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Experimental investigation of CO tolerance in high temperature PEM fuel cells

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ABSTRACT

In the present work, the effect of operating a high temperature proton exchange membrane fuel cell (HT-PEMFC) with different reactant gases has been investigated throughout performance tests. Also, the effects of temperature on the performance of a HT-PEMFC were analyzed at varying temperatures, ranging from $140 °C$ to 200 °C. Increasing the operating temperature of the cell increases the performance of the HT-PEMFC. The optimum operating temperature was determined to be 160 $^{\circ}$ C due to the deformations occurring in the cell components at high working temperatures. To investigate the effects of CO on the performance of HT-PEMFC, the CO concentration ranged from 1 to 5 vol %. The current density at 0.6 V decreases from 0.33 A/cm² for H₂ to 0.31 A/cm² for H₂ containing 1 vol % CO, to 0.29 A/cm² for 3 vol % CO, and 0.25 A/cm² for 5 vol % CO, respectively. The experimental results show that the presence of 25 vol % $CO₂$ or N₂ has only a dilution effect and therefore, there is a minor impact on the HT-PEMFC performance. However, the addition of CO to H_2/N_2 or H_2/CO_2 mixtures increased the performance loss. After longterm performance test for 500 h, the observed voltage drop at constant current density was obtained as ~14.8% for H_2 /CO₂/CO (75/22/3) mixture. The overall results suggest that the anode side gas mixture with up to 5 vol % CO can be supplied to the HT-PEMFC stack directly from the reformer.

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Introduction

Proton exchange membrane fuel cell (PEMFC) is considered as a promising clean energy conversion technology due to the high efficiency, high power density, low $CO₂$ emissions and fast start-up. PEMFC is classified according to working temperature as low temperature and high temperature PEMFC. Typical low temperature (LT-PEMFC) PEMFC using perflourosulfonic acid membrane and the working temperature is limited up to 70–80 °C [\[1\].](#page--1-0) Operational challenges faced by LT- PEMFC include delicate water management and low tolerances to impurities. In addition, low operating temperature causes mass transfer limitations as it causes liquid water to accumulate at high current densities. Increasing the PEMFC working temperature above 100 \degree C can increase the tolerance to impurities and overcome the difficulties in water management [\[2,3\]](#page--1-0). High temperature PEMFC (HT-PEMFC) is gaining more attention of PEMFC research groups due to their ability to work without moisture, better fuel impurities tolerance, fast reaction kinetics and combined heat and power generation systems (CHP) applications $[4-6]$ $[4-6]$.

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PEMFC also need to deal with the drawbacks of the cost and durability for commercialization. Because of its very low tolerance towards impurities in the fuel, the LT-PEMFC requires pure H_2 or proper fine cleaning steps after the reformer to operate reformate gases. However, the use of LT-PEMFC is limited due to the high cost of producing high purity H_2 gas or additional purification systems added to system $[7,8]$. Today, most of the H_2 production is produced by natural gas or methane vapor reforming. The HT-PEMFC systems can be used with reformer systems due to the high CO and impurity tolerance [\[9,10\]](#page--1-0). The use of H_2 produced by inexpensive industrial processes such as the steam reforming of natural gas with steam will facilitate the commercialization of PEMFCs and make it easier for them to enter daily life [\[11\]](#page--1-0). However, as a result of steam reforming, impurities such as $CO₂$, CO, $CH₄$ and N_2 and NH_3 can be present in the produced H_2 rich reformate. Generally, steam reforming is used to produce H_2 rich reformate gas which contains $40-70\%$ H₂, 15 to 25 vol % $CO₂$ and 1 to 3 vol % CO and a small amount of H₂O vapor and N2. A typical CO content in reformate gases is mainly dependent on the type of thermochemical process, fuel, catalyst, temperature and pressure. Generally, CO content could be varied from 1 to 5% in 230–350 °C and up to 10% for H_2 production in the industry [\[12\].](#page--1-0) It is important to know the effects of these impurities on PEMFC performance for the design and production of fuel cell based power generation systems [\[13,14\].](#page--1-0)

Due to the major effect on HT-PEMFC performance at low temperatures CO is the most studied impurity in the literature [\[15](#page--1-0)–[17\].](#page--1-0) CO competes with H_2 for the adsorption regions of the Pt catalyst and blocks the catalytic active sites because Pt is more absorptive on the catalyst surface. As a result, even a very small amount of CO content may prevent H_2 from effectively reaching the Pt catalyst surface. The effect of CO poisoning on the anode side could be immensely reduced by HT-PEMFC operations because the kinetics of CO desorption from the Pt catalyst particles is favored with the increasing temperature [\[18,19\].](#page--1-0) Although HT-PEMFCs show superior CO tolerance, the combined effects of CO poisoning and hydrogen dilution could deteriorate the performance and durability of HT-PEMFCs.

Many researchers have investigated CO poisoning effect on HT-PEMFC with different working conditions. Different approaches have been applied, such as changing the parameters such as CO concentration, catalyst structure [\[20\]](#page--1-0) and oper-ating temperature [\[21\]](#page--1-0) to reduce the adverse effects of CO use on PEMFC [\[22\]](#page--1-0). Reduction of CO poisoning by increasing the working temperature is one of the most used methods among these approaches. Li et al. investigated the CO effect at a temperature range of 125-200 $^{\circ}$ C and determined that the CO tolerance increased with increasing temperature [\[23\]](#page--1-0). However, increasing the working temperature can damage the cell components because of the electrochemical potential, high water partial pressure and increased carbon corrosion. Therefore, it is necessary to determine the optimum temperature at which the highest performance can be achieved [\[24\]](#page--1-0). The effects of CO and $CO₂$ on the HT-PEMFC performance have been extensively reviewed in the literature. However, there are limited studies on the dual effect of $CO₂$ and CO on HT-PEMFC. Andreasen et al. investigated HT-PEMFC performance with CO and $CO₂$ using electrochemical impedance spectroscopy $[25]$. The HT-PEMFC performance was examined subject to some of the poisoning effects experienced when running on a reformate gas.

In this study, poisoning effects of impurities in the anode gas stream on HT-PEMFCs were investigated at various concentrations of H_2 , CO_2 , N_2 and CO. Firstly, the operating temperature at which the highest performance was achieved without damaging the cell components was determined by performing HT-PEMFC tests at the range of $140-200$ °C. Then to simulate poisoning environment, the HT-PEMFC was fed with different concentrations of CO (1-5 vol %) in H_2 gas stream in the same conditions as H_2 . Additionally, we investigated the effects of $CO₂$ and N₂ on HT-PEMFC performances. There is also a limited number of studies on the effects of the anode-side reformate gas feeding on the long-term durability of HT-PEMFC. Long term durability test of HT-PEMFC was performed with $H_2/CO_2/CO$ reformate gas mixture with 75/22/ 3 vol ratio. The results of this research in the future could be the basis for the researcher to design and control HT-PEMFC systems.

Experimental

Materials

The PBI membrane was prepared by a solution casting method according to our previous study $[26]$. N-N dimethylacetamide $(CH₃C(O)N(CH₃)₂$ DMAc), polyvinyl difluoride (PVDF) and phosphoric acid (H₃PO₄, 85 wt %) were used as received. The commercially available Gas Diffusion Layer (GDL, Freudenberg-H2315C2) was obtained from Freudenberg (Germany). The Pt supported carbon black (Pt/C, 70 wt % of Pt) catalyst was purchased from Tanaka Kikinzoku. All gases having high purity (>99.98%) were purchased from Linde. Millipore water was used wherever required. All chemicals and solvents were high-grade reagents and used without further purification.

Method

The acid doping was carried out by immersing the PBI membranes in H₃PO₄ at room temperature for at least 1 week to maintain proton conductivity. Generally, PBI polymer is a nonconductive aromatic heterocyclic polymer in pure form. When PBI is doped with H_3PO_4 , it shows high proton conductivity. The active sites in PBI imidazole rings interact with the H_3PO_4 and 2 mol of H_3PO_4 is attached per PBI unit. [Fig. 1](#page--1-0) shows the proton conduction mechanism in PBI membrane network. Generally, high H_3PO_4 doping levels increase the PBI proton conductivity but excess of H_3PO_4 in the PBI might affect the mechanical properties of the PBI membrane [\[27\]](#page--1-0). The doping level acquired by the PBI membrane was $11 H_3PO_4$ per polymer repeat unit.

For the preparation of the MEA, non-woven carbon cloth coated with a carbon microporous layer was used as the GDL. The Pt/C catalyst was used as a both anode and cathode catalyst with 1.0 mg/cm². During long-term operation of H3PO4 doped PBI membranes often lose proton conductivity

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