## **ARTICLE IN PRESS**

#### JOURNAL OF ENVIRONMENTAL SCIENCES XX (2018) XXX-XXX



Available online at www.sciencedirect.com

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# Strong enhancement of methylene blue removal from binary wastewater by in-situ ferrite process

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ABSTRACT

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#### 13 ARTICLEINFO

- 15 Article history:
- 16 Received 27 October 2017
- 17 Revised 18 January 2018
- 18 Accepted 19 January 2018
- 19 Available online xxxx
- 39 Keywords:
- 40 Dye and metal removal
- 41 Ferrite process
- 42 Multi-porous
- 43 Physisorption
- 44

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#### 59 Introduction

Every year, more than 10,000 types of commercial dyes, with production of  $7 \times 10^5$  tons, are used in various industries, including textiles, paper, plastics, and leather tanning (Natarajan et al., 2017; W. Wang et al., 2017). Approximately 15% of the produced dyes are released as wastewater (Konicki et al., 55 2017), causing serious threats to public health and the environ- 56 ment (Daneshvar et al., 2017; Srivastava and Sillanpää, 2017). 57 Moreover, hazardous heavy metals commonly coexist with dyes 58 in some effluents (Stawiński et al., 2017; Zhao et al., 2015). The 59 conventional removal techniques, such as ion-exchange and 60

Dye wastewater containing heavy metal ions is a common industrial effluent with complex 20

physicochemical properties. The treatment of metal-dye binary wastewater is difficult. In 21

this work, a novel in-situ ferrite process (IFP) was applied to treat Methylene Blue (MB)–Cu(II) 22

binary wastewater, and the operational parameters were optimized for MB removal. Results 23 showed that the optimum operating conditions were OH/M of 1.72,  $Cu^{2+}/Fe^{2+}$  ratio of 1/2.5, 24

reaction time of 90 min, aeration intensity of 320 mL/min, and reaction temperature of 25

40°C. Moreover, the presence of  $Ca^{2+}$  and  $Mg^{2+}$  moderately influenced the MB removal. 26

Physical characterization results indicated that the precipitates yielded in IFP presented 27

high surface area (232.50  $m^2/g$ ) and a multi-porous structure. Based on the Langmuir model, 28

the maximum adsorption capacity toward MB was 347.82 mg/g for the precipitates 29

produced in IFP, which outperformed most other adsorbents. Furthermore, IFP rapidly 30

sequestered MB with removal efficiency 5 to 10 times greater than that by general ferrite 31 adsorption, which suggested a strong enhancement of MB removal by IFP. The MB removal 32 process by IFP showed two different high removal stages, each with a corresponding 33 removal mechanism. In the first brief stage (<5 min), the initial high MB removal (~95%) 34 was achieved by predominantly electrostatic interactions. Then the sweep effect and 35

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#### https://doi.org/10.1016/j.jes.2018.01.019

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Please cite this article as: Hao, H., et al., Strong enhancement of methylene blue removal from binary wastewater by in-situ ferrite process, J. Environ. Sci. (2018), https://doi.org/10.1016/j.jes.2018.01.019

encapsulation were dominant in the second longer stage.

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adsorption on activated carbons, are time-consuming and
arduous, with mediocre efficiency due to the complexity of
metal-dye binary wastewater (Stawiński et al., 2017; Visa et al.,
2010). Hence, developing an efficient and cost-effective method to
treat such refractory wastewater is significant and urgent.

The ferrite process (FP) is an effective method for removing
various heavy metal ions from wastewater (Barrado et al.,
2002; Erdem and Tumen, 2004; Tu et al., 2012, 2013). In FP,
heavy metal ions can be incorporated into a spinel structure
through co-precipitation to form ferrites. The principle is
presented as shown below:

 $xM^{2+} + (3-x)Fe^{2+} + 6OH^{-} + 1/2O_2 \longrightarrow M_xFe_{(3-x)}O_4 + 3H_2O_3$ 

72 Lou and Huang (2009) indicated that sewage containing 75 metal ions treated by FP could meet effluent standards, and 76 the resulting sludge also satisfied the toxicity characteristic 77 leaching procedure (TCLP). Moreover, the ferrite precipitates 78 generated from FP can be separated easily due to its 79 magnetism (Tu et al., 2013) and can be recycled as catalysts 80 (M.-Q. Cai et al., 2017; Lou and Huang, 2009).

Furthermore, ferrites with magnetic and electrical properties 81 have attracted extensive attention due to their applications in 82 preparation of adsorbents, active catalysts, magnetic recording 83 media, suspension materials in ferromagnetic liquids, refractory 84 materials, magnetic seeds, super-hard materials and high 85 86 temperature sensors (Cai et al., 2017; Ding et al., 2013; Manna et 87 al., 2017). So far, application of magnetic ferrites to treat 88 environmental pollution has received a great deal of interest 89 (Almasian et al., 2016; Mahmoodi, 2013; Wu et al., 2016). Magnetic 90 ferrites such as copper ferrite ( $CuFe_2O_4$ ), manganese ferrite 91 (MnFe<sub>2</sub>O<sub>4</sub>) and cobalt ferrite (CoFe<sub>2</sub>O<sub>4</sub>) not only possess photocatalytic and catalytic activity (López-Ramón et al., 2017; Ren et al., 92 2015; Stoia et al., 2017), but also exhibit good adsorption efficiency 93 owing to electrostatic interaction and surface functional group 94 complexation (Wang et al., 2012, 2015; Wu et al., 2016; Yavari et 95 al., 2016; Zhao et al., 2014). In particular, some magnetic 96 ferrites synthesized by sol-gel, co-precipitation or hydrothermal 97 methods were reported to be effective in adsorbing various dyes 98 such as azo-dyes (Chen et al., 2014; Wang et al., 2012; Wu et al., 99 2004), and heterocyclic dyes (K. Cai et al., 2017; Hashemian et al., 100 2013; Iram et al., 2010). 101

Recently, it has been demonstrated that in-situ formed 102 materials, such as Mn-(hydr) oxides (in-situ MnO<sub>x</sub>) (Lu et al., 103 104 2014; Zhang et al., 2008), present a smaller particle size and 105 higher adsorption capacity than aged materials. Thus, it can be an interesting option to conduct an in-situ FP in metal-dye 106 binary wastewater, in which co-precipitation will occur be-107 tween non-ferrous metals and Fe, as well as dye adsorption by 108 the in-situ formed ferrites. However, to our knowledge, no 109 previous report exists on metal-dye binary wastewater treat-110 ment using in-situ FP. 111

In this study, an in-situ FP (IFP) was developed to treat Cu 112 (II)-Methylene Blue (MB) binary wastewater. The influence of 113 114 operational parameters and solution conditions in IFP formation on MB uptake was studied for practical applications. 115 Then, the MB removal performance was also evaluated 116 through isothermal analysis. In addition, the MB removal 117 mechanism by IFP was elucidated after detailed characteriza-118 tion using various techniques. 119

#### 1. Materials and methods

1.1. Materials

All the chemicals were purchased from Sinopharm Chemical 123 Reagent Co., Ltd. (Shanghai, China) in analytically pure grade 124 and were used without further purification. Stock solutions 125 were prepared by dissolving appropriate amounts of metal 126 salts or dye powder in deionized water. 127

**1.2. Batch experiment** 128

The experiment was performed in a series of  $30 \times 300$  mm glass 129 test tubes, in which the solution was mixed with aeration by an 130 air pump. A rubber stopper with a condensing tube and an 131 aerator pipe was used to plug each glass test tube. The reaction 132 temperature was controlled by a thermostatic water bath. After 133 transferring 80 mL of simulated dye wastewater containing Cu<sup>2+</sup> 134 to the tube, a desired amount of solid FeSO<sub>4</sub> · 7H<sub>2</sub>O was added. The 135 solution was mixed well by aeration, and then various quantities 136 of NaOH (5 mol/L) were added dropwise, upon which a fine 137 precipitate formed immediately. The precipitate was maintained 138 in suspension by continuous aeration. Blank experiments 139 without the addition of NaOH were conducted to ensure that 140 the decrease in concentration was not actually due to evapora-141 tion. Samples were withdrawn intermittently and filtered by a 142 0.45 µm membrane. The residual dye concentrations in the 143 solution were determined using a UV-visible spectrophotometer 144 (MAPADA UV-6100, Shanghai, China) at 662 nm for MB. The 145 metal concentrations were analyzed by inductively coupled 146 plasma optical atomic emission spectrometry (ICP-OES) ICPE- 147 9800 (Shimadzu, Japan). All the tests were conducted in duplicate. 148 The calculation of adsorption capacity (mg/g) is shown in Eq. (1), 149 and the removal efficiency was calculated using Eq. (2): 150

$$qt = (C_0 - C_t) \times \frac{V}{m} \tag{1}$$

$$W = \frac{C_0 - C_t}{C_0}$$
(2)

where  $C_0$  (mg/L) is the residual concentration of blank sample **153** (mg/L) and  $C_t$  (mg/L) is the residual concentration of analyte; V 155 (L) is the initial solution volume; m (g) is the total initial Cu<sup>2+</sup> and 156 Fe<sup>2+</sup> dosage. 157

The effects of OH/M,  $Cu^{2+}/Fe^{2+}$  ratio, reaction temperature, 158 aeration intensity, adsorption isotherms, and water hardness 159 on MB removal were investigated. The influence of OH/M was 160 investigated by changing the molar ratio of hydroxyl ions to 161 the combined heavy metal ( $Cu^{2+}$  and  $Fe^{2+}$ ) concentration. 162 When testing the effect of different experimental conditions, 163 only one condition was varied at a time while all other factors 164 remained constant. Unless otherwise specified, the initial MB 165 concentration and  $Cu^{2+}$  concentration of the simulated dye 166 wastewater were 50 mg/L and 0.02 mol/L, respectively. 167

#### 1.3. Characterization methods

After the formation of IFP, the precipitates were collected, 169 washed with distilled water, and then freeze-dried in vacuum 170 prior to analysis unless otherwise specified. Scanning electron 171

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