<sub>3</sub> that lies in the *x*-*y* plane (Larsen et al., 2012). The transfer, optimized for minimum fuel, requires an impulsive burn to leave LEO and then performs a second impulsive maneuver to transfer onto the stable manifold. The spacecraft then travels along the exterior stable manifold and arrives at L<sub>3</sub>. The first and second  $\Delta$ Vs are 3.07 km/s and 0.41 km/s, respectively, for a total  $\Delta$ V of 3.48 km/s. The transfer time is approximately 200 days.

Haapala et al. constructed sample missions that included orbits at or near  $L_3$ , including a tour of the  $L_3$ ,  $L_4$ , and  $L_5$  libration points using resonant orbits as the transfer mechanism, and a transfer between orbits in the vicinity of  $L_2$  and  $L_3$  employing manifolds associated with an  $L_2$ vertical orbit (Haapala et al., 2013).

Davis et al. introduced the concept of the pseudo-manifold for transfers between low-Earth orbit (LEO) and  $L_3$  LPOs (Davis et al., 2013). The trajectories constructed in that study required two impulsive burns: a tangential burn executed to depart from LEO, and a halo orbit injection maneuver upon arrival. The injection maneuver was always performed in the direction of the velocity component of the halo orbit's stable eigenvector, propagated to the injection location. The total  $\Delta Vs$  for the transfers ranged between 3.14 km/s and 3.24 km/s and the time of flight (TOF) varied from 44 to 90 days. The orbit insertion maneuvers ran-

ged from 106 m/s to 200 m/s. In this study, we extend upon our previous work in order to reduce the TOF and/or the insertion maneuver by allowing the direction of  $\Delta V_2$  to vary.

#### 2. Background

The equations of motion for the Circular Restricted Three-Body Problem (CRTBP) have been used for trajectory propagation in this study. The CRTBP models the motion of a particle of negligible mass under the influence of two larger bodies, termed the primaries. Conventionally, the larger of the bodies is termed the primary and the smaller is termed the secondary. The primaries rotate in circular orbits about the system barycenter. Additionally, the reference frame rotates about the barycenter at the same rotation rate as the two primaries. The *x*-axis extends from the origin through the secondary, the *z*-axis extends in the direction of the angular momentum of the system, and the *y*-axis completes the right-hand coordinate frame.

When performing analysis in the CRTBP, it is useful to normalize the system so certain quantities are dimensionless. The system is normalized such that the sum of the masses, the distance between the primaries, and the gravitational parameter all equal one, and the orbital period is normalized to  $2\pi$ . These values are normalized by a Three-Body parameter  $\mu$ , which is defined as the ratio of the smaller primary's mass to the sum of the mass of the two primaries:

$$\mu = \frac{m_2}{m_1 + m_2},\tag{1}$$

where  $m_1$  and  $m_2$  are the masses of the primaries and  $m_1 > m_2$ . After normalizing, the locations of the primary and secondary become  $(-\mu, 0, 0)$  and  $(1 - \mu, 0, 0)$ , respectively.

The equations describing the motion of the third body may be written as:

$$\begin{aligned} \ddot{x} &= 2\dot{y} + x - (1-\mu)\frac{x+\mu}{r_1^3} - \mu\left(\frac{x-1+\mu}{r_2^3}\right) \\ \ddot{y} &= -2\dot{x} + y - (1-\mu)\frac{y}{r_1^3} - \mu\frac{y}{r_2^3} \\ \ddot{z} &= -(1-\mu)\frac{z}{r_1^3} - \mu\frac{z}{r_2^3}, \end{aligned}$$
(2)

where  $r_1$  and  $r_2$  represent the distance from the third body to the primary and secondary, respectively:

$$r_1^2 = (x + \mu)^2 + y^2 + z^2$$
(3)

$$r_2^2 = (x - 1 + \mu)^2 + y^2 + z^2.$$
(4)

The reader is directed to Szebehely (1967) for a derivation of the equations of motion. The equations derived by Szebehely differ slightly than the ones presented here, as the x-axis in Szebehely extends from the origin through the primary. The Jacobi Constant, C, is an integral of motion which emerges in this dimensionless, rotating system: Download English Version:

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