



Fig. 1. Different configurations of auxetic structures: (a) re-entrant hexagonal, (b) star, (c) double-angled, and (d) chiral.

properties [17]. A compressive test on a 3D periodic re-entrant lattice structure fabricated via electron beam melting was conducted by Li [18]. The experimental results pertaining to the mechanical properties of the structure agree well with explicit analytical predictions. A novel auxetic re-entrant hexagonal honeycomb was developed by Fu [19] by embedding the rhombic configuration to enhance the in-plane stiffness and buckling strength. Gao [10] developed theoretical formulas for the effective Young's modulus and Poisson's ratio for a three-dimensional double-angled structure utilizing the homogenization technique. The response of the cylindrical double-angled auxetic structure under low-velocity impact was investigated. The multi-objective optimization algorithm was used to acquire the optimal structure that can absorb the greatest amount of energy and retain a low peak crushing force [20]. Zhou [21] applied the double-angled NPR structure as the core of a crash box to enhance the crashworthiness. Using a numerical method, the crashworthiness performance of a crash box with an NPR core was proven to be better than that with a foam core. The double-angled NPR structure has also been applied to suspension jounce bumpers, as reported by Wang [22]. An NPR suspension jounce can improve vehicle ride comfort by reducing the maximum vertical acceleration. The static low-strain properties of metamaterials as well as the role effect of large deformations on their static properties have been studied thoroughly [34–37]. The equivalent static mechanical properties of auxetic lattices and composites with auxetic inclusions have been studied by the discrete homogenization method [38,39]. Wave propagation in auxetic structures has also been investigated [40]. Furthermore, the acoustic properties of the auxetic material can be controlled by changing the level of pre-deformation [41]. Khaled [42] extended the small strain homogenization technique to predict mechanical properties of auxetic lattice materials in the nonlinear regime. K. El Nady [43] predicted the nonlinear elastic response of auxetic structures based on micropolar continuum models. To obtain an auxetic structure with an optimal in-plane Poisson's ratio, the topology optimization method was previously utilized [44]. In another study, the effective properties of textile composites were obtained computationally by an equivalent strain energy method based on the response of the representative volume unit cell (RUC) under prescribed boundary conditions [45].

Dynamic crushing of auxetic cellular structures is also a popular topic. One-dimensional shock theory was developed by investigating the features of a crushing front through the wood under uniaxial impact [23]. Ruan [24] employed ABAQUS software to investigate the influence of cell wall thickness and impact velocity on the mode of localized deformation and plateau stress. Zhang [25] investigated the effect of cell-wall angles on the dynamic crushing behavior of a re-entrant hexagonal honeycomb. Increases of the cell angle, relative density and impact velocity were shown to enhance the energy-absorbed ability of the auxetic structure. Similar work on hexagonal cellular honeycombs has been carried out by Hu [26], who showed that a honeycomb with a cell angle of 45° performs best in absorbing energy under impact. Zou [27] discussed the dynamic crushing patterns and crushing stress of cellular structures under different impact scenarios. Three different deformation patterns

were characterized. The analytical formula for the dynamic crushing strength of regular hexagonal cellular structures was developed by Hu [28] based on the repeatable collapsing mechanism of cellular structures. The same group further established an analytical model to predict the dynamic crushing strength of hexagonal honeycombs under low-velocity impact. The analytical predictions were validated by numerical simulations [29]. The deformation patterns and dynamic crushing strength of double-angled auxetic (DAA) structures have been discussed by Qiao [30,31]. However, only two deformation modes of DAA structures compressed in the z-direction have been considered. The critical velocity that distinguishes the deformation modes has not been thoroughly discussed. In fact, if the number of cells in the x- or z-direction is not sufficiently large, the DAA structure tends to bend under low-velocity impact.

Experimental investigations have been reported in many studies. Various dynamic characteristics of open cell compliant polyurethane foam with auxetic (negative Poisson's ratio) behavior have been illustrated by F. Scarpa [46]. Qi [47] studied the ballistic resistance of sandwich panels with aluminum and auxetic honeycomb core experimentally. It is observed that the auxetic honeycomb core performs better on the ballistic resistance. 2D/3D re-entrant honeycomb lattices under quasi-static loading and dynamic are investigated compression using Split Hopkinson Pressure Bar [48]. Auxetic cellular structures build from inverted tetrapods were experimentally tested at high strain rate compression loading. It shows that shock deformation mode can enhance the stiffness in comparison to the quasi-static response [49].

This paper discusses the dynamic patterns and crushing strength of DAA structures compressed in the x-direction to fill the abovementioned research gap. Other special deformation patterns of DAA structures are also investigated utilizing one-dimensional shock theory and numerical methods.

2. Numerical simulation

Numerical simulations of the dynamic crushing of DAA structures are conducted with the commercial software Ls-Dyna. The DAA structure features two rigid walls at the bottom and top (Fig. 2). The bottom wall is fixed, and the top wall impacts the DAA structure with an initial impact velocity. The mass of the top wall is set to 2000 kg, which guarantees that the velocity remains nearly constant during crushing. Belytschko-Tsay four-node shell continuum elements with five integration points through the elements' thickness are adopted. The “automatic single surface” and “automatic surface to surface” contact modes are employed to simulate the contact of DAA structures in the crushing period. The “automatic node to surface” mode is utilized to model the contact between the rigid wall and the DAA structure. The dynamic and static coefficients of friction are set to 0.3 and 0.2, respectively [32]. These values can effectively prevent the interpenetration of the FE model.

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