

# In situ synthesis and densification of submicrometer-grained $B_4C$ – $TiB_2$ composites by pulsed electric current sintering

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## Abstract

$B_4C$  composites with 15 and 30 vol%  $TiB_2$  were pulsed electric current sintered from  $B_4C$ – $TiO_2$ –carbon black mixtures in vacuum at 2000 °C. Full densification could be realised when applying an optimized loading cycle in which the maximum load is applied after completion of the  $B_4C$ – $TiB_2$  powder synthesis, allowing degassing of volatile species. The influence of the sintering temperature on the phase constitution and microstructure during synthesis and densification was assessed from interrupted sintering cycles. The in situ conversion of  $TiO_2$  to  $TiB_2$  was a complex process in which  $TiO_2$  is initially converted to  $TiB_2$  with  $B_2O_3$  as intermediate product at 1400–1700 °C. At 1900–2000 °C,  $B_2O_3$  reacted with C forming  $B_4C$  and CO. The  $B_4C$  and  $TiB_2$  grain size in the fully densified 30 vol%  $TiB_2$  composite was 0.97 and 0.63  $\mu m$ , combining a Vickers hardness of 39.3 GPa, an excellent flexural strength of 865 MPa, and modest fracture toughness of 3.0  $MPa m^{1/2}$ .

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## 1. Introduction

As one of the hardest materials known, boron carbide ranks third behind diamond and cubic boron nitride. Being intrinsically brittle,  $B_4C$  often requires different additives to improve its sintering behaviour and mechanical properties. Numerous researchers have shown that the addition of  $TiB_2$  to  $B_4C$  can decrease the porosity level and improve the fracture toughness as well as flexural strength.<sup>1–6</sup> Furthermore, dense  $B_4C$ – $TiB_2$  composites can be easily machined using electrical discharge machining (EDM) since  $TiB_2$  has a good electrical conductivity.<sup>7–10</sup> Since both  $B_4C$  and  $TiB_2$  are covalently bonded compounds, sintering temperatures above 2200 °C were required for pressureless sintering of  $B_4C$ – $TiB_2$  particulate composites.<sup>1,3</sup> However, rapid grain growth and concomitantly decreased strength were observed in pressureless liquid phase sintered  $B_4C$ – $TiB_2$  composites. A recent study showed that hot pressing and pulsed electric current sintering aided in increasing the density of  $TiB_2$  while decreasing the sintering time.<sup>11,12</sup>

Another way to make  $B_4C$ – $TiB_2$  composites is via in situ reaction of  $TiO_2$ , carbon and  $B_4C$ <sup>3–5</sup> or from elemental powders.<sup>13</sup> A flexural strength of 866 MPa and fracture toughness of 3.2  $MPa m^{1/2}$  were reported for fully dense  $B_4C$ –20 mol% (15 vol%)  $TiB_2$  composites made from  $B_4C$ ,  $TiO_2$  and carbon black mixtures prepared by reaction hot pressing for 1 h at 2000 °C under a pressure of 50 MPa.<sup>5</sup> In situ  $TiB_2$  formation is reported when sintering  $B_4C$  with  $TiO_2$  or Ti addition in the 1800–2190 °C range.<sup>14</sup> A mixture of fine-sized  $B_4C$  with 40 wt%  $TiO_2$  was transformed into a 95% dense  $B_4C$ – $TiB_2$  composite when sintering for 1 h at 2160 °C.<sup>14</sup> More recently, pseudo-eutectic micrometer grained  $TiB_2$ – $B_4C$  composites were synthesized by PECS of mechanically alloyed elemental powders at 1200–1700 °C.<sup>13</sup> Phase formation was completed well before full density was achieved and bulk composite materials of nearly full density were obtained when PECS at 1700 °C.<sup>13</sup>

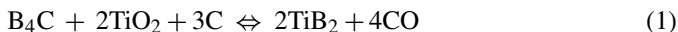
In the present study,  $B_4C$ – $TiB_2$  composites with up to 30 vol%  $TiB_2$  were made by in situ synthesis from  $B_4C$ ,  $TiO_2$  and carbon black powder mixtures during densification by pulsed electric current sintering (PECS). The effect of the processing temperature on the densification, phase constitution, as well as microstructure of the sintered compacts was assessed.

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## 2. Experimental procedure

### 2.1. Material preparation

B<sub>4</sub>C–TiB<sub>2</sub> composites were made by in situ reaction of B<sub>4</sub>C (Grade HD20, H.C. Starck, Germany,  $d_{50}$  = 0.5 μm), TiO<sub>2</sub> (Grade A-HR, Huntsman Tioxide Europe Ltd., crystal size = 0.17 μm) and carbon black (Grade 4, Degussa; Germany) powders. Composites B15T and B30T with a desired TiB<sub>2</sub> content of 15 and 30 vol% respectively were prepared by low energy multidirectional mixing (Turbula T2A, WAB, Switzerland) in ethanol for 24 h using ZrO<sub>2</sub> milling balls ( $\phi$  = 5 mm, grade TZ-3Y, Tosoh, Japan). The solvent was removed in a rotating evaporator at 65 °C and the powder mixture was additionally dried for 24 h at 80 °C. The starting compositions were determined so as to form B<sub>4</sub>C matrix composites with 15 or 30 vol% TiB<sub>2</sub>, which have a theoretical density of 2.82 and 3.12 g/cm<sup>3</sup> respectively, according to the rule of mixtures based on a density of 2.52 and 4.52 g/cm<sup>3</sup> for B<sub>4</sub>C and TiB<sub>2</sub>. The formation of TiB<sub>2</sub> phase can be described according to<sup>3,4</sup>:



Under standard state conditions, the change in Gibbs free energy of this reaction can be expressed as:  $\Delta G = 732.7 - 6.5 T$  (kJ), which is thermodynamically favourable at temperatures above 1150 °C.<sup>14</sup> Reaction (1) proceeds more rapidly when the CO partial pressure is below the equilibrium pressure, i.e. in vacuum or Ar atmosphere. In the absence of free carbon, TiO<sub>2</sub> can be converted to TiB<sub>2</sub> using B<sub>4</sub>C as carbon source.<sup>14–17</sup>

In the present study, in situ powder synthesis and sintering was performed during PECS (Type HP D 25/1, FCT Systeme, Rauenstein, Germany) in a vacuum of 4 mbar. A pulsed electric current was applied with a pulse duration of 10 ms and pause time of 5 ms throughout all the experiments. Powder mixtures were poured into a cylindrical graphite die with an inner and outer diameter of 30 and 56 mm. The B30T powder mixture was PECS at 1400, 1700, 1900 and 2000 °C for 5–13 min, including outgassing, pressure loading and dwell time at the sintering temperature, under a maximum pressure of 60 MPa, with a heating and initial cooling rate of 200 °C/min. A representative thermal cycle is given in Fig. 1 for the powder mixture heated for 9 min at 2000 °C. In all experiments, a minimum pressure of 8 MPa was applied to ensure constant contact of the electrodes with the die/punch/sample system. Two different loading cycles were investigated. In loading cycle C1, the pressure was gradually increased from 8 to 60 MPa within 1 min upon reaching 2000 °C. In the optimized cycle C2, the maximum pressure of 60 MPa was applied within 1 min, 4 min after reaching 2000 °C allowing degassing of volatile species. Graphite paper was used to separate the graphite die/punch set-up and powder mixture. A 10 mm thick porous carbon felt insulation was placed around the graphite die to obtain a homogeneous temperature distribution and concomitant sintering behaviour. The sintering temperature was measured by a two-colour pyrometer (400–2300 °C, Impac, Chesterfield, UK), focused at the bottom of a central borehole in the upper punch, 2 mm away from the top surface of the sam-

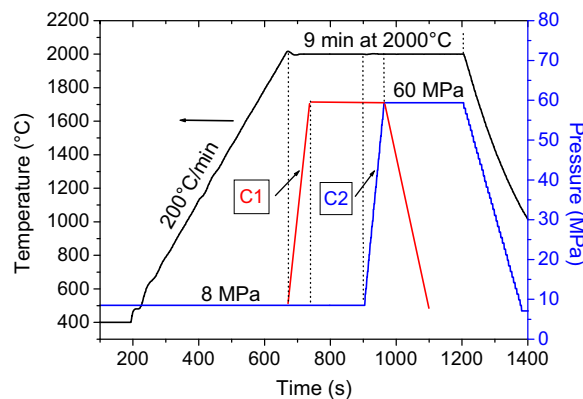


Fig. 1. Thermal and mechanical loading cycles during in situ synthesis and consolidation of B<sub>4</sub>C–TiO<sub>2</sub>–C starting powder mixtures without (C1) and with (C2) a degassing step upon reaching the targeted sintering temperature.

ple. The actual set-up and temperature monitoring procedure is described in detail elsewhere.<sup>18</sup>

### 2.2. Characterization

After PECS and sand blasting, the sintered 4 mm thick discs were cross-sectioned and polished to a mirror finish. The bulk density of the sintered composites was measured in ethanol. The crystalline phases during the reaction were investigated by a  $\theta$ – $\theta$  X-ray diffractometer (XRD, Seifert, Ahrensburg, Germany) using Cu–K $\alpha$  radiation (40 kV, 40 mA). The microstructure and composition of the PECS materials were examined by scanning electron microscopy (SEM, XL30-FEG, FEI, Eindhoven, the Netherlands), equipped with an energy dispersive analysis system (EDS, EDAX, Tilburg, the Netherlands) for compositional analysis. The Vickers hardness, HV<sub>1</sub>, was measured (Model FV-700, Future-Tech Corp., Tokyo, Japan) with an indentation load of 9.81 N. The fracture toughness, K<sub>IC</sub>, was calculated from the length of the radial cracks of the indentations according to the formula of Anstis et al.<sup>19</sup> The elastic modulus,  $E$ , of the B<sub>4</sub>C–TiB<sub>2</sub> composites was measured on rectangular bars by the resonance frequency method.<sup>20</sup> The resonance frequency was measured by the impulse excitation technique (Grindo-Sonic, Lemmens N.V., Leuven, Belgium). The flexural strength at room temperature was measured in a three-point bending test (Series IX Automated Materials Testing System 1.29, Instron Corporation) with a span width of 20 mm and a crosshead displacement of 0.1 mm/min on rectangular (25 mm × 3 mm × 2 mm) bars, which were cut from the PECS discs by electrical discharge machining. All surfaces were ground (grinding wheel type D46SW-50-X2, Technodiamant, The Netherlands) on a Jung grinding machine (JF415DS, Göppingen, Germany). The reported flexural strength values are the mean and standard deviation of five measurements.

## 3. Results and discussion

### 3.1. In situ synthesis of B<sub>4</sub>C–TiB<sub>2</sub> powder

In the present study, a heating rate of 200 °C/min was applied to in situ synthesize TiB<sub>2</sub> and densify B<sub>4</sub>C–TiB<sub>2</sub> composite

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