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The influence of calcium chloride deicing salt on phase changes and damage development in cementitious materials



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ABSTRACT

The conventional CaCl₂–H₂O phase diagram is often used to describe how calcium chloride behaves when it is used on a concrete pavement undergoing freeze-thaw damage. However, the chemistry of the concrete can alter the appropriateness of using the CaCl₂–H₂O phase diagram. This study shows that the Ca(OH)₂ present in a hydrated portland cement can interact with CaCl₂ solution creating a behavior that is similar to that observed in isoplethal sections of a ternary phase diagram for a Ca(OH)₂–CaCl₂–H₂O system. As such, it is suggested that such isoplethal sections provide a reasonable model that can be used to describe the behavior of concrete exposed to CaCl₂ solution as the temperature changes. Specifically, the Ca(OH)₂ can react with CaCl₂ and H₂O resulting in the formation of calcium oxychloride. The formation of the calcium oxychloride is expansive and can produce damage in concrete at temperatures above freezing. Its formation can also cause a significant decrease in fluid ingress into concrete. For solutions with CaCl₂ concentrations greater than about 11.3% (by mass), it is found that calcium oxychloride forms rapidly and is stable at room temperature (23 °C).

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1. Introduction

Concrete pavement and flatwork may degrade when they are exposed to deicing chemicals. The deicing salt solution can be absorbed into the pores of concrete and can alter the cementitious matrix. The interaction between the deicing salt solution and the cementitious matrix may result in damage to the concrete [1]. Physical damage can occur due to a number of processes: 1) exposure of concrete with a high degree of saturation to freeze-thaw cycles [2–7], 2) scaling of concrete surfaces [8–11], 3) crystallization of salt in concrete pores that results in production of an internal stress [12–14], and 4) expansive forces as a result of corrosion of reinforcement when a chloride-based deicing salt is used [15,16]. While the physical attack of deicing salts has been

widely investigated, the chemical reaction between the matrix and the deicing salts has been studied less frequently.

The use of deicing salts can cause damage in cementitious materials even if a concrete does not experience freezing and melting [10,17–22]. This may be caused by the formation of Friedel's salt, Kuzel's salts [18,21–23], and/or calcium oxychloride, changes in the pore solution properties [4,17], or changes in the microstructure of hydration products [19,20,22]. Deicing salt solution, like many external solutions, may also dissolve calcium hydroxide, causing leaching that leads to an increase in permeability and a reduction of concrete alkalinity [16,24].

Deicing salts have different chemical and physical interactions with cementitious materials. The use of NaCl deicing salt increases freeze-thaw damage in concrete. This increase in freeze-thaw damage has been explained by the formation of an unexpected phases and the creation of osmotic pressures [4,17,20]. Concrete exposed to CaCl₂ and MgCl₂ de-icing salts also exhibited changes in the concrete microstructure. These changes have been accompanied by a severe cracking and deterioration, even if the concrete did

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(2)

not experience any freeze-thaw cycles [18,21,22,25].

Chloride-based deicers can result in the formation of calcium chloroaluminate phases such as Friedel's salt and Kuzel's salt that can bind chloride [22,23,26–28]. Possible reactions for the formation of Friedel's salt in the presence of CaCl₂, for example, are shown in Eq. (1) [28] and Eq. (2). Kuzel's salt (3CaO·Al₂O₃·0.5CaSO₄·0.5CaCl₂·11H₂O) may be also produced in the presence of chloride-based deicing salts [23,29].

$$CaCl_2 + 3CaO \cdot Al_2O_3 + 10H_2O \rightarrow 3CaO \cdot Al_2O_3 \cdot CaCl_2 \cdot 10H_2O$$
(Friedel's salt)
(1)

 $\begin{array}{c} \text{CaCl}_2 + 3\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot \text{CaSO}_4 \cdot 12\text{H}_2\text{O} \rightarrow 3\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot \text{CaCl}_2 \cdot 10\text{H}_2\text{O} \\ & (\text{Monosulfate}) \\ + \text{CaSO}_4 \cdot 2\text{H}_2\text{O} \\ & (\text{Gypsum}) \end{array}$

Collepardi et al. [19] concluded that $CaCl_2$ can result in a reaction that leads to damage, even in the absence of freeze-thaw cycles. The chemical reaction is described by the formation of calcium oxy-chloride (Eq. (3)).

$$\begin{aligned} & 3\text{Ca}(\text{OH})_2 + \text{Ca}\text{Cl}_2 + 12\text{H}_2\text{O} \rightarrow \text{Ca}\text{Cl}_2 \cdot 3\text{Ca}(\text{OH})_2 \cdot 12\text{H}_2\text{O} \\ & (\text{Calcium oxychloride}) \end{aligned} \tag{3}$$

The temperature at which calcium oxychloride forms is above the freezing point of water [18,21,22,26,30,31]. The reaction has also been described as a rapid reaction between calcium hydroxide and calcium chloride, however the rate of this reaction has not been quantified. The reaction between calcium chloride and calcium hydroxide (i.e., solid phases in the reaction) is expansive and can be destructive when it forms in the concrete matrix due to the internal hydraulic pressures that may be generated. Calcium oxychloride is unstable at room temperature and lower levels of relative humidity [18,32]. Calcium oxychloride has been reported with different molar ratios (i.e., $CaCl_2 \cdot 3Ca(OH)_2 \cdot 12H_2O$, $CaCl_2 \cdot Ca(OH)_2 \cdot xH_2O$, and $CaCl_2 \cdot Ca(OH)_2$; these phases may coexist and be interchangeable in Ca(OH)₂-CaCl₂-H₂O systems. However, CaCl₂·3Ca(OH)₂·12H₂O was observed to be destructive and can be simply altered to $CaCl_2 \cdot Ca(OH)_2$ or $CaCl_2 \cdot Ca(OH)_2 \cdot xH_2O$ if the ambient temperature or humidity varies [32–34].

Fig. 1a shows the conventional phase diagram for the $CaCl_2-H_2O$ binary system. Fig. 1b illustrates an isoplethal section from the work of Vol'nov and Latysheva, and Makarov and Vol'nov [35,36] for a ternary system containing $Ca(OH)_2-CaCl_2-H_2O$. It

should be mentioned that the formation of the different phases in this isoplethal section (Fig. 1b) were reported only as a function of temperature and CaCl₂ concentration. As such, the effect of Ca(OH)₂:CaCl₂ mass/molar ratio on the formation of the different phases was not considered, but is important. Different phases exist in the Ca(OH)₂-CaCl₂-H₂O system: CaCl₂ solution, Ca(OH)₂, ice, CaCl₂·3Ca(OH)₂·12H₂O, CaCl₂·Ca(OH)₂·xH₂O, and CaCl₂·nH₂O (where n is 2, 4, or 6).

A conventional interpretation of the CaCl₂–H₂O phase diagram (Fig. 1a) shows that using a higher concentration of CaCl₂ can reduce freezing temperature. However, Fig. 1b shows the Ca(OH)₂–CaCl₂–H₂O isopletal section that occurs when Ca(OH)₂ is added as a third phase. It can be seen that Ca(OH)₂ from the cementitious matrix in concrete alters the behavior. The interaction between Ca(OH)₂ and CaCl₂ can alter concrete microstructure and pore solution properties resulting in the formation of calcium oxychloride. The formation and precipitation of calcium oxychloride (as an expansive phase) may change transport properties of concrete due to pore blocking and may also cause a severe deterioration due to internal expansion, even when the concrete temperature remains above 0 °C, since it forms at a temperature greater than 0 °C (Fig. 1b).

The temperature at which calcium oxychloride forms, its relation to the concentration of CaCl₂ solution, and its rate of formation can play an important role in concrete freeze-thaw behavior, concrete degradation, and fluid ingress into concrete.

The main purpose of this study is to provide an improved understanding of the interaction between the calcium chloride deicing salt and cementitious material and to investigate its impact on concrete deterioration. In this paper, several techniques were used to understand the $Ca(OH)_2-CaCl_2-H_2O$ system and isoplethal sections (varying the concentration of $Ca(OH)_2$) were used as a model system for a cementitious system. The temperatures at which different phase changes occur were also determined.

2. Experimental program

Mortar freeze-thaw behavior, mortar degradation, and fluid ingress into mortar were evaluated when the specimens were exposed to a CaCl₂ deicing salt. First, a low temperature longitudinal guarded comparative calorimeter equipped with acoustic emission detection (AE-LGCC) was used to investigate the damage (cracking) that occurs during the freezing and melting of mortar specimens saturated with solutions containing different concentrations of CaCl₂. Micro focused X-ray fluorescence (µXRF) examination was used to study the CaCl₂ solution ingress into these mortar specimens. Low temperature differential scanning



Fig. 1. a) Classical phase diagram for $CaCl_2-H_2O$ system and b) an isoplethal section for a $Ca(OH)_2-CaCl_2-H_2O$ system developed from Refs. [35,36] ($Ca(OH)_2:CaCl_2$ molar ratios ≤ 0.5).

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