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Integrated evaluation of mixed surfactant distribution in water-oil-steel pipe environments and associated corrosion inhibition efficiency



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ABSTRACT

One multiphysics model, integrated corrosion inhibition (ICI) model, has been theoretically introduced and experimentally validated for the integrated evaluation of water-oil partitioning, aggregation, adsorption/desorption, and corrosion inhibition of mixed surfactant inhibitors in salt-containing water-oil-steel pipe (WOS) environments. The ICI model is based on three major sub-models which consider water-oil surfactant partitioning, micellization, effective adsorption/desorption on substrate, surfactant type, surfactant-solvent interactions, surfactant-counterion pair, and lateral surfactant interactions etc., and intended to serve as a basic framework in the design, selection, optimization, and utilization of various pure and mixed surfactant inhibitors in WOS environments.

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1. Introduction

Carbon steel is one of the most widely used metals in production and transportation in the oil and gas industries [1-3]. However, carbon steel is highly susceptible to corrosion in environments that contain water, CO_2 , H_2S , and various ions (such as CI^-), etc. [4,5]. The presence of CO_2 in oil pipelines exposes carbon steel components to substantial damage due to the accelerated corrosion, which eventually threatens environments, production, and safety [4,6,7]. An illustrated example of a corroded sample, a piece of X65 steel, which is commonly used in oil pipelines, is shown in Fig. 1(a).

A variety of methods for CO_2 -related corrosion control have been developed. The use of surfactant inhibitors has received extensive attention in the oil and gas industry for corrosion inhibition of production and transportation pipes (metallic materials, such as steel and copper) in a way that surfactant molecules usually adsorb on steel surface and form a protective film which acts as a barrier to reduce corrosive media penetration and attack [1–4,8,9]. Inhibitor mixtures have been used in wide ranging applications due to their superior physicochemical properties and capabilities

in efficient solubilization, adsorption, and transportation [4,10,11]. Inhibitor mixtures can often be conveniently tuned to achieve desired properties by adjusting surfactant type and mixture ratios [12]. More surface-active and expensive inhibitors are often mixed with less surface-active and cheaper inhibitors to reduce cost [4,5]. Many of the organic inhibitors, are surfactant molecules with hydrophilic and hydrophobic molecular sections, which increases the complexity of their interactions in water-oil-steel pipe (WOS) environments.

The hydrophilic portion of surfactant strongly favors interactions with polar entities such as water, metals, and ions, which facilitates surfactant aggregation and surfactant adsorption on metal surfaces, blocks active surface sites, and thereby protects metal from corrosion [8,9]. On the other hand, surfactant molecules tend to escape from polar aqueous phase by associating and aggregating hydrocarbon chains together because of hydrophobicity [9,13].

When an aqueous solution containing surfactant comes into contact with an immiscible organic liquid in one environment, such as water-oil interface, surfactant monomers with longer hydrocarbon chains prefer partitioning into the organic liquid until equilibrium is reached [14–19], which usually reduces the availability of surfactant monomers in the aqueous phase for adsorption on the metal surface and for corrosion inhibition. The partitioning is usually characterized by the partitioning coefficient, which

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Nomenclature		
List of symbols		
	Electron affinity	
$\frac{A_{\mathrm{e}}}{A}$	A vector of regression coefficients specific to surfac-	
	tant/mixture and solution conditions	
\vec{A}'	A modified vector of regression coefficients	
\bar{B}	A regression constant	
$ar{m{B}}'$	A modified regression constant	
$C_{\rm c}$	The concentration of counterion dissociated from	
	electrolyte salt and from ionic surfactant in aqueous	
6	solution	
$C_{\rm m}$	The average concentration of total monomeric sur-	
C	factant in WOS environments The mole concentration of oil	
$C_{ m mo}$ $C_{ m mw}$	The mole concentration of water	
C_{tol}	The initial concentration (not at equilibrium) of total	
Ctol	surfactant added to aqueous phase	
$C_{\mathrm{m}}^{\mathrm{o}}$	The concentration of total monomeric surfactant in	
-111	oil phase	
$C_{\rm mi}^{\rm o}$	The concentration of monomeric surfactant 'i' in oil	
1111	phase	
$C_{\mathrm{m}}^{\mathrm{w}}$	The concentration of total monomeric surfactant in	
	aqueous phase	
$C_{\mathrm{mi}}^{\mathrm{w}}$	The concentration of monomeric surfactant 'i' in	
-	aqueous phase	
<u></u>	The overall average concentration of total surfactant	
E	in water and oil phases	
Ecorr	Open circuit potential Energy of highest occupied molecular orbital	
$E_{ m HOMO} \ E_{ m ip}$	Ionization potential	
E_{HOMO}	Energy of lowest unoccupied molecular orbital	
$f_{\rm i}$	Activity coefficient of surfactant 'i' in micelles	
i	Arbitrary surfactant	
ia	Anodic current density	
i_{C}	Cathodic current density	
i_{corr}	Corrosion current density with surfactant inhibitors	
	in solution	
i _{meas}	Measured current density	
i_{ocorr}	Corrosion current density without surfactant	
	inhibitors in solution	
j v	Arbitrary counterion	
K _{ad} K _i	Equilibrium adsorption constant The partitioning coefficient of pure surfactant 'i'	
K_{mix}	The apparent partitioning coefficient of surfactant	
rmix	mixture	
<i>K'</i>	A constant equal to the equilibrium adsorption con-	
	stant K_{ad} multiplied by Γ^{w}	
$M_{\rm ad}$	The surfactant adsorbed on steel surface and	
	water/oil interface	
$M_{\rm o}$	The surfactant (both monomeric and micellar	
	forms) distributed in the oil phase	
$M_{ m tol}$	The total quantity of surfactant added to the WOS	
	environments	
M_{W}	The surfactant (both monomeric and micellar	
ō	forms) distributed in the water phase	
Q	A vector of quantum chemical descriptors for a par-	
R	ticular surfactant or surfactant mixture	
$R_{\rm p}$	Gas constant Polarization resistance in the presence of surfactant	
R_{po}	Polarization resistance in the absence of surfactant	
T _{po}	Temperature	
V_0	Volume of oil phase	
$V_{\rm W}$	Volume of water/aqueous phase	
-		

ν.	The mole fraction of surfactant 'i' in total surfactant
x_{i}	mixture in bulk solution
$X_{\rm mi}^{\rm o}$	The mole fraction of surfactant 'i' in total amount of
⁷¹ mi	molecules in oil phase
χW	The mole fraction of surfactant 'i' in total amount of
$X_{\rm mi}^{\rm w}$	molecules in oil phase
X_{j}^{w}	The mole fraction of counter 'j' in total amount of
Λj	molecules in water phase
	A
αί	The mole fraction of surfactant 'i' in mixed micelles
,	at partitioning and adsorption equilibrium
α_{i}	The mole fraction of surfactant 'i' in mixed micelles
ρ	without partitioning process
β_a	Anodic tafel slope
$\beta_{\rm c}$	Cathodic tafel slope The mean activity coefficient of counterion
γ _c	Activity coefficient of monomeric surfactant 'i' in oil
$\gamma_{\rm mi}^{\rm o}$	phase
a.W	Activity coefficient of monomeric surfactant 'i' in
$\gamma_{\rm mi}^{\rm w}$	water phase
W	•
$\gamma_{\rm mj}^{\rm w}$	Activity coefficient of counterion 'j' in water phase
$\Gamma_{ m app}$	The apparent cmc of surfactant mixture which is
	defined as the average concentration of mixed sur-
	factants at which mixed micelles start to form in
П	WOS environments
$\Gamma_{ m app,i}$	The apparent cmc of surfactant 'i' which is defined
	as the concentration of surfactant at which micelle
П0	starts to form in WOS environments
I_{i}^{o}	The cmc value of surfactant 'i' in oil phase
$\begin{array}{c} \varGamma_i^o \\ \varGamma_i^p \\ \varGamma^w \end{array}$	The cmc of surfactant 'i' in pure water
Γ^{w}	The cmc value of surfactant mixture in aqueous
	phase
$\Gamma_{ m i}^{ m w} \ \delta_{ m i}$	The cmc value of surfactant 'i' in aqueous phase
$\delta_{\rm i}$	An experimental constant that is interpreted as the
	counterion binding coefficient with respect to sur-
0	factant 'i'
$\delta_{ m j}$	The binding coefficient to micelles with respect to
4.5	counterion 'j'
ΔE	Energy difference between HOMO and LUMO
ΔN	The fraction of electrons transferred from the sur-
	factant to the steel surface
$\Delta\mu_{ ext{tri}}^{ ext{o}}$	The standard free energy change of surfactant 'i'
~	transferring from water to oil
Υ	Global handress
$\gamma_{\rm inh}$	Global hardness of surfactant molecule
γ_{mel}	Global hardness of metals (electrodes)
$\eta(\%)$	Corrosion inhibition efficiency
0	The effective surface coverage and assumed to be
m	equal to corrosion inhibition The chamical potential of surfactant 'i' in mixed.
μ_{i}^{m}	The chemical potential of surfactant 'i' in mixed
,,0	micelles The chemical potential of monomeric surfactant 'i'
μ_{i}^{o}	
,,0,0	in oil phase The standard chemical potential of monomeric sur-
$\mu_{\rm i}^{\rm o,o}$	The standard chemical potential of monomeric sur- factant 'i' in oil/organic phase
$\mu_{\rm i}^{ m pm}$	factant 'i' in oil/organic phase The chemical potential of surfactant 'i' in pure
μ_{i}	The chemical potential of surfactant 'i' in pure micelles
,,W	The chemical potential of monomeric surfactant 'i'
μ_{i}^{w}	in water phase
$\mu_{\mathrm{i}}^{w,o}$	The standard chemical potential of monomeric sur-
μ_{i}	factant 'i' in water/aqueous phase
μ_{i}^{w}	The chemical potential of counterion 'j' in water
$\sim_{\rm j}$	phase
	Printe

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