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## Cell transport and suspension in high conductivity electrothermal flow with negative dielectrophoresis by immersed boundary-lattice Boltzmann method



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#### ABSTRACT

The cell transport and suspension using AC electrokinetics is essential for cell patterning and other biomedical applications in microfluidics. To avoid the undue cellular stress and irreversible damage to cells caused by low conductivity media, direct manipulations of cells in physiological solution of high electrical conductivity without dilution becomes significant. The driving mechanism of alternating current electrothermal (ACET) flow makes it attractive for pumping the physiological conductivity solution and transporting cells through the electrohydrodynamic (EHD) force. In addition, negative dielectrophoresis (nDEP) force is induced on a cell when its electrical conductivity is lower than that of solution media. In this paper, the effectiveness of ACET flow and negative DEP force in high conductivity solution is novelly used simultaneously to achieve a successful long-range cell transport and suspension in the microfluidic chamber. An immersed boundary-lattice Boltzmann method (IB-LBM) is developed to investigate the cell transport and suspension mechanism with respect to AC voltage magnitude, electrical conductivities of cell and solution, cell initial position, and cell size. It is found that a sufficient DEP force is indispensable for stabilizing the cell transport process and anchoring cells by overcoming the cell-cell interaction. Based on this, the design of a lab-on-a-chip device to generate a large DEP force is essential for future research to realize an efficient AC electrokinetic-based cell transport and suspension in physiological fluids.

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#### 1. Introduction

Microfluidics has been developed as an innovative technology for several biomedical applications such as cell manipulation, bacteria trapping, drug delivery, analyte mixing, protein immunoassay and so on due to the progress of microfabrication techniques [1]. Due to the requirement of a fast, precise, and low-damaged technique to manipulate or separate cells for the organ regeneration in the tissue engineering, several technologies have been developed by researches in this field during recent years. AC electrokinetics which include dielectrophoresis (DEP), AC electroosmosis (ACEO), and AC electrothermal (ACET) is one of the efficient approaches used in several biomedical devices for manipulating the bioparticles and fluid flow [2]. The DEP phenomenon refers to the motion of an electrically polarizable particle under the

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https://doi.org/10.1016/j.ijheatmasstransfer.2018.09.062 0017-9310/© 2018 Elsevier Ltd. All rights reserved. existence of non-uniform AC electric field, and it has been used to control different bioparticles such as cells, bacteria, and DNA molecules [3]. When AC voltage with frequency ranging from 100 Hz to 100 kHz is applied in an aqueous solution, due to the interaction between the tangential electric field and the induced charges in the electrical double layer (EDL), the fluid flow is activated termed as the ACEO flow [4]. However, when the electrical conductivity of aqueous solution (above 0.002 S/m) or the AC voltage frequency (above 100 kHz) is high, the ACEO flow is negligible due to the compression of EDL. Under this situation, the ACET flow which is caused by the gradients of permittivity and conductivity through local heating becomes dominant, and it serves as an efficient technique for pumping high conductivity solutions in microfluidic chambers [5]. Dielectrophoresis-based cell manipulation or patterning which aims at the capability of locating the cells on a desired location using DEP force has been developed as an important tool in the cellular microenvironment [6,7]. Ho et al. designed the concentric-ring array electrodes combined with stellate tips which could enhance the spatial electric field gradient

### Nomenclature

Α	cell surface area	Vc	characteristic AC voltage applied on the electrodes
$A^*$	dimensionless cell surface area	V <sub>rms</sub>	root mean square value of AC electric potential
С	lattice speed	$V_{rms}^*$	dimensionless root mean square value of AC electric
$C_s$	sound speed	TINS	potential
$D_x$	horizontal distance between cells	<b>X</b> (s)	vector of location on the Lagrangian grids
$D_x$ $D_y$	vertical distance between cells	$X_{c}$	location vector of the cell center
$d_h$	function defined in Eq. (26)	$X_c^*$	dimensionless location vector of the cell
	distance between the centers of i <sup>th</sup> cell and i <sup>th</sup> cell	$X_{i}$	location vector of the i <sup>th</sup> cell center
$d_{i,j}$	distance between the centers of i <sup>th</sup> cell and j <sup>th</sup> cell distance between the centers of i <sup>th</sup> cell and imaginary		location vector of the j <sup>th</sup> cell center
$d_i^{\prime}$		Xj	
F	cell	X <sub>i</sub>	location vector of the nearest imaginary cell center on
E <sub>rms</sub>	root mean square of AC electric field		the wall
$E_{rms}^{*}$	dimensionless root mean square of AC electric field	$X_w$	location vector of points at the cell surface
$\boldsymbol{e}_i$	discrete lattice velocity in directioni	$X_w^*$	dimensionless location vector of points at the cell sur-
F <sub>b</sub>	fluid-cell interactive momentum force		face
F <sup>*</sup> <sub>b</sub>	dimensionless fluid-cell interactive momentum force	x	vector of location on the Cartesian grids
<b>F</b> <sub>DEP</sub>	dielectrophoresis force	x	coordinate in horizontal direction
$F_{DEP}^*$	dimensionless dielectrophoresis force	<i>x</i> *	dimensionless coordinate in horizontal direction
$F_e$	AC electrothermal force	y	coordinate in vertical direction
$F_e^*$	dimensionless AC electrothermal force	y*	dimensionless coordinate in vertical direction
$\vec{F_s}$	'momentum force' on the Lagrangian grids	y	uniclisioness coordinate in vertical uncetion
$F_i$	discrete body force in directioni	C 1	
$F_{i,j}^p$	repulsive force between cells	Greek sy	
- 1.j W	-	ho	criterion parameter used in the repulsive force
$F_i^W$	repulsive force between cell and wall	$ ho_e$	charge density
$F_i$ f $\tilde{f}_{CM}$	total repulsive force	$ ho_f$	solution density
f	body force	$\rho_p$	cell density
Ĩ	Clausius-Mossotti factor	$\dot{\rho_r}$	density ratio between cell and solution
f:	density distribution function in direction <i>i</i>	μ	dynamic viscosity
$f_i \\ f_i^{eq}$	equilibrium distribution function of density in directioni	$\sigma_{f}$	electrical conductivity of solution
<b>g</b>	gravitational acceleration	$\sigma_{fr}$	reference electrical conductivity of solution at $T_r$
<b>L</b> <sub>c</sub>	characteristic length	$\sigma_p$	electrical conductivity of cell
		ε <sub>f</sub>	electrical permittivity of solution
$I_f$ $I_p$	parameter defined as $I_f = 0.5 \rho_f \pi R_p^4$ mass momentum inertia of cell $I_p = 0.5 \rho_p \pi R_p^4$	E <sub>fr</sub>	reference electrical permittivity of solution at $T_r$
		$\tilde{\tilde{\epsilon}}_{f}$	complex permittivity of solution
JH	Joule heating term	$\varepsilon_p$	electrical permittivity of cell
k	thermal conductivity $P^2$	$\tilde{\epsilon}_p$	complex permittivity of cell
$M_f$	mass of solution with the cell size volume $M_f = \rho_f \pi R_p^2$		parameter used in the repulsive force between cells
$M_p$	mass of 2D circular cell $M_p = \rho_p \pi R_p^2$	$\epsilon_p \ \epsilon_p'$	parameter used in the repulsive force between cells
Ν	number of cells		
n	normal direction of boundary surfaces	$\epsilon_W$	parameter used in the repulsive force between cell and wall
р	pressure	2	
$p^*$	dimensionless pressure	$\epsilon_W$	parameter used in the repulsive force between cell and
Re	Reynolds number defined as $Re = \frac{\rho_f U_c L_c}{\mu}$		wall
$Re(\tilde{f}_{CM})$	real part of Clausius-Mossotti factor	α	parameter defined as $\alpha = \frac{\delta_{\sigma}}{\delta_{\varepsilon}}$
$R_p$	cell radius	$\delta_h$	Dirac's delta unction
$R_{pi}$	i <sup>th</sup> cell radius	$\delta_s$	arch length of the segment on the Lagrangian grids
$\dot{R_{pj}}$	j <sup>th</sup> cell radius	$\delta_{\chi}$	lattice space
$ \vec{r} $	distance between the Cartesian grid and Lagrangian grid	$\delta_{\sigma}$	parameter defined as $\delta_{\sigma} = \frac{1}{\sigma_f} \frac{d\sigma_f}{dT}$
S	Lagrangian coordinate	$\delta_{arepsilon}$	parameter defined as $\delta_{\varepsilon} = \frac{1}{\varepsilon_f} \frac{d\varepsilon_f}{dT}$
Т	temperature		thermal expansion coefficient of fluid
$T^*$	dimensionless temperature	$eta_T \Delta T$	characteristic temperature defined as $\Delta T = \frac{\sigma_{fr}V_c^2}{k}$
T <sub>r</sub>	reference room temperature $T_r = 298K$		
t	time	$\Delta t$	time step
t*	dimensionless time	$\Delta x$	lattice space in x direction
U <sub>c</sub>	characteristic velocity defined as $U_{-} = \sqrt{\frac{\xi_{\rm fr}\delta_{\sigma}\Delta T V_{\rm c}^2}{2}}$	$\Delta y$	lattice space in <i>y</i> direction
$U_p$	characteristic velocity defined as $U_c = \sqrt{\frac{\epsilon_{fr}\delta_\sigma \Delta T V_c^2}{\rho_f L_c^2}}$ cell translational velocity vector	τ	the charge relaxation time of AC signal
Ср П*	dimensionless cell translational velocity vector	$ au_f$	dimensionless relaxation time of density
$U_p^*$	5	ω	AC voltage frequency
$\boldsymbol{U}^{d}$	desired velocity on the Lagrangian grids	$\omega_i$	weight coefficient in direction <i>i</i>
$\boldsymbol{U}^t$	temporary velocity vector on the Lagrangian grids	$\Omega_s$	cell surface curve
u	velocity vector	$\Omega_p$	cell angular velocity
<b>u</b> *	dimensionless velocity vector	$\Omega_p^*$	dimensionless cell angular velocity
u <sup>t</sup>	temporary velocity on the Cartesian grids		

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