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The impact of self-stabilization on traffic stability considering the current lattice's historic flux for two-lane freeway

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HIGHLIGHTS

- A new lattice model is proposed with self-stabilization effect for two lanes.
- Linear stability condition is obtained with self-stabilization effect on two-lane highway.
- Simulation tests verify that traffic jams are suppressed efficiently with self-stabilization effect besides lane changing.

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ABSTRACT

Self-stabilization effect reflects the adaptive change of the current lattice in traffic flow. To improve traffic flow, a new self-stabilization term in this paper is inserted into lattice hydrodynamic model for two-lane freeway. It is shown that the self-stabilization effect can increase traffic stability on two lanes whether lane changing occurs or not according to linear stability analysis. In view of numerical simulation, the self-stabilization effect enhances the stability of the traffic flow in the modified lattice hydrodynamic model for two-lane freeway.

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1. Introduction

With the rapid growth of traffic flux, traffic problems are attracting more and more people's attention. In order to study traffic characteristics, many scholars set up many mathematical models [1–11]. Among them, traffic flow lattice hydrodynamic model, which firstly proposed by Nagatani [12,13], has been continuously concerned and developed in recent years. Recently, Tian et al. [14] proposed a lattice model by considering flow difference effect. Tian et al. [15] presented a lattice model with the consideration of optimal current difference effect. Gupta et al. [16,17] took into account some traffic factors such as driver's anticipation and interruption probability with passing to develop some lattice models. Ge et al. [18] adopted control method to investigate lattice model. Zhang et al. [19] further studied the lattice's self-anticipative density effect on traffic stability. Recently, Zhang [20] put forward a different lattice model with the self-stabilization effect of lattice's historical flow, which showed that the self-stabilization effect can increase the traffic stability on single lane. But above lattice models did not investigate the traffic phenomenon under lane changing. Consequently, Nagatani [21] considered lane changing behaviors to develop a two-lane lattice model. Subsequently, some factors such as driver's lane-changing aggressiveness [22], global average flux [23], average density difference [24], timid and aggressive behaviors [25] and density

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Fig. 1. The schematic model of traffic flow on a two-lane highway.

difference [26] have been investigated in lattice model under lane changing situation. However, the self-stabilization effect resulted from the current lattice's historic flux has not been taken into account in two-lane lattice models. In order to explore the influence of self-stabilization about the current lattice's historic flux on two lanes, we propose a new two-lane lattice model by considering self-stabilization effect and lane changing in the following section.

2. Modeling with the self-stabilization effect

Fig. 1 can describe the schematic diagram for two-lane highway [21]. When $\rho_{2,j-1} > \rho_{1,j}$, the lane changing rate is $\gamma \left| \rho_0^2 V'(\rho_0) \right| (\rho_{2,j-1} - \rho_{1,j})$. When $\rho_{2,j+1} < \rho_{1,j}$, the lane changing rate is $\gamma \left| \rho_0^2 V'(\rho_0) \right| (\rho_{1,j} - \rho_{2,j+1})$. Here γ means the rate constant coefficient with dimensionless. Therefore, the continuity equations [21] were written with lane changing as follows:

$$\partial_t \rho_{1,j} + \rho_0(\rho_{1,j} v_{1,j} - \rho_{1,j-1} v_{1,j-1}) = \gamma \left| \rho_0^2 V'(\rho_0) \right| (\rho_{2,j+1} - 2\rho_{1,j} + \rho_{2,j-1}) \tag{1}$$

$$\partial_t \rho_{2,j} + \rho_0(\rho_{2,j} v_{2,j} - \rho_{2,j-1} v_{2,j-1}) = \gamma \left| \rho_0^2 V'(\rho_0) \right| (\rho_{1,j+1} - 2\rho_{2,j} + \rho_{1,j-1})$$
(2)

By adding Eqs. (1) and (2), we get the following continuity equation:

$$\partial_t \rho_j + \rho_0(\rho_j v_j - \rho_{j-1} v_{j-1}) = \gamma \left| \rho_0^2 V'(\rho_0) \right| (\rho_{j+1} - 2\rho_j + \rho_{j-1})$$
(3)

Here $\rho_j = (\rho_{1,j} + \rho_{2,j})/2$ and $\rho_j v_j = (\rho_{1,j} v_{1,j} + \rho_{2,j} v_{2,j})/2$. Besides, the evolution equation was adopted [21] as below:

$$\partial_t(\rho_j v_j) = a[\rho_0 V(\rho_{j+1}) - \rho_j v_j] \tag{4}$$

where $a = 1/\tau$ shows driver's sensitivity. The optimal velocity function $V(\rho)$ is described as [21]:

$$V(\rho) = (v_{\text{max}}/2)[\tanh(1/\rho - 1/\rho_c) + \tanh(1/\rho_c)]$$
(5)

where ρ_c means the safety density. Moreover, based on the Nagatani's lattice model of two-lane traffic [21], some extended models [22–26] have been developed under different traffic factors. However, the impact of self-stabilization on traffic stability resulted from the current lattice's historic flux has not been investigated in two-lane lattice model. Accordingly, we think about the self-stabilization term into the evolution equation as below:

$$\partial_t(\rho_j v_j) = a[\rho_0 V(\rho_{j+1}) - \rho_j v_j] + \lambda a[\rho_j v_j - \rho_j (t - \tau_0) v_j (t - \tau_0)]$$
(6)

where $[\rho_j v_j - \rho_j (t - \tau_0) v_j (t - \tau_0)]$ means the self-stabilization effect resulted from flow difference with the information of current lattice's historical flow. τ_0 shows the historical time and λ represents the reaction coefficient. In virtue of eliminating the velocity in Eqs. (3) and (6), we certainly receive the density evolution as below:

$$\begin{aligned} \partial_t^2 \rho_j + a\rho_0^2 [V(\rho_{j+1}) - V(\rho_j)] &= a\gamma \left| \rho_0^2 V'(\rho_0) \right| (\rho_{j+1} - 2\rho_j + \rho_{j-1}) \\ &+ a(1-\lambda)\partial_t \rho_j + a\lambda \partial_t \rho_j (t-\tau_0) - \gamma \left| \rho_0^2 V'(\rho_0) \right| (\partial_t \rho_{j+1} - 2\partial_t \rho_j + \partial_t \rho_{j-1}) = 0 \end{aligned}$$
(7)

3. Linear stability analysis

To study the steady state of the uniform traffic flow, we assume the optimal velocity $V(\rho_0)$ corresponding to the constant density ρ_0 on two-lane highway. A small deviation y_j is inserted into the steady-state flow on site j as below:

$$\rho_j(t) = \rho_0 + y_j(t) \tag{8}$$

Through linearizing Eq. (7), we deduce

$$\begin{aligned} \partial_t^2 y_j &+ a\rho_0^2 V'(\rho_0)(y_{j+1} - y_j) - a\gamma \left| \rho_0^2 V'(\rho_0) \right| (y_{j+1} - 2y_j + y_{j-1}) \\ &+ a(1 - \lambda)\partial_t y_j - a\lambda \partial_t y_j(t - \tau_0) - \gamma \left| \rho_0^2 V'(\rho_0) \right| (\partial_t y_{j+1} - 2\partial_t y_j + \partial_t y_{j-1}) = 0 \end{aligned}$$

$$(9)$$

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