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**Research Paper** 

# Mathematical modeling and validation of a 320 MW tangentially fired boiler: A case study



APPLIED HERMAL

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#### HIGHLIGHTS

- Detailed and robust mathematical model of 1056 t/h capacity boiler is developed.
- Air pollutants prediction is captured considering equilibrium combustion.
- Rotary regenerative air heater (Ljungström) model is validated and included.
- Inlet/outlet temperature of each part of the boiler are validated with 8.72% error.
- Averaged energy distribution in the boiler are presented and analyzed.

#### ARTICLE INFO

Keywords: Mathematical modeling Boiler Equilibrium combustion Ljungström

#### ABSTRACT

The main step to evaluate the effect of various parameters on optimal operation conditions and pollution reduction of a boiler is to create a detailed model. In this paper, a steady state integrated model of boiler has been developed. Besides implementing main components of boiler applying thermodynamics laws, heat transfer and pressure drop correlations, following aspects have been considered: equilibrium combustion to predict flue gas composition and temperature, recirculation gas in the furnace, furnace exit gas temperature, radiation of the flue gases to the waterwall and superheaters, desuperheaters and rotary regenerative air heater (Ljungström). Heat transfer surfaces are considered as heat exchangers including direct and inter-tube radiation energy. The model was successfully applied to 320 MW tangentially fired boiler of Bandar Abbas power plant in Iran at six different loads 240, 250, 260, 270, 280 and 290 MW. Inlet/outlet temperature of working fluids for each heat transfer surfaces of the boiler are presented, compared and validated against the actual measured data from the power plant with maximum relative error of 8.72%. Effect of each heat transfer surfaces of boiler on its efficiency is presented and analyzed by averaged energy distribution in the boiler.

#### 1. Introduction

The energy required to generate electricity in fossil power plants is achieved by combustion of the fuel, and the operation of fossil power plants does entail the release of harmful pollutants and greenhouse gases to the environment [1]. Despite renewable energy growth, fossil fuels will remain dominant energy source for next 20 years [2], therefore improving the performance of boiler as the frontline of energy conversion can have a significant impact on reducing these noxious gases. Create a model to predict boiler behavior in a wide range of loads and assessing different scenarios is an essential step in performance optimization [3,4].

A good model should consist of various phenomena that occur in the

boiler, such as combustion in the furnace, diversity of the flue gas composition include air pollutions, hot flue gas absorptivity and emissivity, various heat transfer modes, pressure drop and phase change.

In the last decade, many researchers focused on CFD (Computational Fluid Dynamics) simulation of boiler and its components especially combustion in the furnace and heat transfer surfaces. For example, Modlinski [5] presented three dimensional numerical model of utility boiler tangentially-fired furnace retrofitted with swirl burners and showed how the flow, combustion performance and heat transfer in the furnace are affected by burners. Choi and Kim [6] used CFD codes to investigate the combustion and  $NO_x$  emissions in a 500 MW tangentially fired pulverized-coal boiler. Madejski et al. [7] developed a numerical three dimensional model of a steam superheater

https://doi.org/10.1016/j.applthermaleng.2018.09.102

Received 13 June 2018; Received in revised form 6 September 2018; Accepted 24 September 2018 Available online 29 September 2018 1359-4311/ © 2018 Elsevier Ltd. All rights reserved.

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Nomenclature		Т	temperature (°C)
		t	thickness of the fins (m); time (s)
Abbreviation		$t_B$	duration of hot-to-cold or cold-to-hot blow process
		$T_P$	transverse pitch
Α	surface area (m <sup>2</sup> )	$\Delta T$	temperature difference (°K)
$A_c$	cross-sectional area (m <sup>2</sup> )	U	overall heat transfer coefficient (W/m <sup>2</sup> °K)
$A_r$	total surface area of the regenerator matrix exposed to the	ν	velocity (m/s)
	fluid (m <sup>2</sup> )	$V_r$	volume of regenerator material (m <sup>3</sup> )
A, B	experimental coefficients	$V\bar{C}_p$	average specific heat (kJ/kg°K)
Во	Boltzman number	x	mass fraction; distance in the flow direction measured
$C, C_p$	specific heat capacity (kJ/kg°K)		from the hot inlet (m)
$C_{1,}C_{2,}C_{3}$	correction factor	$X_r$	relative position of the highest temperature zone in the
D	diameter of tubes (m)		furnace
$d_{ea}$	equivalent diameter (m)	$\Delta X$	correction factor
F	effective surface area of the waterwall (m <sup>2</sup> )	y	mole fraction
f	friction factor	5	
$F_c$	LMTD correction factor	Subscript	S
Fii	view factor from i to i		
$F_{\rm s}$	effectiveness factor based on areas	f	fluid
н	height (m)	fl	flame
h	specific enthalpy (kJ/kg): convection heat transfer coeffi-	fu	furnace
	cient (W/m <sup>2</sup> °K)	form	formation
h	convection heat transfer coefficient of flue gas side ( $W/$	σ	flue gas
ric,g	$m^{2}$ °K)	o in	inlet: inside
h	has in region heat transfer coefficient ( $W/m^{2}$ °K)	LMTD	logarithmic mean temperature difference
h.	inter-tube radiation heat transfer coefficient ( $W/m^2$ °K)	out	outlet: outside
k	thermal conductivity (W/m°K)	nrod	product
k.	fuel factor	r	regenerator
K K	aquilibrium constant	Pad	radiation
к <sub>р</sub> I	tube length (m)	react	reactant
L I	corrected fin length (m)	rof	reference
	fin length (m)	ch	reference
L <sub>fin</sub> I	lin lengui (iii)	SIL	superileater
		sta	standard
$L_r$	length of the regenerator (m)	u	
M	temperature field	W	water/steam
MM	molar mass (kg/kmol)	ww	waterwall
т	mass flow rate (kg/s)	0 11.	
n	mole	GIEEK LELLEIS	
$N_P$	number of passes		1
$N_R$	number of tube rows	α	absorptivity
$N_T$	number of tubes	ε	emissivity
Р	pressure (Pa)	$\eta_{fin}$	fin efficiency
P <sub>fin</sub>	perimeter of fins (m)	ρ	density (kg/m <sup>3</sup> )
Pr	Prandtl number	σ	Stefan-Boltzmann constant (W/m <sup>2</sup> ŰK <sup>4</sup> )
$\Delta P$	pressure drop (Pa)	$\phi$	coefficient of heat retention
Q	heat transfer rate (W)	$\psi$	thermal efficiency coefficient
Re	Reynolds number	ω	rotational speed (rpm)
S	distance between the tubes' axes (m)		

using control volume based on finite element method to determine the tube wall temperature, steam temperature and pressure distributions. Maakala et al. [8] presented a detailed, three dimensional CFD modeling of heat transfer and fluid flow in a full superheater region of recovery boiler. Xu et al. [9] developed a comprehensive CFD combustion model for large-scale supercritical circulating fluidized bed (CFB) boilers and was applied in a simulation of a 350 MW supercritical CFB boiler.

On the other hand, one dimensional mathematical modeling is an efficient and economical method to investigate and calculate the energy transfer and fluids temperature in the boiler [10,11]. Pan et al. [12] developed a mathematical model for predicting mass flux distribution and metal temperature in the vertical water wall based on the mass, momentum and energy conservation equations and validated with the power plant data. Kim et al. [13,14] developed a simplified

mathematical model of CFB boiler as a system of heat exchanger blocks under various loads. Validation has been carried out by comparing calculated results with experimental data of a pilot-scale CFB. Tzolakis et al. [15,16] carried out the one dimensional mathematical simulation of a 300 MW lignite-fired power boiler in gPROMS software. Also, the efficiency of the plant at full load was optimized, using the turbine stages' mass flow rate extractions and the fuel consumption. Chandrasekharan et al. [17] presented a review of modeling, identification and control of coal-fired boilers in a thermal power plant. They showed modeling of the plant is essential to design better power plants in response to meet the growing demand for power worldwide. A mathematical model of a plate fin and tubular cross-flow heat exchangers with application to automatic control of the liquid outlet temperature was developed and validated experimentally by Taler [18]. A dynamic mathematical model suitable for simulation of fast cut back of coal-fired Download English Version:

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