

Available online at www.sciencedirect.com

SciVerse ScienceDirect

journal homepage: www.elsevier.com/locate/he



Numerical predictions of design and operating parameters of reformer on the fuel conversion and CO production for the steam reforming of methanol

Shiang-Wuu Perng^a, Rong-Fang Horng^{a,*}, Hui-Wen Ku^b

^a Department of Mechanical Engineering, Kun Shan University, No. 949, Da Wan Rd., Yung-Kang District, Tainan 710, Taiwan ^b Department of Systems and Naval Mechatronic Engineering, National Cheng Kung University, Tainan, Taiwan

ARTICLE INFO

Article history: Received 12 September 2012 Received in revised form 20 October 2012 Accepted 21 October 2012 Available online 17 November 2012

Keywords: Methanol reforming Reaction chamber Catalyst bed Carbon monoxide concentration

ABSTRACT

SIMPLE-C algorithm and Arrhenius form of reaction model were employed to simulate the three-dimensional laminar flow field and the chemical reaction in a cylindrical methanol reformer under steam reforming. The effects of geometrical and thermo-fluid parameters on the CO and CO₂ productions as well as the heat and mass transfer in a cylindrical methanol reformer with a constant-volume catalyst bed will be observed in the present study. Low CO concentration in hydrogen-rich gas denotes a low load of CO removal in purifying processes. The results indicate that the smaller diameter-to-length ratio of chamber with a thicker catalyst bed enhances the methanol conversion and reduces the overall CO concentration in the cylindrical methanol reformer. This is because that a lower temperature distribution restrains the reverse water–gas-shift reaction to reduce the production of CO with a thicker catalyst bed.

Copyright © 2012, Hydrogen Energy Publications, LLC. Published by Elsevier Ltd. All rights reserved.

1. Introduction

Owing to the high energy efficiency and low operating temperature, a proton exchange membrane fuel cell (PEMFC) has been regarded as a promising candidate of the power sources in the future. Applying PEMFC to the power sources needs enough hydrogen fuel. Accordingly, the hydrogen production is a major topic for PEMFC. Methanol clearly has obvious benefits as a fuel for hydrogen production by reforming because it has a higher hydrogen-to-carbon ratio, lower reforming temperature and greater environmental friendliness [1]. However, PEMFC performance would become worse as the carbon monoxide (CO) concentration gets up to 5–10 ppm [2]. In order to prevent the CO poisoning in a fuel cell system, controlling the CO concentration is an important issue.

Several published literature [3-8] focused on the experiments about the CO poisoning in the PEMFC. Various experimental methods of reducing the CO concentration have been utilized to improve the CO tolerance of a PEMFC system. Waszczuk et al. [3] performed electrochemical measurements to study adsorption and desorption of methanol-derived surface CO on fuel cell grade platinum and platinum-ruthenium alloy nanoparticle catalysts. Takeda et al. [4] investigated experimentally the chemical reaction rates of reforming and CO oxidation in a methanol reforming system, and then obtained the dynamic changes in CO concentration from the reformer. Abdollahi et al. [5] observed that the Pd membrane reactor system is capable of attaining almost complete CO conversion and full hydrogen recovery at realistic experimental conditions through the water-gas-shift (WGS) reaction. Chein et al. [6] observed experimentally that

^{*} Corresponding author. Tel.: +886 62050496; fax: +886 6 2050509. E-mail address: hong.rf@msa.hinet.net (R.-F. Horng).

^{0360-3199/\$ —} see front matter Copyright © 2012, Hydrogen Energy Publications, LLC. Published by Elsevier Ltd. All rights reserved. http://dx.doi.org/10.1016/j.ijhydene.2012.10.070

| Nomenclature | R _{i,r} Arrhenius reaction mole rate of creation and |
|---|---|
| c_i concentration of species i, mol m ⁻³ C_P specific heat at constant pressure, kJ kg ⁻¹ K ⁻¹ Dflow channel diameter of reformer chamber, m D_{eff} effective diffusivity, m ² s ⁻¹ D_k mass diffusion coefficient, m ² s ⁻¹ D_P diameter of the catalyst particles, m E_a activation energy, kJ mol ⁻¹ h_i^0 enthalpy of species i, kJ mol ⁻¹ k_1 pre-exponential factor for steam reforming k_2 pre-exponential factor for water-gas shift k_3 pre-exponential factor for water-gas shift K_{eff} effective thermal conductivity, W m ⁻¹ K ⁻¹ | $\begin{array}{rl} \mbox{destruction of species i in the reaction r,} \\ \mbox{mol } m^{-3} s^{-1} \\ \hline R_{SR} & \mbox{Arrhenius reaction mole rate for the steam} \\ \mbox{reforming reaction, mol } m^{-3} s^{-1} \\ \hline R_{rWGS} & \mbox{Arrhenius reaction mole rate for reverse} \\ \mbox{water-gas-shift reaction, mol } m^{-3} s^{-1} \\ \hline S_t & \mbox{energy source term for chemical reaction} \\ \hline T & \mbox{temperature, } ^C \\ \hline T_0 & \mbox{inlet fuel temperature, } ^C \\ \hline T_W & \mbox{wall temperature, } ^C \\ \hline \vec{u} & \mbox{velocity vector, m } s^{-1} \\ \hline u_r, u_{\theta}, u_z & \mbox{velocity components in the } r, \theta \mbox{ and } z \mbox{ directions,} \\ \hline respectively, m s^{-1} \\ \hline \end{array}$ |
| reaction | Greek symbols |
| K_f thermal conductivity of fluid, W m ⁻¹ K ⁻¹ K_S thermal conductivity of solid, W m ⁻¹ K ⁻¹ Lflow channel length of reformer chamber, m L_C distance between inlet and catalyst bed, m L_{CB} catalyst bed thickness, m M_i mole fraction of species i $M_{w,i}$ molecular weight of species i, kg mol ⁻¹ Nnumber of species in the chemical reactionppressure, N m ⁻² r, θ, z coordinates, mNunitized are constant L m cl ⁻¹ K ⁻¹ | $ \begin{array}{lll} \beta & \mbox{inertial loss coefficient} \\ \epsilon & \mbox{porosity of the catalyst bed} \\ \kappa & \mbox{permeability of the catalyst bed} \\ \mu & \mbox{dynamic viscosity, kg m^{-1} s^{-1}} \\ \mu_{mix} & \mbox{viscosity of the gas mixture, kg m^{-1} s^{-1}} \\ \phi_{ij} & \mbox{a term used in calculating the viscosity of the gas} \\ & \mbox{mixture} \\ \rho_{f} & \mbox{fluid density, kg m^{-3}} \\ \tau & \mbox{tortuosity of the catalyst bed} \\ \end{array} $ |
| K universal gas constant, j mor K | in inlet |

the CO methanation, CO_2 methanation, and reversed watergas-shift reactions took place simultaneously with a higher reaction temperature. Besides, an increase in the H_2 consumption causes a decrease in the CO conversion. Fukahori et al. [7,8] applied a papermaking approach to create the pore paper-structured catalysts (so-called catalyst paper). Methanol steam reforming was performed over pieces of catalyst paper to produce hydrogen for fuel cell applications. Their results displayed that higher heat conductivity leads to a lower CO concentration.

In the past decade, for saving the experimental cost, many researches and engineering applications utilized extensively numerical simulations to investigate the CO poisoning in the fuel cell. Hao et al. [9] performed a numerical analysis of a micro methanol steam reformer with eight non-parallel channels. Their results indicated that the catalyst thickness can affect CO concentration in the product gases indirectly. Yan et al. [10] investigated numerically the effects of CO and CO2 poisoning on the degradation of PEM fuel cell performance. The results showed that, the performance drop was only 18% as the CO concentration is 50 ppm. Consequently, CO₂ poisoning became much more significantly when the CO content in the reactant gas was small. Suh et al. [11,12] investigated mass and heat transport phenomena in a methanol reformer by using a cylindrical mathematical modeling of a packed bed reactor. Their results presented that the CO concentration increases by the internally heated reformer. Jang et al. [13] built a three-dimensional numerical model to predict the effects of channel patterns and the inlet and outlet manifold configuration with a fixed inlet flow rate on a reformer in a PEMFC system. The numerical results presented that a CO mole fraction can be reduced through the preferential oxidation reaction effectively. Wang and Wang [14] utilized FLUENT to investigate the influences of pressure, temperature, oxygen-to-carbon molar ratio, and steam-tocarbon molar ratio on the auto-thermal reforming of methanol. Chein et al. [15] performed a numerical analysis of a micro-scale cylindrical packed bed reformer. In the lowtemperature zone of the reformer, the forward water-gasshift reaction was clearly demonstrated to decrease the CO concentration selectivity. On the basis of the above reasons, it is important to develop a suitable numerical model of the methanol reformer for investigating the mass and heat transport phenomena and the control of CO concentration.

Although many papers have focused on developing a numerical model of the cylindrical methanol steam reformer, few reports on the CO and CO₂ productions with various thermo-fluid parameters and diameter-to-length ratios applied to the reaction chamber in the reformer. Moreover, our previous studies [16–18] developed the numerical program to simulate the heat and mass transport in the fuel channel of a PEMFC for obtaining the cell performance enhancement. A good agreement between numerical and experimental results is presented in the results of our studies, so the numerical program is proved to deal properly with the physical problem which involves the continuity, momentum, energy and species equations with chemical reaction in a PEMFC system.

In general, SIMPLE-C method [19] integrating with the preconditioned conjugate gradient method [20,21] costs less computer storage and CPU computation time than the Download English Version:

https://daneshyari.com/en/article/1282050

Download Persian Version:

https://daneshyari.com/article/1282050

Daneshyari.com