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Characterization of sintered TiC-SiC composites

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Abstract

TiC–SiC composites were fabricated using TiC and SiC powders as starting materials at the range of $1650-2000~^{\circ}$ C in Ar atmosphere by two-step method. In the first step, the ingots with intragranular SiC or TiC particle were prepared by arc-melting technique, subsequently, crushed and ground into TiC and SiC composite powders. In the second step, TiC–SiC composites were sintered using these as-prepared composite powders by SPS method. It was concluded that these TiC–SiC composites prepared by two-step method showed more excellent properties than that prepared by arc-melting technique. The hardness of the fabricated TiC–SiC composites was 25–27 GPa at the load of $0.98-9.8~^{\circ}$ N, which was obviously greater than that of arc-melting composites. The thermal conductivity of the TiC–SiC composites was $18-48~^{\circ}$ W K $^{-1}$ m $^{-1}$ at the range of $298-1273~^{\circ}$ K and slightly decreased with increasing temperature. The electrical conductivity of the composites was $(2-5)\times 10^5~^{\circ}$ S m $^{-1}$ at the range of $298-1273~^{\circ}$ K and slightly decreased with increasing temperature.

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Keywords: TiC-SiC composites; Two-step method; Microstructure; Arc-melting technique

1. Introduction

Silicon carbide has extremely high hardness and wear resistance, excellent corrosion, thermal shock and oxidation resistance, good high temperature strength, which allow the use of SiC for numerous structural and wear applications, e.g. heat exchanger, metal working parts, nozzles. However, the moderate fracture of toughness of SiC ceramic limits its use under severe conditions. Additions of TiC [1–7] particles were found to be effective in terms of increasing the fracture toughness of SiC ceramic. However, the TiC-SiC composites are difficult to be densified due to the low self-diffusion of SiC in TiC. The TiC-SiC composites are generally synthesized by the hot pressing [8] and SPS technique [9-11]. Moreover, the properties of composites strongly depend on their microstructure. The intragranular microstructure is effective in improving mechanical properties of composite [12]. However, the intragranular composites are difficult to be fabricated by above sintering method. The arc-melted method was one of the best techniques of the preparation of intragranular composites [13–15]. However, the as-prepared specimens have smaller size and are easily cracking. In this paper, the ingots with intragranular SiC or TiC particle, which were prepared by arc-melting technique, were crushed and ground into TiC and SiC composite powders. Subsequently, TiC–SiC composites were sintered using these as-prepared composite powders by SPS method and characterizations were investigated.

2. Experimental

An amount of TiC and SiC powders of high purity (99.9%) and small grain size (0.5–1 μm), produced by Sinopharm Chemical Reagent Co., Ltd., Shanghai, China, were used as starting materials (source, chem.com., grain size). The powders were weighted and mixed in an agate mortar by adding a small amount of ethanol. The mixtures of powders, pressed into disks with 10 mm in diameter at 30 MPa, were melted and directionally solidified by an arc-melted method on the copper base in Ar atmosphere. The arc-melting ingots were crushed and ground into powders with the size of 1–10 μm in an agate mortar. The as-prepared TiC–SiC composite powders were filled into a carbon die for the SPS sintering at 1650–2000 °C, 80 MPa. The sintered TiC–SiC composites were cut into specimens of various sizes for measurement.

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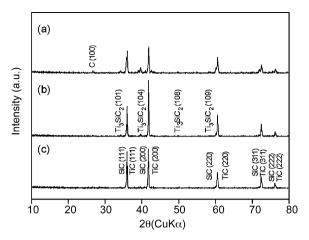


Fig. 1. XRD pattern of as-prepared composite powders at the composition of (a) 50TiC–50 SiC, (b) 70TiC–30 SiC, and (c) 80TiC–20SiC.

The phases of composites were determined by X-ray powder diffraction (Model D/MAX-3B, Rigaku, Japan) with Cu K α radiation. The microstructure was observed by scanning electron microscopy (SEM, SX-40, Akashi Seisakushu). The

hardness of the TiC-SiC composites were measured by the Akashi MVK-E Hardness Tester (Akashi Co., Tokyo, Japan) and calculated by taking the average value of 30 points in the composite indented at random. The electrical conductivities were measured by a dc four-probed method for rectangular specimens. The thermal conductivities were measured by a laser flash method using disk specimens in the temperature range between room temperature and 1023 K (TC-7000 Laser Flash Thermal Constant Analyzer, Japan).

3. Results and discussion

Fig. 1 shows XRD pattern of composite powders prepared by an arc-melting method at the composition of $80 \mbox{TiC-20SiC}, 70 \mbox{TiC-30SiC}$ and $50 \mbox{TiC-50SiC}$ (mol%). The phase of composites had a certain $Ti_3 \mbox{SiC}_2$ and C due to the reaction of TiC and SiC as well as raw materials, TiC and SiC phases. The content of the $Ti_3 \mbox{SiC}_2$ and C increased with increasing the content of SiC due to more decomposing of SiC. Fig. 2 shows the microstructures of TiC–SiC composites sintered by two-step method at $1800\mbox{~°C}$ using $80 \mbox{TiC-20SiC}, 70 \mbox{TiC-30SiC}$ and

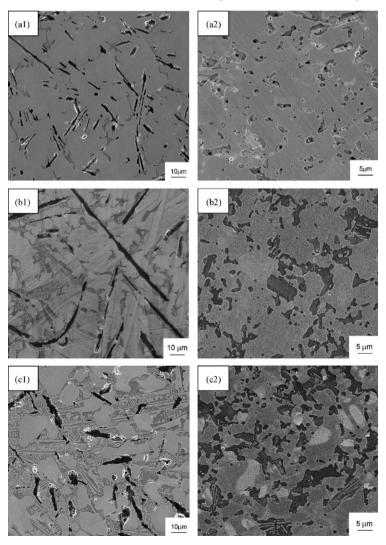


Fig. 2. SEM photograph of TiC–SiC composites prepared under the conditions of (a1) 80TiC–20SiC, arc-melting method, (a2) 80TiC–20SiC, two-step method, (b1) 70TiC–30SiC, arc-melting method, (b2) 70TiC–30SiC, two-step method, (c1) 50TiC–50SiC, arc-melting method, and (c2) 50TiC–50SiC, two-step method.

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