

Available online at www.sciencedirect.com





Mathematics and Computers in Simulation 81 (2011) 2001-2017

www.elsevier.com/locate/matcom

Finite volume approximation of a diffusion–dissolution model and application to nuclear waste storage $\stackrel{\text{tr}}{\approx}$

O. Angelini^{a,b,*}, C. Chavant^a, E. Chénier^b, R. Eymard^b, S. Granet^a

^a Laboratoire de Mécanique des Structures Industrielles Durables, UMR EDF/CNRS 2832, France
 ^b Université Paris-Est, 5 bd Descartes, 77454 Marne-la-Vallée, France
 Received 17 November 2009; received in revised form 11 June 2010; accepted 8 December 2010

Available online 11 January 2011

Abstract

The study of two phase flow in porous media under high capillary pressures, in the case where one phase is incompressible and the other phase is gaseous, shows complex phenomena. We present in this paper a numerical approximation method, based on a two pressures formulation in the case where both phases are miscible, which is shown to also handle the limit case of immiscible phases. The space discretization is performed using a finite volume method, which can handle general grids. The efficiency of the formulation is shown on three numerical examples related to underground waste disposal situations. © 2010 IMACS. Published by Elsevier B.V. All rights reserved.

Keywords: Two phase Darcy flow in porous media; Finite volume method; Nuclear waste storage

1. Introduction

A large community of scientists is concerned with understanding the mechanical and hydraulic behaviour of deep repository radioactive waste, in reason of its large impact on environment and human safety. This implies to be able to model and simulate complex phenomena such as the de-saturation and re-saturation of geological media, gas production induced by the corrosion of steel containers, within complex 3D heterogeneous and anisotropic domains including singular zones such as galleries and cells intersections. Moreover, materials with highly contrasted physical properties are involved in long time phenomena (from thousand to millions of years).

Hence the simulation of these physical features happens to be a complex task, and their validation is a major concern for the safety improvement of the industrial devices. Computational benchmarks, such as the Couplex Gaz benchmark [18], are useful for the definition of relevant physical models and numerical methods. Indeed, the Couplex Gaz benchmark has shown that the Darcy flow of two immiscible phases, the first one being an incompressible liquid phase and the second one the gaseous phase, can lead, in presence of high capillary pressures, to unphysical situations and to drastic numerical difficulties. This model implies the displacement of a free boundary between zones where the

 $[\]stackrel{\scriptscriptstyle{\,\,\mathrm{tr}}}{\to}$ This work has been supported by GDR MOMAS.

^{*} Corresponding author at: Laboratoire de Mécanique des Structures Industrielles Durables, UMR EDF/CNRS 2832, France. Tel.: +33 147651617; fax: +33 147654118.

E-mail addresses: ophelie-externe.angelini@edf.fr (O. Angelini), clement.chavant@edf.fr (C. Chavant), eric.chenier@univ-mlv.fr (E. Chénier), robert.eymard@univ-mlv.fr (R. Eymard), sylvie.granet@edf.fr (S. Granet).

Nomenclature	
\mathcal{E}_{K}	Set of all faces of control volume <i>K</i>
\mathcal{M}	Mesh
\mathbf{F}_{p}	Mass flux for phase $p = l, g$
g	Gravity acceleration
\mathbf{J}_{n}^{c}	Mass diffusive flux for component $c = h$, w in phase p
k	Absolute permeability
$\mathcal{C}(P)$	Capacity function
μ_p	Viscosity of phase $p = l, g$
$\mathbf{n}_{K,\sigma}$	Unit vector normal to σ outward to K
ϕ	Porosity
$ ho_p$	Density of phase $p = l, g$
σ	Face of a control volume
\mathbf{x}_{σ}	Barycentre of face σ
\mathbf{x}_K	Centre of control volume <i>K</i>
C_p	Molar concentration of phase $p = l, g$
C_p^c	Molar concentration of the component $c = h$, w in phase $p = l$, g
D_p^c	Diffusion coefficient of component $c = h$, w in phase $p = l$, g
$d_{K,\sigma}$	Orthogonal distance between point \mathbf{x}_K and face σ
$D_{l,K,\sigma}^{n}$	Approximation of diffusion flux of component h in phase l outward to K at face σ
$F_{K,\sigma}$	Approximation of normal gradient outward to K integrated over face σ
$F_{p,K,\sigma}^c$	Approximation of Darcy flux of component $c = h$, w in phase $p = l$, g outward to K at face σ
8	Subscript for gaseous phase
H	Henry's law constant at the temperature of the domain
h	Superscript for gaseous component
K	Control volume, element of \mathcal{M}
K_{σ}	Cone with vertex \mathbf{x}_K and basis σ
k_{rp}	Relative permeability of phase $p = l, g$
	Control volume, element of \mathcal{M}
l	Subscript for liquid phase
m MC	Parameter of van Genuchten-Mualem law
M	Molar mass of component $c = h, w$
m_p^*	Volumic mass of component $c = n$, with phase $p = l$, g
n D	
P _C D	Capillary pressure \mathbf{P} rescure of phase $\mathbf{n} = l_{-} a$
I p D	Pressure of pildse $p - l$, g
I _r D	Ideal gas constant
л S	Seturation of phase $n - l_{a}$
S_p	Saturation of phase $p = i$, g
S_{gr}	Parameter of Van Genuchten-Mualem law
$\frac{S_{lr}}{T}$	
1 11)	Superscript for water component
X^c	Molar fraction of component $c = h$, w in phase $n = l$, g
p	

two fluid phases are simultaneously present (called in this paper the "under-saturated" zone) and zones where the only present fluid phase is the liquid phase (called in this paper the "saturated" zone). In an unexpected way, it can lead to the existence of zones where the liquid phase has been removed because of capillary forces and cannot be instantaneously replaced by the gaseous phase, hence creating a vacuum volume. It is interesting to exhibit the origin of such behaviour

Download English Version:

https://daneshyari.com/en/article/1140539

Download Persian Version:

https://daneshyari.com/article/1140539

Daneshyari.com