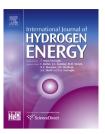


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# Hydrogen non-premixed combustion in enclosure with one vent and sustained release: Numerical experiments



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#### ABSTRACT

Numerical experiments are performed to understand different regimes of hydrogen nonpremixed combustion in an enclosure with passive ventilation through one horizontal or vertical vent located at the top of a wall. The Reynolds averaged Navier-Stokes (RANS) computational fluid dynamics (CFD) model with a reduced chemical reaction mechanism is described in detail. The model is based on the renormalization group (RNG) k- $\epsilon$  turbulence model, the eddy dissipation concept (EDC) model for simulation of combustion coupled with the 18-step reduced chemical mechanism (8 species), and the in-situ adaptive tabulation (ISAT) algorithm that accelerates the reacting flow calculations by two to three orders of magnitude. The analysis of temperature and species (hydroxyl, hydrogen, oxygen, water) concentrations in time, as well as the velocity through the vent, shed a light on regimes and dynamics of indoor hydrogen fires. A well-ventilated fire is simulated in the enclosure at a lower release flow rate and complete combustion of hydrogen within the enclosure. Fire becomes under-ventilated at higher release flow rates with two different modes observed. The first mode is the external flame stabilised at the enclosure vent at moderate release rates, and the second mode is the self-extinction of combustion inside and outside the enclosure at higher hydrogen release rates. The simulations demonstrated a complex reacting flow dynamics in the enclosure that leads to formation of the external flame or the self-extinction. The air intake into the enclosure at later stages of the process through the whole vent area is a characteristic feature of the self-extinction regime. This air intake is due to faster cooling of hot combustion products by sustained colder hydrogen leak compared to the generation of hot products by the ceasing chemical reactions inside the enclosure and hydrogen supply. In general, an increase of hydrogen sustained release flow rate will change fire regime from the well-ventilated combustion within the enclosure, through the external flame stabilised at the vent, and finally to the self-extinction of combustion throughout the domain.

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Nomenclature		β	coefficient of expansion, –
Α	vent area, m <sup>2</sup>	$\beta_r$	temperature exponent, –
$A_r$	pre-exponent, consistent units	Γ	net effect of third bodies on the reaction rate
a	speed of sound, m/s	γ	specific heat ratio, –
	molar concentration of species $j$ in reaction $r$ ,	$\gamma_{i,r}$	third-body efficiency of specie $j$ in reaction $r$ , –
$C_{j,r}$	kmol/m <sup>3</sup>	$\delta_{ij}$	Kronecker symbol
С	specific heat, J/kg-K	$\varepsilon$	energy dissipation rate, m <sup>2</sup> /s <sup>3</sup>
D	molecular diffusivity, m <sup>2</sup> /s, diameter, m	λ	thermal conductivity, W/m/K
E	total energy, J/kg	$\mu$	dynamic viscosity, Pa s
E <sub>r</sub>	activation energy, J/kmol	υ	kinematic viscosity, m²/s
L <sub>r</sub> Н	vent height, m	$\nu'_{m,r}$	stoichiometric coefficient for reactant m in
h	enthalpy, J/kg		reaction r, –
	generation of kinetic energy due to mean velocity	$\nu_{m,r}^{\prime\prime}$	stoichiometric coefficient for product m in
$G_k$	gradients, kg/ms <sup>-3</sup>		reaction r, –
C	generation of kinetic energy due to buoyancy, kg/	ξ	length fraction of turbulent structures, –
$G_b$	ms <sup>-3</sup>	$\rho$	density, kg/m³
0	gravity acceleration, m/s <sup>2</sup>	τ	time scale, s
g K <sub>r</sub>	equilibrium constant for the reaction r, –	ω	component of the flow velocity parallel to the
k	turbulent kinetic energy, m <sup>2</sup> /s <sup>2</sup> ; thermal		gravitational vector, m/s
K	conductivity, W/m/K	Subscripts	
h	forward rate constant for reaction r, consistent	atm	atmospheric
k <sub>f,r</sub>	units	E	
h.	backward rate constant for reaction <i>r</i> , consistent	eff	energy effective
k <sub>b,r</sub>	units	i,j,k	spatial coordinate indexes
M	Mach number, –	ı,,,k m	index of chemical species
N	number of chemical species in the system, –		pressure
Pr	Prandtl number, –	p t	turbulent
	pressure, Pa	r	reaction index
p R <sub>m</sub>	source term, kg/m³/s	,	reaction muex
***	rate of species <i>m</i> production/destruction in	Bars	
$R_{m,r}$	reaction <i>r</i> , consistent units	_	Reynolds averaged parameters, –
Sc	Schmidt number, –	~	Favre averaged parameters, –
S	source term, –	*	fine scale quantities, –
$S_m$	entropy, –	^	Arrhenius reaction, –
	rate-of-strain tensor, s <sup>-1</sup>	Constants and model parameters	
S <sub>ij</sub> T	temperature, K	$C_{1e}$	nts and model parameters 1.42
t	time, s	$C_{1arepsilon}$	1.68
	velocity components, m/s	$C_{2e}$ $C_{3e}$	tanh $ \omega/u $
u <sub>i,j,k</sub>	spatial coordinates, m	$C_{3arepsilon}$	0.0845
$X_{i,j,k}$ Y	mass fraction, –		volume fraction constant $C_{\xi} = 2.1277$
•	mass macuon,	$C_{\xi}$	time-scale constant $C_{\tau} = 0.4082$
Greek		$C_{\tau}$	
α	inverse effective Prandtl number	R	universal gas constant

### Introduction

Unscheduled release of hydrogen followed by a jet fire in an enclosure with one vent is a possible incident/accident scenario for hydrogen and fuel cell systems and infrastructure. To the best authors' knowledge there are no experimental or numerical studies on indoor hydrogen fires published up to date. There are publications on under-ventilated compartment fires with "regular" combustion materials. For example, Sugawa et al. [1] investigated behaviour of a methyl alcohol pool fire, including so-called ghosting flames, in a poorly ventilated compartment of size  $W \times L \times H = 2 \times 3 \times 0.6$  m. Bertin et al. [2] performed experiments with wall fires

simulated by porous vertical burner fed with propane in a semi-confined room to understand temperature distribution, chemical composition of products and radiation from ghosting flames in vitiated atmosphere. Utiskul et al. [3] studied heptane pool fires behaviour in a compartment under limited ventilation, and observed three distinct regimes of indoor combustion: extinction, blow off (separation of fire from the pan with fuel) and ghosting flames, and sustained steady oscillations. In two last regimes burning was observed at the vent area too. Under-ventilated enclosure fires of natural gas and other combustibles without extinction were carried out by Lock et al. [4] to measure room temperature, heat fluxes, and composition of combustion products depending on fuel type and ventilation rate. Coppalle et al. [5]

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