



Cubic yttria stabilized zirconia sintering additive impacts: A comparative study

Andrew J. Flegler, Theodore E. Burye, Qing Yang, Jason D. Nicholas*

Chemical Engineering & Materials Science Department, Michigan State University, East Lansing, MI 48824, USA

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Abstract

To evaluate the impact sintering additives have on the processing and performance of 8 mol% yttria stabilized zirconia (8YSZ), the 25–1525 °C sintering kinetics, phase purity, microstructure, and electrical properties of a single batch of 8YSZ powder surface-coated with 1, 3 and 5 mol% of barium, bismuth, calcium, cobalt, copper, iron, lithium, magnesium, manganese, nickel, strontium or zinc were investigated via constant heating rate dilatometry, X-ray diffraction, scanning electron microscopy, and AC impedance spectroscopy. For electrochemical applications where dense 8YSZ is required, iron was found to give the best combination of 8YSZ cubic zirconia phase stability, high oxygen ion conductivity, and enhanced densification kinetics. 5 mol% iron was found to reduce the 8YSZ sintering temperature by ~150 °C. © 2014 Elsevier Ltd and Techna Group S.r.l. All rights reserved.

Keywords: Zirconia; Sintering additive; Dopant; Sintering Aid

1. Introduction

8 mol% Yttria stabilized zirconia (8YSZ) is used in a variety of applications including solid oxide fuel cells [1,2], oxygen sensors [3,4], electrolyzers [5], biocompatible implant coatings [6], and thermal barrier coatings [7]. Because sintering additives can induce changes in sintering temperature, fracture toughness and/or electrical conductivity [8–18], an understanding of 8YSZ sintering additive impacts is critical for tailoring the fabrication and/or high-temperature operational stability of these devices. To evaluate the relative impact of different 8YSZ sintering additives (be they intentionally added dopants/sintering aids or unintentionally added impurities), constant heating rate dilatometry on a single batch of 8YSZ powder surface-coated with 1, 3 and 5 mol% of Ba, Bi, Ca, Co, Cu, Fe, Li, Mg, Mn, Ni, Sr or Zn was performed. Further, since retention of the cubic 8YSZ crystal structure and a high ionic conductivity are often important in electrochemical

applications, X-ray diffraction (XRD) and electrochemical impedance spectroscopy (EIS) were also performed.

2. Experimental methods

2.1. Sample preparation

To eliminate interpretation difficulties caused by differences in 8YSZ particle size, particle size distribution, impurities etc., a single batch of TZ-8Y YSZ powder (Tosoh USA; Grove City, OH, USA) was used for the experiments reported here. As indicated by the manufacturer's certificate of analysis, this powder was 13.45 wt% Y_2O_3 (i.e. $Y_{0.1450}Zr_{0.8550}O_{1.927}$, $(Y_2O_3)_{0.07817}(ZrO_2)_{0.9218}$, or 7.817 mol% yttria stabilized zirconia) and had a SiO_2 content of 175 ppm. According to the manufacturer, and confirmed here via scanning electron microscopy, this spray dried powder had a 13.6 m²/g specific surface area and consisted of 21 nm diameter crystallites agglomerated into 600 nm diameter (d_{50}) particles forming the walls of hollow, 60 μm diameter (d_{50}) spray dried granules. To eliminate possible silica contamination from glassware and cross-contamination between sintering additives, dedicated

*Corresponding author.

E-mail address: jdn@msu.edu (J.D. Nicholas).

URL: <https://www.egr.msu.edu/nicholasgroup/> (J.D. Nicholas).

Nomenclature

8YSZ	$(\text{Y}_2\text{O}_3)_{0.08}(\text{ZrO}_2)_{0.92}$	M_{Bulk}	oxygen vacancy mobility in the bulk
A	sample cross-sectional area	$PLC(T)$	percent linear change in sample length, $((l-l_o)/l_o)100$
c_{Bulk}	oxygen vacancy concentration in the bulk	R_{Bulk}	bulk impedance arc resistance
$C_{G.B.}$	grain boundary impedance arc capacitance	$R_{G.B.}$	grain boundary impedance arc resistance
DS	cubic zirconia destabilization into monoclinic and/or tetragonal zirconia.	ρ_{Arc}	the post-sintering, 25 °C relative density measured by the Archimedes method
d	grain size	ρ_{Dil}	the post-sintering, 25 °C relative density measured by the dilatometer using Eq. (1)
$\delta_{G.B.}$	electrical grain boundary width	$\rho(T)$	relative density
EIS	electrochemical impedance spectroscopy	$\rho_{\text{th}}(T)$	theoretical density
ϵ_o	permittivity of free space	q	charge
$\epsilon_{T,\text{Creep}}$	true strain induced by creep	σ_{Bulk}	bulk oxygen ion conductivity
$\epsilon_{T,\text{Dens}}$	true strain induced by densification	σ_T	total oxygen ion conductivity
$\epsilon_{T,\text{Dil}}$	true dilatometer-recorded strain	$\sigma_{G.B.}$	total grain boundary oxygen ion conductivity
$\epsilon_{T,\text{Mass Loss}}$	true strain induced by sample mass loss	$\sigma_{G.B.}^{\text{sp}}$	specific grain boundary oxygen ion conductivity
$\epsilon_{T,\text{Phase Change}}$	true strain induced by phase changes	SEM	scanning electron microscopy
$\epsilon_{T,\text{Total}}$	total true strain	SSS	solid state sintering
k_{gb}	grain boundary dielectric constant	T	temperature
l	sample length	TGA	thermo-gravimetric analysis
l_o	original sample length	XRD	X-ray diffraction
LPS	liquid phase sintering		

polyethylene ball milling jars, polyethylene coated magnetic stir bars, and polypropylene beakers were used for each of the twelve sintering additives.

Dissolved nitrates were used to introduce sintering additives into the 8YSZ powder. All the nitrates (Alfa Aesar; Ward Hill, MA, USA) had nominal purities greater than 99.99%. Prior to use, the water content in each nitrate was measured to five significant figures through thermo-gravimetric analysis (TGA) from 25 °C to temperatures as high as 850 °C. In all cases, the measured water of hydration coefficients rounded to the single digit values provided by the manufacturer.

To prepare 1, 3 and 5 mol% surface-coated 8YSZ powders for dilatometry, appropriate amounts of barium nitrate, bismuth nitrate, calcium nitrate, cobalt nitrate, copper nitrate, iron nitrate, lithium nitrate, magnesium nitrate, manganese nitrate, nickel nitrate, strontium nitrate, or zinc nitrate were dissolved into 22 mL of 0.182 MΩ/cm Milli-Q deionized water (Milli-Pore; Billerica, MA, USA). Sintering additive mole percentages were calculated as the ratio of the moles of nitrate cation to moles of 8YSZ. For instance, 0.9310 g of $\text{Bi}(\text{NO}_3)_3 \cdot 5.1720\text{H}_2\text{O}$ was added to 7.506 g of $\text{Y}_{0.1450}\text{Zr}_{0.8550}\text{O}_{1.927}$ to produce a 3% Bi-8YSZ powder with a composition of $\text{Bi}_{0.3000}\text{Y}_{0.1407}\text{Zr}_{0.8293}\text{O}_{1.915}$. For each sintering additive, the dissolved nitrate, 55 g of 3 mm diameter YTZ[®] tetragonal yttria stabilized zirconia milling media (Tosoh USA; Grove City, OH, USA), and 7.5 g of 8YSZ powder were placed inside a sealed 40 mL polyethylene bottle and ball milled at 50 rpm for 16 h. After removing the milling media, the water was evaporated from the ball-milled colloidal suspensions by stirring the suspensions in 600 mL polypropylene beakers under a fan. The dried, sintering-additive-nitrate-coated 8YSZ powders were then ground using an alumina mortar and pestle

pre-cleaned with 30 μm diamond suspension, and sieved through a 150 μm polyethylene coated stainless steel mesh to break up agglomerates. Afterwards, 1.25 g of powder was uniaxially pressed to 46 MPa in a 1.27 cm diameter steel die to make cylindrical samples with heights ranging from 4.040–4.089 mm. After sample pressing, mass, height and diameter measurements were taken for sample volume/mass green density determinations.

Prior to dilatometry experiments, alumina spacers were produced by uniaxially pressing 3.3 g of AKP-50 alumina powder (Sumitomo Corporation of America; Los Angeles, CA, USA) to 32 MPa in a 1.27 cm diameter steel die. The resulting cylindrical spacers were fired to 1450 °C at 5 °C/min, held there for 20 h, and cooled back to room temperature at a nominal rate of 5 °C/min. In separate 25–1525 °C dilatometry tests, the resulting 10.7 mm thick, > 95% dense alumina pellets only displayed recoverable thermal-expansion induced strain.

2.2. Dilatometry measurements

Dilatometry was performed on doped and undoped 8YSZ samples using a 402C Dilatometer (Netzsch Instruments North America; Burlington, MA, USA) continuously flushed with 50 mL/min of air. To limit dilatometer contamination, each sample was sandwiched between two of the previously described alumina spacers so that the dilatometer pushrod and backstop were not in contact with the sample. In all dilatometry experiments, the entire length of the sample and spacers was 25.4 ± 0.1 mm. Dilatometry was performed from 25 °C to 1525 °C with a 5 °C/min heating rate, no high

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