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Melanoidin removal in multi-oxidant supplemented microwave system: Optimization of operating conditions using response surface methodology and cost estimation



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ARTICLE INFO	A B S T R A C T
Keywords: Melanoidin removal Microwave coupled system Response surface methodology Multi-oxidant system	Melanoidin removal in a microwave (MW) coupled with persulfate (PS) and/or hydrogen peroxide (H ₂ O ₂) system was investigated. As a precursor, batch-mode MW-PS experiment was conducted at 250 mg/L of melanoidin concentration. The removal was observed to be 100% in 20 min of MW irradiation at PS dose of 2500 mg/L and it was found that the rate constant increased with PS dosage. On the other hand, the MW-H ₂ O ₂ process has shown 31% removal at 6000 mg/L H ₂ O ₂ dosage in 20 min. A central composite design (CCD) was used to identify the interaction between melanoidin concentration (500–10000 mg/L), pH (2–12), H ₂ O ₂ (0–6000 mg/L) and PS (0–5000 mg/L) dosages on melanoidin removal in MW system. The basic condition (pH > 7) has shown higher melanoidin removal in the presence of H ₂ O ₂ /PS; however, proportionate decrease in removal was observed with increase in melanoidin concentration. The addition of H ₂ O ₂ and PS has amplified the removal of colour induced by melanoidin, which was modeled by quadratic (R ² -0.87) and cubic (R ² -0.98) regression models. A set of validation experiments were carried out under model predicted optimum conditions. The experimental observations were in good correlation with the cubic model predicted values. Alcohol scavenging experiment shows that both sulfate and hydroxyl radical are responsible for melanoidin removal. The generation of hydroxyl radicals was estimated. A simple first-order kinetic equation-based model was developed to calculate the cost per kg of melanoidin removal in MW-PS/H ₂ O ₂ system. Overall, MW-PS/H ₂ O ₂ system seems to be a better alternative for high-rate melanoidin removal.

1. Introduction

The treatment of wastewater from agro-based industries like distillery, winery, and brewery has become a serious challenge at present due to the high organic content and the presence of recalcitrant and refractory compounds like melanoidin, phenolics, etc. Melanoidins are dark brown coloured, high molecular weight polymers formed as the end-products of Maillard reaction. They have antioxidant, anti-hypertensive, and antimicrobial activities [1]. Maillard reaction occurs when a carbohydrate reacts with an amino acid or an amine at a temperature higher than 40 °C. Therefore, these melanoidins are common constituents in the wastewater of agro-based industries that process organic food materials at high temperatures. Due to the presence of melanoidins as high as 2–20 g/L, biological treatment is not feasible for wastewater from such industries. Aerobic and anaerobic treatment systems can easily remove sugars, volatile organics and other easily biodegradable compounds that constitute COD and BOD but the colour and COD constituted by melanoidin remain unchanged after treatment. Biological treatment systems could remove only 6–7% of melanoidin and therefore, reverse osmosis and/or advanced oxidation processes (AOPs) have been used to concentrate or degrade melanoidins [2–4].

Microwave (MW) technology has been used for various applications including preparation of catalysts [5–7], sludge management [8,9], biogas production [10], heating and enhancement of different catalytic oxidation and reduction processes [11,12]. MW systems are coupled with other AOPs and oxidants such as persulfate (PS) and hydrogen peroxide (H₂O₂) for the treatment of wastewaters containing various organic pollutants. [13–21]. MW creates hotspots and favors free radical generation, which in turn reduces the activation energy [22]. The mechanism of sulphate radicals (SO₄ \bullet^-) and hydroxyl radicals (OH \bullet) reaction under MW irradiation is explained based on Eqs. (1–9). Under acidic conditions, the addition of PS to MW system accelerates the generation of SO₄ \bullet^- as shown in Eq. (1). Subsequently, the generated SO₄ \bullet^- can lead to the formation of OH \bullet (Eqs. 3,4). Similarly, the

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presence of H₂O₂ under MW environment can generate OH[•] and superoxide ion $(O_2^{\bullet^-})$ (Eq. 9) whereas under combined PS/H₂O₂, peroxymonosulfate (HSO₅⁻) can be generated as shown in Eq. 12 [23,24]. The efficiency of HSO₅⁻ is higher compared to PS, which can result in enhancement of pollutant removal [19,23]. On the other hand, the presence of HSO_5^- , $SO_4^{\bullet-}$, OH^{\bullet} and $O_2^{\bullet-}$ could accelerate the rate of pollutant removal and better mineralization of the organics. However, high concentration of radicals may result in self-quenching effect (Eq. 2,10) and in turn could reduce the rate of oxidation [25-27]. The generation of radical has been quantified in the past with alcohol quenching experiments [27,26]. In addition, the removal rate also depends on the nature of pollutant, type of bonding between molecules and structure of the target compound.

$$MW Heat + S_2 O_8^2 \rightarrow 2SO_4^{-} \tag{1}$$

$$SO_4^{\bullet-} + SO_4^{\bullet-} \rightarrow S_2 O_8^{2^-} (k = 4 \text{ to } 8.1 * 10^8 L \text{ mol}^{-1} \text{s}^{-1})$$
 (2)

$$SO_4^{\bullet-} + H_2O \rightarrow SO_4^2 + OH^{\bullet} + H^+ (k = 6 \times 10^1 L \, mol^{-1}s^{-1})$$
 (3)

$$SO_4^{\bullet-} + OH^- \rightarrow SO_4^{2^-} + OH^{\bullet} (k = 4.6 \text{ to } 8.3 \times 10^7 L \text{ mol}^{-1} \text{s}^{-1})$$
 (4)

$$OH^{\bullet} + H_2O_2 \rightarrow HO_2^{\bullet} + H_2O \ (k = 2.7 \times 10^7 L \ mol^{-1}s^{-1})$$
 (5)

$$OH^{\bullet} + OH^{-} \to H_2O + O^{\bullet-}(k = 1.3 \times 10^{10} L \ mol^{-1}s^{-1})$$
 (6)

 $OH^{\bullet} + SO_4^{2^-}/HSO_4^{-} \rightarrow SO_4^{\bullet-} + OH^{-}/H_2O \ (k = 3.5 \times 10^5 L \ mol^{-1}s^{-1})$

$$S_2 O_8^{2^-} + 2e^- \rightarrow 2SO_4^{2^-}(E0 = 2.01 V)$$
 (8)

MW Heat + $3H_2O_2 \rightarrow 2OH^{\bullet} + 2H_2O_2 \rightarrow 2O_2^{\bullet-} + 2H^+$ + $2H_2O$ (k = 1.2 to 6.5 × 10^7L mol⁻¹s⁻¹) (9)

$$SO_4^{\bullet-} + S_2 O_8^{2-} \to SO_4^{2-} + S_2 O_8^{\bullet-} (k = 5.5 \times 10^5 L \, mol^{-1} s^{-1})$$
(10)

$$MW Heat + S_2 O_8^{2^-} + H^+ \to HS_2 O_8^- \to SO_4^{2^-} + SO_4^{\bullet} + H^+$$
(11)

$$MW Heat + SO_4^{\bullet} + OH^{\bullet} \to HSO_5^{-}$$
(12)

$$MW Heat + Pollutant + HSO_5^-/SO_4^{-}/OH^{\bullet}/O_2^- \rightarrow Intermediate \ products + CO_2 + H_2O$$
(13)

able of p in coupled MW-multi-oxidant system has not been investigated in detail. Moreover, the interactions of oxidant dosage with pH and initial melanoidin concentration are difficult to be predicted in traditional experimental design under MW-multi-oxidant systems. Central composite design (CCD) is an effective tool used for design of experiment, optimization of system parameters, analysis of variance and error analysis. Therefore, this investigation is focused to study the (a) melanoidin removal between MW-PS, MW-H₂O₂ and MW-PS/ H₂O₂ systems, (b) melanoidin removal rate constants under different systems, (c) interaction between initial melanoidin concentration, pH and oxidant dosage by CCD, (d) generation of free radical species with alcohol scavenging experiments, and (e) cost for melanoidin removal in the MW-multi-oxidant system.".

2. Materials and methods

2.1. Chemicals

The

[28-30]

Sodium persulfate (98% w/w) and hydrogen peroxide (30% w/w) were purchased from AVRA Chemicals, India and Fischer Scientific,

India, respectively. Premium grade ethanol (EtOH) and analytical grade tert-butanol (TBA, 99% purity) was purchased from Hayman, UK, and Merck, India, respectively. Analytical grade Dimethyl sulfoxide (DMSO) and 2,4-Dinitrophenylhydrazine (DNPH) were purchased from Cisco research laboratory ltd., India. Acetonitrile (HPLC grade) was purchased from Rankem, India. Dextrose, glycine, NaOH, and H₂SO₄ used for the experiments were procured from Merck, India. Distilled water (DW) was used for all experimental purpose.

2.2. Preparation of melanoidin solution

A stock melanoidin solution of 210 \pm 20 g/L (COD ~ 240 \pm 10 g/ L) was prepared by mixing dextrose (1 M), glycine (1 M) and sodium carbonate (0.5 M). Subsequently, the solution pH was adjusted to 7 by adding 1 N H₂SO₄, stirred for 30 min and incubated in a hot air oven at 95°C for 7 h. The dark brown solution obtained was cooled and stored at 4°C in the refrigerator.

2.3. MW reactor set-up

(7)

A customized MW reactor, as used previously [14], of frequency 2450 MHz and capable of operating at 1000 W with an inbuilt magnetic stirrer and temperature sensor was used for the experimental work (Ragatech Pvt. Ltd., India). A reaction vessel of 1 L volume was used and 500 W power and 80 °C was maintained throughout the experiment. The MW reactor was operated in batch mode with 100 mL working volume. A counterflow heat-exchanging condenser was housed to collect the vapour which was circulated back into the reaction vessel to maintain a constant working volume.

2.4. Experimental techniques

2.4.1. Melanoidin removal batch experiments

In order to evaluate the effect of pH, dosage and irradiation time on melanoidin removal, MW- batch experiments were conducted with 250 mg/L of melanoidin and under different combinations of pH (2-12), PS dosage (100-5000 mg/L) and H₂O₂ dosage (100-6000 mg/ L). The experiments were conducted for 20 min and the samples were withdrawn from the reactor at various time intervals to determine melanoidin removal. The batch study was divided into three phases: 1) MW-PS, 2) MW-H₂O₂ and 3) MW-PS/H₂O₂. The effect of PS and/or H₂O₂ dose, MW irradiation time and pH on melanoidin removal observed in these experiments are used to evaluate boundary condition for CCD experiments with MW-PS/H₂O₂ system.

Alcohol quenching experiment was conducted for melanoidin degradation with MW-PS/H₂O₂ process in presence of scavenging agent to stop radical generation during the reaction. The scavengers used were TBA and EtOH for quenching OH^{\bullet} and SO_4^{\bullet} , respectively. The concentration of each scavenging agent added during the experiment was 0.4 M to compare effect of scavengers on melanoidin removal. The OH was estimated by trapping with DMSO and converting into formaldehyde by adding DNPH. The DNPH-HCHO concentration was detected and calibrated in HPLC (Dionex, USA) fitted with C18 silicabased reverse phase column and UV-vis detector. The mobile phase was acetonitrile: water (60:40) with a flow rate of 1 mL/min. The retention time of DNPH and DNPH-HCHO derivatives were found at 4.8 and 7.4 min, respectively. For HPLC analysis, 2.5 mL of sample was added to 2.5 mL of 25 mM phosphate buffer and 0.2 mL of DNPH. Subsequently, the sample was mixed well and kept for 30 min in room temperature. Finally, the resultant mixture was diluted 20 times and injected into HPLC for analysis.

2.4.2. Experimental design for melanoidin removal

The response surface methodology was used to optimise experimental parameters of MW-PS/H2O2 system for better melanoidin removal at different initial concentrations. A 2⁴ full factorial design with Download English Version:

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