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# Melanoidin removal in multi-oxidant supplemented microwave system: Optimization of operating conditions using response surface methodology and cost estimation



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## **1. Introduction**

The treatment of wastewater from agro-based industries like distillery, winery, and brewery has become a serious challenge at present due to the high organic content and the presence of recalcitrant and refractory compounds like melanoidin, phenolics, etc. Melanoidins are dark brown coloured, high molecular weight polymers formed as the end-products of Maillard reaction. They have antioxidant, anti-hypertensive, and antimicrobial activities [\[1\]](#page--1-0). Maillard reaction occurs when a carbohydrate reacts with an amino acid or an amine at a temperature higher than 40 °C. Therefore, these melanoidins are common constituents in the wastewater of agro-based industries that process organic food materials at high temperatures. Due to the presence of melanoidins as high as 2–20 g/L, biological treatment is not feasible for wastewater from such industries. Aerobic and anaerobic treatment systems can easily remove sugars, volatile organics and other easily biodegradable compounds that constitute COD and BOD but the colour

and COD constituted by melanoidin remain unchanged after treatment. Biological treatment systems could remove only 6–7% of melanoidin and therefore, reverse osmosis and/or advanced oxidation processes (AOPs) have been used to concentrate or degrade melanoidins [\[2–4](#page--1-1)].

Microwave (MW) technology has been used for various applications including preparation of catalysts  $[5-7]$ , sludge management  $[8,9]$  $[8,9]$  $[8,9]$  $[8,9]$  $[8,9]$ , biogas production [[10\]](#page--1-5), heating and enhancement of different catalytic oxidation and reduction processes [\[11](#page--1-6)[,12](#page--1-7)]. MW systems are coupled with other AOPs and oxidants such as persulfate (PS) and hydrogen peroxide  $(H_2O_2)$  for the treatment of wastewaters containing various organic pollutants. [\[13–21](#page--1-8)]. MW creates hotspots and favors free radical generation, which in turn reduces the activation energy [[22\]](#page--1-9). The mechanism of sulphate radicals (SO<sub>4</sub><sup> $\bullet$ </sup>) and hydroxyl radicals (OH<sup> $\bullet$ </sup>) reaction under MW irradiation is explained based on Eqs. (1–9). Under acidic conditions, the addition of PS to MW system accelerates the generation of  $SO_4^{\bullet -}$  as shown in Eq. (1). Subsequently, the generated SO4 ●<sup>−</sup> can lead to the formation of OH● (Eqs. 3,4). Similarly, the

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presence of  $H_2O_2$  under MW environment can generate OH<sup> $\bullet$ </sup> and superoxide ion  $(O_2^{\bullet -})$  (Eq. 9) whereas under combined PS/H<sub>2</sub>O<sub>2</sub>, per-oxymonosulfate (HSO<sub>5</sub>) can be generated as shown in Eq. 12 [[23,](#page--1-10)[24](#page--1-11)]. The efficiency of HSO<sub>5</sub> is higher compared to PS, which can result in enhancement of pollutant removal [[19,](#page--1-12)[23\]](#page--1-10). On the other hand, the presence of HSO<sub>5</sub>, SO<sub>4</sub><sup> $\bullet$ </sup>, OH<sup> $\bullet$ </sup> and O<sub>2</sub> $\bullet$ <sup>-</sup> could accelerate the rate of pollutant removal and better mineralization of the organics. However, high concentration of radicals may result in self-quenching effect (Eq. 2,10) and in turn could reduce the rate of oxidation [[25–27\]](#page--1-13). The generation of radical has been quantified in the past with alcohol quenching experiments [\[27](#page--1-14)[,26](#page--1-15)]. In addition, the removal rate also depends on the nature of pollutant, type of bonding between molecules and structure of the target compound.

$$
MW\text{ Heat} + S_2O_8^{2-} \rightarrow 2SO_4^{\bullet-} \tag{1}
$$

$$
SO_4^{*-} + SO_4^{*-} \to S_2 O_8^{2-} (k = 4 \text{ to } 8.1 * 10^8 L \text{ mol}^{-1} s^{-1})
$$
 (2)

$$
SO_4^{\bullet -} + H_2O \to SO_4^{2-} + OH^{\bullet} + H^+(k = 6 \times 10^1 L \, mol^{-1} s^{-1})
$$
 (3)

$$
SO_4^{\bullet -} + OH^- \rightarrow SO_4^{2-} + OH^{\bullet} \ (k = 4.6 \ to \ 8.3 \times 10^7 L \ mol^{-1} s^{-1})
$$
 (4)

$$
OH^{\bullet} + H_2O_2 \rightarrow HO_2^{\bullet} + H_2O \ (k = 2.7 \times 10^7 L \ mol^{-1} s^{-1}) \tag{5}
$$

$$
OH^{\bullet} + OH^- \rightarrow H_2O + O^{\bullet -} (k = 1.3 \times 10^{10} L \, mol^{-1} s^{-1})
$$
 (6)

 $OH^{\bullet}$  +  $SO_4^{2^-}$ /  $HSO_4^{-}$   $\rightarrow$   $SO_4^{\bullet}$  +  $OH^-$ / $H_2O$  ( $k = 3.5 \times 10^5 L$  mol<sup>-1</sup>s<sup>-1</sup>)

$$
S_2O_8^{2^-} + 2e^- \to 2SO_4^{2^-}(E0 = 2.01 V) \tag{8}
$$

 $MW$  Heat +  $3H_2O_2 \rightarrow 2OH^* + 2H_2O_2 \rightarrow 2O_2^* + 2H^*$  $+ 2H_2O (k = 1.2 \text{ to } 6.5 \times 10^7 L \text{ mol}^{-1} \text{s}^{-1})$  (9)

$$
SO_4^{\bullet -} + S_2 O_8^{2-} \to SO_4^{2-} + S_2 O_8^{\bullet -} (k = 5.5 \times 10^5 L \, mol^{-1} s^{-1}) \tag{10}
$$

$$
MW\;Heat \; + \; S_2O_8^{2^-} + H^+ \to HS_2O_8^- \to SO_4^{2^-} + SO_4^{\bullet} + H^+ \tag{11}
$$

$$
MW\text{ Heat} + \text{SO}_4^{\bullet-} + \text{OH}^{\bullet} \rightarrow \text{HSO}_5^{\bullet} \tag{12}
$$

 $MW$  Heat + Pollutant +  $HSO_5^-/SO_4^{\bullet-}/OH^{\bullet}/O_2^{\bullet-} \rightarrow Intermediate$  products

$$
+ CO2 + H2O \t\t(13)
$$

The presence of melanoidin produces deep brown colour and therefore, AOPs that are not dependent on photochemical activation are generally preferred. As a result, ozonation, ultrasound, and other similar hybrid systems have been adopted for melanoidin removal [[28–30\]](#page--1-16). It was reported that coupled multi-oxidant systems are capable of producing synergistic effects [\[31\]](#page--1-17). Thus far, melanoidin removal in coupled MW-multi-oxidant system has not been investigated in detail. Moreover, the interactions of oxidant dosage with pH and initial melanoidin concentration are difficult to be predicted in traditional experimental design under MW-multi-oxidant systems. Central composite design (CCD) is an effective tool used for design of experiment, optimization of system parameters, analysis of variance and error analysis. Therefore, this investigation is focused to study the (a) melanoidin removal between MW-PS, MW-H<sub>2</sub>O<sub>2</sub> and MW-PS/ H<sub>2</sub>O<sub>2</sub> systems, (b) melanoidin removal rate constants under different systems, (c) interaction between initial melanoidin concentration, pH and oxidant dosage by CCD, (d) generation of free radical species with alcohol scavenging experiments, and (e) cost for melanoidin removal in the MW-multi-oxidant system.".

#### **2. Materials and methods**

#### *2.1. Chemicals*

Sodium persulfate (98% w/w) and hydrogen peroxide (30% w/w) were purchased from AVRA Chemicals, India and Fischer Scientific,

India, respectively. Premium grade ethanol (EtOH) and analytical grade tert-butanol (TBA, 99% purity) was purchased from Hayman, UK, and Merck, India, respectively. Analytical grade Dimethyl sulfoxide (DMSO) and 2,4-Dinitrophenylhydrazine (DNPH) were purchased from Cisco research laboratory ltd., India. Acetonitrile (HPLC grade) was purchased from Rankem, India. Dextrose, glycine, NaOH, and  $H<sub>2</sub>SO<sub>4</sub>$  used for the experiments were procured from Merck, India. Distilled water (DW) was used for all experimental purpose.

### *2.2. Preparation of melanoidin solution*

A stock melanoidin solution of 210  $\pm$  20 g/L (COD ~ 240  $\pm$  10 g/ L) was prepared by mixing dextrose (1 M), glycine (1 M) and sodium carbonate (0.5 M). Subsequently, the solution pH was adjusted to 7 by adding  $1 \text{ N H}_2\text{SO}_4$ , stirred for  $30 \text{ min}$  and incubated in a hot air oven at 95℃ for 7 h. The dark brown solution obtained was cooled and stored at 4℃ in the refrigerator.

#### *2.3. MW reactor set-up*

(7)

A customized MW reactor, as used previously [\[14](#page--1-18)], of frequency 2450 MHz and capable of operating at 1000 W with an inbuilt magnetic stirrer and temperature sensor was used for the experimental work (Ragatech Pvt. Ltd., India). A reaction vessel of 1 L volume was used and 500 W power and 80 ℃ was maintained throughout the experiment. The MW reactor was operated in batch mode with 100 mL working volume. A counterflow heat-exchanging condenser was housed to collect the vapour which was circulated back into the reaction vessel to maintain a constant working volume.

#### *2.4. Experimental techniques*

#### *2.4.1. Melanoidin removal batch experiments*

In order to evaluate the effect of pH, dosage and irradiation time on melanoidin removal, MW- batch experiments were conducted with 250 mg/L of melanoidin and under different combinations of pH (2-12), PS dosage (100-5000 mg/L) and  $H_2O_2$  dosage (100-6000 mg/ L). The experiments were conducted for 20 min and the samples were withdrawn from the reactor at various time intervals to determine melanoidin removal. The batch study was divided into three phases: 1) MW-PS, 2) MW-H<sub>2</sub>O<sub>2</sub> and 3) MW-PS/H<sub>2</sub>O<sub>2</sub>. The effect of PS and/or  $H<sub>2</sub>O<sub>2</sub>$  dose, MW irradiation time and pH on melanoidin removal observed in these experiments are used to evaluate boundary condition for CCD experiments with MW-PS/H<sub>2</sub>O<sub>2</sub> system.

Alcohol quenching experiment was conducted for melanoidin degradation with MW-PS/H<sub>2</sub>O<sub>2</sub> process in presence of scavenging agent to stop radical generation during the reaction. The scavengers used were TBA and EtOH for quenching OH<sup> $\bullet$ </sup> and SO<sub>4</sub> $\bullet$ , respectively. The concentration of each scavenging agent added during the experiment was 0.4 M to compare effect of scavengers on melanoidin removal. The OH<sup>\*</sup> was estimated by trapping with DMSO and converting into formaldehyde by adding DNPH. The DNPH-HCHO concentration was detected and calibrated in HPLC (Dionex, USA) fitted with C18 silicabased reverse phase column and UV–vis detector. The mobile phase was acetonitrile: water (60:40) with a flow rate of 1 mL/min. The retention time of DNPH and DNPH-HCHO derivatives were found at 4.8 and 7.4 min, respectively. For HPLC analysis, 2.5 mL of sample was added to 2.5 mL of 25 mM phosphate buffer and 0.2 mL of DNPH. Subsequently, the sample was mixed well and kept for 30 min in room temperature. Finally, the resultant mixture was diluted 20 times and injected into HPLC for analysis.

#### *2.4.2. Experimental design for melanoidin removal*

The response surface methodology was used to optimise experimental parameters of MW-PS/H<sub>2</sub>O<sub>2</sub> system for better melanoidin removal at different initial concentrations. A  $2<sup>4</sup>$  full factorial design with Download English Version:

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