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Experimental advances and preliminary mathematical modeling of the Swiss-roll mixed-reactant direct borohydride fuel cell



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mixed-feed mist convective direction

HIGHLIGHTS

G R A P H I C A L A B S T R A C T

- Engineering advancements presented for the Swiss-roll mixed reactant borohydride—oxygen alkaline fuel cell.
- \bullet High power density (2500 W $m^{-2})$ and excellent durability demonstrated with Pt–Ag anode–cathode catalyst combination.
- The role of porous diaphragm separator and fluid distributor metallic mesh pore size is demonstrated.
- First preliminary mathematical model of the mixed reactant borohydride—oxygen fuel cell.

A R T I C L E I N F O

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The Swiss-roll single-cell mixed reactant (SR-MRFC) borohydride – oxygen fuel cell equipped with Pt/ carbon cloth 3D anode and either MnO₂ or Ag gas-diffusion cathodes is investigated by a combination of experimental studies and preliminary mathematical modeling of the polarization curve. We investigate the effects of four variables: cathode side metallic mesh fluid distributor, separator type (Nafion 112[®] vs. Viledon[®]), cathode catalyst (MnO₂ vs. Ag), and the hydrophilic pore volume fraction of the gas-diffusion cathode. Using a two-phase feed of alkaline borohydride solution (1 M NaBH₄ – 2 M NaOH) and O₂ gas in an SR-MRFC equipped with Pt/C 3D anode, MnO₂ gas diffusion cathode, Viledon[®] porous diaphragm, expanded mesh cathode-side fluid distributor, the maximum superficial power density is 2230 W m⁻² at 323 K and 105 kPa(abs). The latter superficial power density is almost 3.5 times higher than our previously reported superficial power density for the same catalyst combinations. Furthermore, with a Pt anode and Ag cathode catalyst combination, a superficial power density of 2500 W m⁻² is achieved with superior performance durability compared to the MnO₂ cathode. The fuel cell results are substantiated by impedance spectroscopy analysis and preliminary mathematical model predictions based on mixed potential theory.

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1. Introduction

The conventional design of proton exchange membrane (PEM) fuel cell stacks is based on a plate-and-frame in series architecture that evolved from Volta's original concept of the zinc-air battery stack. The performance, durability and cost of the various

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Nomenclature

а	electrode specific surface area (m ² m ⁻³)
$C_{\rm BH^-}^{\rm inlet}$	inlet concentration of sodium borohydride (mol m^{-3})
Cair	inlet concentration of oxygen in air (mol m^{-3})
C_{0_2}	$\frac{1}{2} = \frac{1}{2} = \frac{1}$
$C_{O_2}^{\text{inter}}$	inlet concentration of oxygen in O_2 (mol m ⁻³)
C_{NaOH}^{inlet}	inlet concentration of NaOH (mol m^{-3})
Ci	concentration of component i (mol m ⁻³)
	BH ₄ diffusion coefficient ($m^2 s^{-1}$)
Deff	effective BH ⁻ diffusion coefficient $(m^2 s^{-1})$
$\mathcal{L}_{BH_4^-}$	standard notantial of POP at 200 K (V \sim)
^L BOR 298 H	(Standard potential of DOR at 298 K (V _{SHE})
^E ORR 298 I	^K standard potential of BOR at 298 K (V _{SHE})
E_a	anode potential (V _{SHE})
E_a^{OCP}	anode open circuit potential (V _{MMO or SHE})
E_a^e	equilibrium potential of BOR (V _{SHE})
E _c	cathode potential (V _{SHE})
ECCP	cathode open circuit potential ($V_{MMO or SHF}$)
Fe	equilibrium potential of ORR (Vsue)
E_{C}	cell voltage at current density of $i(V)$
V Cell (J)	local mass transfer coefficient of anode (m s ^{-1})
к _а и	(113)
K _C	giodal cathode mass transfer coefficient (m s)
$K_{m,i}$	mass transfer coefficient of component i (m s ⁻¹)
P_{O_2}	partial pressure of oxygen in feed (kPa(abs))
R _{contact}	electronic plus contact resistance (Ohm m ²)
$d_{\rm cloth}$	carbon cloth fiber diameter (m)
1 _{BOR}	current density of BOR on MnO_2 (A m ⁻²)
	current density of BOR on Pt (A m^{-2})
jbok _{Pt}	limiting current density of ORR in anode (A m^{-2})
$J_{L_{0_2}}$	limiting current density of okk in anouc $(A \text{ m}^{-2})$
$J_{L_{air}}$	$\frac{1}{1000} \frac{1}{1000} \frac{1}{1000} \frac{1}{1000} \frac{1}{1000} \frac{1}{1000} \frac{1}{1000} \frac{1}{10000} \frac{1}{10000} \frac{1}{10000} \frac{1}{100000} \frac{1}{10000000000000000000000000000000000$
$J_{ORR_{MnO_2}}$	current density of OKK on $MinO_2$ (A m ⁻²)
$j_{\rm ORR_{Pt}}$	current density of ORR on Pt (A m^{-2})
$j_{o, BOR_{MnO_2}}$	apparent exchange current density of BOR on MnO ₂
2	$(A m^{-2})$
Jo BORDE	apparent exchange current density of BOR on Pt (A m
•••,=••••	-2)
10 OPP.	apparent exchange current density of ORR on MnO ₂
JU, OKKMn02	$(A m^{-2})$
i ann	apparent exchange current density of ORR on Pt (A m
Jo,ORR _{Pt}	-2
) 1 inviting a sum of 1 and 1 is a factor of 1 and 1 is $(A = -2)$
JL,i	limiting current density of component I (A m ⁻²)
J _{L,i}	limiting current density of component i (A m ⁻²)
j_{L,BH_4}	local limiting current density of BH_4^- (A m ⁻²)
j_L^a	effective BH ₄ ⁻ mass transfer limiting current density in
	3D anode (A m^{-2})
i ^c	limiting current density of O_2 cathode (A m ⁻²)
j_ j_	ionic current density $(A m^{-2})$
je i	net current density (A m^{-2})
jnet i	electronic current density (A m^{-2})
Js	number of electron transformed in BOD reaction (9)
n _{BOR}	indifiber of electron transferred in box reaction (8)
n _{ORR}	number of electron transferred in ORR reaction (4)
n_{rds}^{a}	number of electron transferred in rate determining
	step of BOR
n_{rds}^c	number of electron transferred in rate determining
145	step of ORR
ť	electro-active thickness of 3D electrode (m)
F	Faradic constant (96.485 C mol ^{-1})
- P	oxidant pressure (kPa(abs))
r R	Universal gas constant ($9.214 \text{ J} \text{ mol}^{-1} V^{-1}$)
к т	Universal gas constant (0.514 J III01 \mathbb{N})
1	temperature (K) $(A = -2)$
J	current density (A m ⁻²)
t	time (s)

ΔV	potential drop in the anolyte under mass transfer
٨٢	CONTROL standard entropy change of BOP $(I K^{-1} mol^{-1})$
ΔS_{BOR}	standard entropy change of OPR ($I K^{-1} mol^{-1}$)
	standard entropy enables of order (V)
$\Delta \varphi_{R_{\text{contact}}}$	
$\Delta \phi_{\rm ACL}$	ionic Onmic voltage drop across ACL (V)
$\Delta \phi_{\text{GDE}}^{\text{IOIIIC}}$	ionic Ohmic voltage drop across GDE (V)
$\Delta \phi_{ m Ohm}$	total Ohmic voltage drop (V)
$\Delta \phi_{\text{sep}}$	Ohmic drop over separator (V)
$\alpha_{BOR}^{MnO_2}$	charge transfer coefficient of BOR on MnO ₂
α_{BOR}^{Pt}	charge transfer coefficient of BOR on Pt
$\alpha^{MnO_2}_{OBB}$	charge transfer coefficient of ORR MnO ₂
α ^{Pt}	charge transfer coefficient of ORR on Pt
^α ORR δ _{ACL}	carbon cloth thickness (m)
δCDE	gas diffusion electrode thickness (m)
δsen	separator thickness (m)
EACI.	ACL (carbon cloth) porosity
^E GDE	GDE porosity
2 Еd	diaphragm porosity
к ^{298 К}	effective ionic conductivity of electrolyte at 298 K
···e	(mho m^{-1})
к ³²³ К	effective ionic conductivity of electrolyte at 323 K
L	$(mho m^{-1})$
κ_{ρ}^{T}	effective ionic conductivity of electrolyte at
c	temperature T (mho m^{-1})
K _{eff}	effective electrolyte conductivity (mho m ⁻¹)
KACL	effective electrolyte conductivity in ACL
KGDE	effective ionic conductivity of GDE (mho m^{-1})
sep	effective ionic conductivity of separator (mbo m^{-1})
λeff	volume fraction of liquid in fact
v	scan rate (V s ⁻¹)
τ	hydrophilic pore fraction of ϵ_{CDE}
ω	liquid volumetric flow rate $(m^3 s^{-1})$
Abbrevic	itions
3D	3-dimensional
ACL	anode catalyst layer
BOR	borohydride oxidation reaction
CE	counter electrode
CV	cyclic voltammetry
DBFC	direct borohydride fuel cell
EIS	electrochemical impedance spectroscopy
GDE	gas diffusion electrode
MMO	mercury/mercury oxide
MRFC	mixed-reactant fuel cell
OCP	open circuit potential
OCV	open circuit voltage
ORR	oxygen reduction reaction

- PEM proton/polymer exchange membrane
- RE reference electrode
- RHE reversible hydrogen electrode
- SEM scanning electron microscopy
- SHE standard hydrogen electrode
- SR-MRFC Swiss-roll mixed-reactant fuel cell
- SS stainless steel
- WE working electrode

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