



Short communication

## Nanohardness and elastic anisotropy of ZrB<sub>2</sub> crystals

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### ABSTRACT

Room temperature instrumented nano-indentation with a Berkovich tip was carried out on polycrystalline ZrB<sub>2</sub>. The orientation of the individual grains was mapped using electron backscattered diffraction. The anisotropy in properties was ~20% and ~7% for nanohardness and indentation modulus, respectively. The nanohardness decreased from basal towards prismatic orientation with a minimum at ~50–60° and the indentation modulus increased with a maximum at ~70–80°. The indentation modulus anisotropy, calculated by Vlassak-Nix model, shows similar tendency as the experimental values.

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## 1. Introduction

Ultra-high temperature ceramics (UHTC) are a family of materials that are chemically and physically stable at very high temperatures. They are usually based on the refractory borides, carbides, nitrides and oxides of early transition metals [1,2]. Zirconium diboride (ZrB<sub>2</sub>) is an important member of the UHTCs family due to its high melting point (>3000 °C), high oxidation resistance above 1500 °C and excellent thermal and electrical conductivity. These properties make ZrB<sub>2</sub> an ideal candidate to withstand extreme chemical and thermal environments, including hypersonic flight [3].

Zirconium diboride is a non-oxide ceramic with hexagonal structure, (space group P6/mmm, No. 191) with lattice parameters of  $a = 3.170 \text{ \AA}$  and  $c = 3.53 \text{ \AA}$ , respectively [4]. The individual grains within the polycrystalline ZrB<sub>2</sub> are essentially single crystals with orientation-dependent mechanical properties. It is necessary to understanding this orientation dependence in order to optimize microstructures containing grains with desired orientations to design composites having enhanced combinations of hardness, toughness and wear resistance [5]. The mechanical properties of ZrB<sub>2</sub> crystals, similarly to other materials, are not absolutely the same at micro or nano levels compared with their macroscopic counterparts due to the different internal defect structure (dislo-

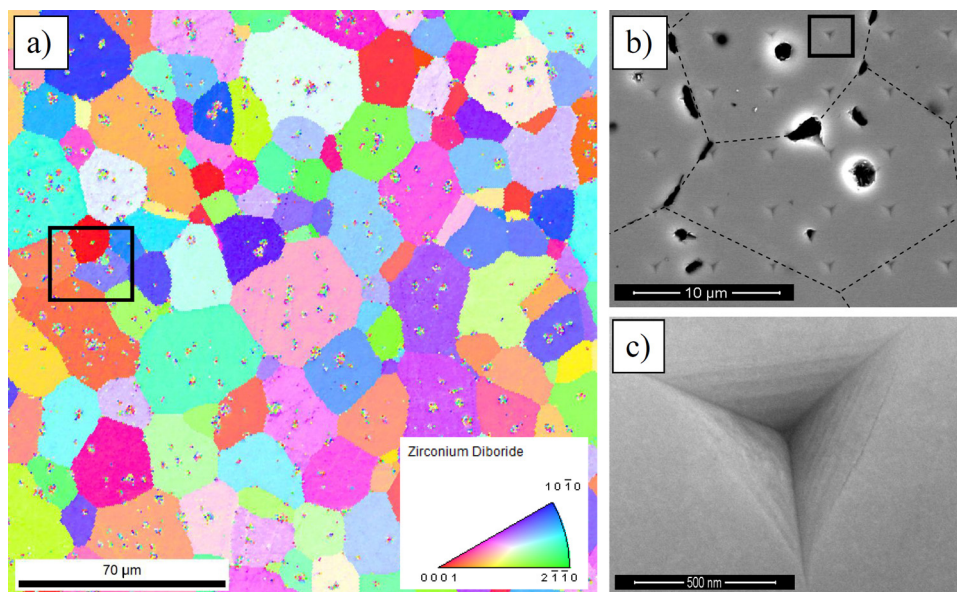
cations, impurities, etc.). Thus, direct measurements are necessary to be performed on the grains in that condition as they are in presence in polycrystalline ZrB<sub>2</sub> instead of on properly oriented single crystals.

In the past, several investigations focused on the understanding of the orientation dependence of microhardness and the possible deformation mechanisms at room and elevated temperatures in ZrB<sub>2</sub> single crystals [6–9]. Xuan et al. [6] performed Vickers microhardness measurements on ZrB<sub>2</sub> single crystals, on basal (0001), and the prismatic (10 $\bar{1}0$ ) and (11 $\bar{2}0$ ) planes at room and elevated temperatures up to 1000 °C. According to their results, the hardness was very similar on both types of prismatic planes and lower than on the basal plane. A similar result was reported in the work of Nakano et al. [7] who used Knoop indentation testing. They reported a slight hardness anisotropy (~15%) for ZrB<sub>2</sub> single crystal, which was explained by activation of the {10 $\bar{1}0$ } {11 $\bar{2}0$ } slip system based on the critical shear stress analysis of Daniels and Dunn [8]. Later TEM investigations clearly identified {10 $\bar{1}0$ } {11 $\bar{2}0$ } type slip, which is typical for hexagonal crystals, as the only responsible mechanism for room-temperature plastic deformation in single crystal ZrB<sub>2</sub>, [9].

Recent scratch [10–12] and indentation [13,14] investigations on polycrystalline ZrB<sub>2</sub> and ZrB<sub>2</sub>-SiC composites have also revealed readily detectable plastic deformation features in the form of slip-lines. Ghosh et al. inferred {10 $\bar{1}0$ } {11 $\bar{2}0$ } type slip activation by TEM observation and reported for the first time a [0001] type Burgers vector in ZrB<sub>2</sub> grains, which possibly corresponds to the {10 $\bar{1}0$ } [0001] system, [11]. Performing low-load indentation,

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**Fig. 1.** Characteristic maps of polycrystalline  $ZrB_2$  made by (a) EBSD prior to indentation; (b) SEM on a particular part of the indented surface (grain boundaries are marked together with; (c) a selected indent located in grain close to basal orientation.

Guicciardi et al. [14] observed pop-in phenomena in  $ZrB_2$ –SiC composite when indents were placed inside  $ZrB_2$  grains.

While the mechanisms of plastic deformation of  $ZrB_2$  have been widely studied in single crystals and also in polycrystalline  $ZrB_2$  ceramics, the orientation dependence (anisotropy) of hardness and elastic properties of single crystals or polycrystalline  $ZrB_2$  have not been reported.

The aim of the present work was to study the influence of grain orientation on the nanoindentation hardness and indentation modulus of polycrystalline  $ZrB_2$  ceramic to reveal the anisotropy of the elastic and plastic properties.

## 2. Experimental

The experimental material was a spark plasma sintered (SPS)  $ZrB_2$  sample prepared by two steps SPS process. The starting material was a  $ZrB_2$  powder with average grain size of  $2.4\ \mu\text{m}$  (Starck, Germany) containing impurities of C 0.13; O 0.8; N 0.21; Hf 1.77 wt%. All of the experiments were carried out using an SPS furnace (FCT HPD 25; FCT Systeme GmbH) under vacuum (5 Pa). In the first step, the cold pressed material (10 MPa for 1 min) was subjected to pressure-less sintering at  $1900\ ^\circ\text{C}$  for 20 min and cooled down at  $100\ ^\circ\text{C}/\text{min}$ . In the second step, the sample was heated up to  $1700\ ^\circ\text{C}$  (heating rate of  $100\ ^\circ\text{C}/\text{min}$ ) under constant pressure of 16 MPa, which followed by an additional heating up to  $2100\ ^\circ\text{C}$  (heating rate of  $50\ ^\circ\text{C}/\text{min}$ ) under a linearly increasing pressure up to 60 MPa. The sample was dwelled for 20 min and then cooled to room temperature at  $100\ ^\circ\text{C}/\text{min}$ .

The microstructure parameters were determined using standard ceramographic procedures (cutting, grinding, polishing, etching), SEM observation (FEI Quanta 3D and JEOL JSM 7000F) and statistical analyses [15]. Before nanoindentation the  $ZrB_2$  sample was subjected to EBSD investigation on a FEI Quanta 3D to determine the crystal orientation of the individual  $ZrB_2$  grains.

Nanoindentation tests were carried out at room temperature on an Agilent G200 Nano Indenter operating in continuous stiffness measurement (CSM) mode using a brand new diamond Berkovich tip. The tip was calibrated prior to the measurements using a fused silica sample. Nanoindentation was performed with a maximum penetration depth of 200 nm and strain rate of  $0.05\ \text{s}^{-1}$ . The

indentation depth was selected to be as small as possible but be in possession of a well developed plastic zone close to the tip with a surrounding elastic region. According to the general rule of nanoindentation, the distance between the indents should be cca. triple of their diameter ( $d$ ), which is  $d \sim 1.3\ \mu\text{m}$  in the present case, to avoid the interaction of their stress fields. Thus, indents were positioned on the previously EBSD mapped surface area, in a  $30 \times 30$  array with distance of  $4\ \mu\text{m}$  between the indents. The hardness and indentation modulus was calculated according to the Oliver Pharr method [16] using Poisson ratio and Young's modulus values of  $\nu_{ZrB_2} = 0.26$ ,  $\nu_i = 0.07$  and  $E_i = 1140\ \text{GPa}$  for  $ZrB_2$  and diamond indenter tip, respectively. The measured hardness and modulus values were almost constants in the depth region of 50–200 nm which confirmed the selection of 200 nm.

The crystal orientations of the indented  $ZrB_2$  grains were determined on the basis of the measured EBSD map using the OIM software, which defines the crystal orientations in terms of Euler angles ( $\varphi_1, \Phi, \varphi_2$ ) relative to the sample coordinate system [17]. Only those indents that were located inside the grains farther than  $2\ \mu\text{m}$  from the grain boundaries, inclusions and pores observed by SEM were taken into account. The averaged hardness and modulus values, deriving from the depth range of 150–200 nm, were paired with the corresponding grain orientation as a function of the relevant Euler angles  $\Phi$  and  $\varphi_2$ , due to the assumed rotational symmetry of nanoindentation [17].

## 3. Results and discussion

The characteristic microstructure of the investigated  $ZrB_2$  is shown in Fig. 1a,b. Fig. 1a is an EBSD image of the particular surface area where the indentation testing was carried out. It shows a wide range of grain orientations, which provided a suitable area for the orientation dependence analysis. The majority of the  $ZrB_2$  grain diameters fall into the range of 10–40  $\mu\text{m}$ . Fig. 1b shows the microstructure of the  $ZrB_2$  ceramics along with the indentation impressions. There are micro-pores at the triple point, grain boundaries and also located within the grains with diameters up to several micrometers. From Fig. 1b, which the selected area marked in Fig. 1a, it is evident that the grains size is large enough to guarantee statistically low probability of interaction between the indents

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