



# Effect of nitrite on the $\text{N}_2\text{O}$ and $\text{NO}$ production on the nitrification of low-strength ammonium wastewater

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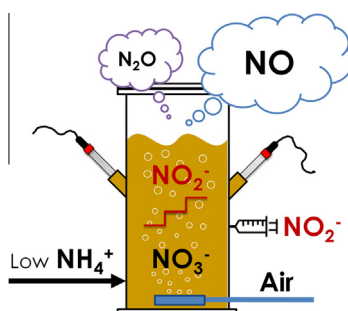
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## HIGHLIGHTS

- Nitrite effect on  $\text{N}_2\text{O}$ – $\text{NO}$  emission in a low strength nitrifying system was studied.
- Nitrite presence in the reactor increases  $\text{N}_2\text{O}$  and  $\text{NO}$  emissions.
- High nitrite concentrations affect more  $\text{NO}$  emissions than  $\text{N}_2\text{O}$  emissions.
- The intermediate  $\text{NO}$  cannot be neglected during autotrophic denitrification.
- High nitrite concentrations inhibit the ammonium oxidising activity.

## GRAPHICAL ABSTRACT



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## ABSTRACT

The effect of nitrite on  $\text{N}_2\text{O}$  and  $\text{NO}$  emission was assessed in a nitrifying lab-scale reactor fed with low strength ammonium wastewater. The effect of nitrite pulse additions ( $5\text{--}50\text{ mg NO}_2^- \text{N L}^{-1}$ ) and of step-wisely increasing nitrite concentrations ( $0\text{--}150\text{ mg NO}_2^- \text{N L}^{-1}$ ) was studied. For the pulse addition experiments,  $\text{N}_2\text{O}$  and  $\text{NO}$  emissions increased upon pulse addition of nitrite, decreasing to the original concentration once nitrite was consumed. The highest peak emissions were detected at nitrite concentrations of  $50\text{ mg NO}_2^- \text{N L}^{-1}$ . For the step-wisely increasing nitrite tests,  $\text{N}_2\text{O}$ -N emission per  $\text{NH}_4^+$ -N converted increased linearly from 0.16% to 1.5%.  $\text{NO}$  emissions were substantially affected at nitrite concentrations higher than  $50\text{ mg NO}_2^- \text{N L}^{-1}$ , reaching 3.8%  $\text{NO}$ -N per  $\text{NH}_4^+$ -N converted at  $150\text{ mg NO}_2^- \text{N L}^{-1}$ . The results provide one of the first evidences of the combined effect of nitrite on  $\text{N}_2\text{O}$  and  $\text{NO}$  emissions, showing a stronger effect on  $\text{NO}$  emissions at high nitrite concentrations.

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## 1. Introduction

Nitrogen removal during wastewater treatment emits nitrous oxide ( $\text{N}_2\text{O}$ ) and nitric oxide ( $\text{NO}$ ) [1,2].  $\text{N}_2\text{O}$  is an important greenhouse gas with a global warming potential of 298- $\text{CO}_2$  equivalents [3], which may contribute significantly to the carbon footprint of wastewater treatment plants (WWTPs) [4,5].  $\text{NO}$  is a very reactive gas that is involved in different physiological reactions in living

organisms and becomes toxic at certain concentrations [6]. Both  $\text{N}_2\text{O}$  and  $\text{NO}$  contribute significantly to the ozone layer depletion [7,8]. The importance of studying the emissions of these gases from wastewater treatment lies on their environmental impact and their potential function as useful indicators of process disturbances [9]. Understanding the responsible mechanisms involved during the production of  $\text{N}_2\text{O}$  and  $\text{NO}$ , as well as knowing the factors that influence these emissions is essential to minimise their emissions and to reach a better process operation.

There is increasing evidence that the first step of nitrification (the conversion of ammonia to nitrite) conducted by ammonium

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oxidising bacteria (AOB), is the major contributor to  $\text{N}_2\text{O}$  and NO emissions in the biologically mediated wastewater treatment processes [10,11]. AOB can produce  $\text{N}_2\text{O}$  and NO via two known pathways: the nitrifier denitrification and the hydroxylamine oxidation pathway. The first one is favored by limited oxygen conditions [12,13] and the presence of nitrite [1]. The second is enhanced at high ammonium oxidation rates [14]. Moreover, other factors such as pH [15], transient anoxic-aerobic conditions [16], salinity [17] or aeration intensity [18] have been reported to affect  $\text{N}_2\text{O}$  and NO emissions from nitrifying systems.

A lot of studies focused on the emissions of  $\text{N}_2\text{O}$  and NO for high strength ammonium wastewater, typically the reject water from the anaerobic digester [19–21]. The removal of nitrogen from such wastewater via nitrite has been gaining importance over the last years since it allows substantial energy (less aeration) and chemical savings compared to conventional processes over nitrate. However, partial nitrification systems used for the treatment of high strength wastewater have been shown to produce higher  $\text{N}_2\text{O}$  and NO emissions compared to full nitrification reactors [10,11] probably because of the high accumulation of nitrite in those systems and also the high ammonium conversion rates.

Relatively little research has been devoted to  $\text{N}_2\text{O}$  and NO emissions from systems treating low strength wastewater. Some studies focused on  $\text{N}_2\text{O}$  emissions from nitrification or combined nitrification–denitrification systems, without measuring NO [13,22]. Kampschreur et al. [23] is one of the few studies where NO was measured together with  $\text{N}_2\text{O}$  in a nitrifying culture. They found that  $\text{N}_2\text{O}$  and NO emissions are linearly proportional to the nitrite increase. In systems dealing with low-strength wastewater, the accumulation of nitrite may happen depending on the operating conditions and loading rates of the plant at certain moments. Occasional nitrite accumulation was also put forward as the cause for  $\text{N}_2\text{O}$  emissions from a full-scale municipal (low strength) wastewater treatment plant [24]. Moreover, the application of autotrophic nitrogen removal via nitrite for low strength ammonium wastewater is gaining interest since this technology can contribute to energy-positive WWTPs [25,26]. However, there is a lack of studies assessing the potential  $\text{N}_2\text{O}$  and NO emissions in these systems where nitrite can accumulate. Besides, the effect of nitrite on NO in nitrifying cultures adapted and non-adapted to nitrite is not well understood yet. Thus, further research is needed regarding the  $\text{N}_2\text{O}$  and NO emissions during nitrification of domestic wastewater and the effect of nitrite accumulation on the  $\text{N}_2\text{O}$  and NO emissions in these systems.

The present study explores the effect of nitrite on the  $\text{N}_2\text{O}$  and NO emissions during the full-nitrification of low strength synthetic ammonium wastewater through dedicated experiments. The effect of nitrite shocks as well as step-wisely increasing nitrite concentrations in the reactor on the emissions of both gases was assessed to gain understanding of the mechanisms producing  $\text{N}_2\text{O}$  and NO and to fully capture the overall emission dynamics of both gases. The results thus contribute to the potential reduction of their emissions during municipal wastewater treatment with punctual nitrite accumulation.

## 2. Materials and methods

### 2.1. Reactor operation

A sequencing batch reactor (SBR) of 8 L was inoculated with activated sludge from the municipal WWTP of Girona (Spain) and was operated during 5 months, obtaining a nitrifying mixed bacterial culture. The SBR was operated in 6-h cycles: 240 min of continuous feeding and aeration, settling during 100 min and 20 min for decanting. Four litres of synthetic wastewater were fed in each

cycle, resulting in a hydraulic retention time (HRT) of 12 h. The influent ammonium concentration was set low ( $50 \text{ mg NH}_4^+\text{-N L}^{-1}$ ) and no temperature control was established in the reactor. Dissolved oxygen (DO) was controlled with a programmable logic controller (PLC) between 2.0 and  $2.5 \text{ mg O}_2 \text{ L}^{-1}$  by adjusting the amount of air and nitrogen in the added gas stream, of which the total flow was kept constant at  $3.5 \text{ L min}^{-1}$ . The pH was controlled between 6.7 and 7.0 by adding 1 M  $\text{NaHCO}_3$ .

The composition of the synthetic wastewater used as influent consisted of:  $282.1 \text{ mg NH}_4\text{HCO}_3 \text{ L}^{-1}$ ,  $87.8 \text{ mg KH}_2\text{PO}_4 \text{ L}^{-1}$ ,  $110.0 \text{ mg K}_2\text{HPO}_4 \text{ L}^{-1}$  and  $2 \text{ mL L}^{-1}$  of a trace element solution that included ( $\text{g L}^{-1}$ ): 1.25 EDTA, 0.55  $\text{ZnSO}_4\cdot 7\text{H}_2\text{O}$ , 0.40  $\text{CoCl}_2\cdot 6\text{H}_2\text{O}$ , 1.27  $\text{MnCl}_2\cdot 4\text{H}_2\text{O}$ , 0.40  $\text{CuSO}_4\cdot 5\text{H}_2\text{O}$ , 0.05  $\text{Na}_2\text{MoO}_4\cdot 2\text{H}_2\text{O}$ , 1.37  $\text{CaCl}_2\cdot 2\text{H}_2\text{O}$ , 1.25  $\text{FeCl}_3\cdot 6\text{H}_2\text{O}$ ,  $44.4 \text{ mg SO}_4\cdot 7\text{H}_2\text{O}$ .

The batch tests were conducted when the reactor had been operating for 4 months and it showed stable operation, with all the ammonium from the influent converted to nitrate without accumulation of nitrite (detailed cycle analysis and nitrogen balance presented in [Section S1 from Supplementary information](#)).

### 2.2. Analysis and measurements

Cycle studies were carried out on a weekly basis to assess the reactor performance. Samples were taken along the cycle and immediately filtered through disposable Millipore filter units ( $0.22 \mu\text{m}$  pore size) and then analysed to determine the  $\text{NH}_4^+\text{-N}$ ,  $\text{NO}_2^-\text{-N}$  and  $\text{NO}_3^-\text{-N}$  concentrations by ion chromatography (ICS5000, DIONEX). Mixed liquor suspended solids (MLSS) and volatile MLSS (MLVSS) were determined according to the standard methods [27]. During the batch tests the averaged MLSS and MLVSS in the reactor were  $0.63 \pm 0.09 \text{ g MLSS L}^{-1}$  and  $0.50 \pm 0.05 \text{ g MLVSS L}^{-1}$ , respectively.

$\text{N}_2\text{O}$  and NO were monitored online in the gas phase every 5 s during the batch tests.  $\text{N}_2\text{O}$  was analysed with the infrared gas analyser Servomex 4900 (Servomex Group Ltd. East Sussex, UK) and NO was measured via the chemiluminescence gas analyser CLD64 (Eco Physics. Dürnten, Switzerland).

### 2.3. Batch tests

All batch tests were conducted in the SBR. After the decanting phase of the cycle previous to the batch test, the feeding pump was disconnected and the desired addition of ammonium and/or nitrite started. The pH and DO were kept at the same levels as normal reactor operation (described in [Section 2.1](#)). After each test, the SBR operation was kept normal at least for 24 h before another test was conducted.

#### 2.3.1. Intermittent ammonium feeding with nitrite pulse additions

An experiment was designed to assess the effect of nitrite on  $\text{N}_2\text{O}$ –NO emissions in the absence of ammonium oxidation. A pulse of nitrite of  $10 \text{ mg NO}_2^-\text{-N L}^{-1}$  (reactor concentration) was added without ammonium feeding. Once nitrite was completely oxidised to nitrate, ammonium feeding was re-established at a rate of  $0.833 \text{ mg NH}_4^+\text{-N min}^{-1}$ . This test was repeated twice.

#### 2.3.2. Continuous ammonium feeding with nitrite pulse addition

Four sets of tests were conducted to check the effect of 4 different nitrite concentrations (5, 10, 25 and  $50 \text{ mg NO}_2^-\text{-N L}^{-1}$ ), added as pulses, on  $\text{N}_2\text{O}$ –NO emissions. During all the tests, ammonium was fed continuously at a rate of  $0.833 \text{ mg NH}_4^+\text{-N min}^{-1}$  and 3–4 pulses of nitrite (to provide the desired concentration of  $\text{NO}_2^-\text{-N L}^{-1}$  in the reactor, see [Table 1](#)) were added.

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