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Journal of Non-Crystalline Solids





JOURNAL OF NON-CRYSTALLINE SOLIDS

# Elastic moduli of borosilicate glasses doped with heavy metal oxides

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#### ARTICLE INFO

Article history: Received 16 September 2013 Received in revised form 21 January 2014 Available online 7 February 2014

Keywords: Amorphous materials; Glasses; Structural materials; Ultrasonic measurements; Elastic properties

## ABSTRACT

Comparative studies on the theoretical and experimental values of elastic moduli of the borosilicate glasses (70-*x*) SiO<sub>2</sub>–30B<sub>2</sub>O<sub>3</sub>–*x*HMOs glass system, where HMOs (heavy metal oxides) are TiO<sub>2</sub>, BaO and Bi<sub>2</sub>O<sub>3</sub> with 0, 1, 2, 3, 4 and 5 mol% of each HMO, were investigated. Elastic moduli were assessed by measuring the ultrasonic velocities. The number of network bonds per unit volume, the average of a stretching force constant, the average of cross-link density, the average of ring diameter and the theoretical bond compression bulk modulus were calculated by using a theoretical bond compression model to confirm the obtained results from the experiments. The results show that changes in the structure of the glass depend on a type and concentration of HMOs. Moreover, the experimental elastic moduli are in good agreement with the theoretical values.

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#### 1. Introduction

Glass is a solid material of interest because it is transparent to visible light and is a good insulator. Of specific interest for a glass material, borosilicate glasses have high chemical and mechanical resistance, very low electrical conductivity and thermal expansion coefficient. Thus, they are widely used in laboratory, optical, heat-resistant, fiber, pharmaceutical and sealing glass applications, and even for nuclear waste immobilization [1–4].

Elastic properties are very informative regarding the structures of glasses and they are directly related to the interatomic potentials. The glasses are isotropic and have only two independent elastic constants: longitudinal and shear moduli. These parameters are obtained from calculating the longitudinal and shear velocities and the densities of the glasses. The bulk modulus, Young's modulus and Poisson's ratio can also be deduced. The elastic moduli of borosilicate glasses containing transition, rare earth and/or heavy metal oxide (HMO) depend on ultrasonic waves at room temperature and were previously reported by several groups [4–15].

The glasses based on heavy metal oxides (HMOs) such as BaO,  $Bi_2O_3$ , PbO, TiO<sub>2</sub>, Ag<sub>2</sub>O, etc. have always been an area of interest because of their characteristic structural and physical properties such as high refractive index, high thermal expansion, high density, low transformation temperature and excellent infrared transmission (IR). Therefore, these glasses have been desirable aspirants for potential applications in IR technologies, design of laser devices and non-linear optics [16,17]. Among HMO glasses, bismuth and/or barium borosilicate glasses are the subject of growing and intense research. The glasses containing BaO and/or  $Bi_2O_3$  have attracted considerable attention because

\* Corresponding author. *E-mail address:* cherdsak\_per@hotmail.co.th (C. Bootjomchai). of their vast range of applications in the fields of radiation shielding, glass-ceramics, reflecting windows, thermal and mechanical sensors, etc. [18–20]. In addition, the glasses containing significant concentrations of transition metal oxides (TMOs) such as TiO<sub>2</sub>, ZnO, Fe<sub>2</sub>O<sub>3</sub>, V<sub>2</sub>O<sub>5</sub>, MnO<sub>2</sub>, etc. are of continuing interest because of their applicability in memory switching, electrical threshold, optical switching devices, etc. [21–25].

In this work, the elastic moduli of borosilicate glasses will be discussed. Information regarding the number of network bonds per unit volume, the average of stretching force constant, the average of ring size diameter and the average of the cross-link density will be examined and discussed. The theoretical values of bond compression bulk modulus and elastic moduli will be calculated and compared with the experimental values.

#### 2. Materials and methods

#### 2.1. Preparation of glass samples

Rectangular shaped glass samples of the  $(70-x)SiO_2-30B_2O_3-xHMOs$  glass system (where HMOs are TiO<sub>2</sub>, BaO and Bi<sub>2</sub>O<sub>3</sub> with 0, 1, 2, 3, 4 and 5 mol% of each HMO) were prepared by the conventional melting technique. The oxides of SiO<sub>2</sub>, B<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, BaO and Bi<sub>2</sub>O<sub>3</sub> used in this work were of an analytical regent grade. To prepare the glass samples, appropriate amounts of SiO<sub>2</sub>, B<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, BaO and Bi<sub>2</sub>O<sub>3</sub> were weighed using an electronic balance with the accuracy of the order of 0.0001 g. The homogeneous mixtures were placed in ceramic crucible and melted in an electric furnace until homogeneity of the glass melt was ensured. The melted glasses were poured into graphite molds and annealed for 2 h before naturally cooling down to room temperature.

<sup>0022-3093/\$ -</sup> see front matter © 2014 Elsevier B.V. All rights reserved. http://dx.doi.org/10.1016/j.jnoncrysol.2014.01.039

[27]:

### 2.2. Density and molar volume measurements

The densities of the glass samples were determined by Archimedes' principle, using n-hexane as an immersion liquid and applying the relationship (1) [6]

$$\rho = \rho_L \left( \frac{W_a}{W_a - W_b} \right) \tag{1}$$

where  $\rho_L$  is density of the immersion liquid, and where  $W_a$  and  $W_b$  are the sample weights in air and in the immersion fluid, respectively. The experiment was repeated three times to obtain an accurate value for the density. The estimated error in these measurements was about  $\pm 0.015$  g cm<sup>-3</sup> (shown in Table 1). The molar volume ( $V_a$ ) was calculated from the expression  $V_a = \frac{M}{\rho}$ , where M is the molecular weight of the glass, which was calculated according to the relationship  $M = \sum x_i M_i$  [26], where  $x_i$  is the mole fraction of the component oxide iand  $M_i$  is its molecular weight. The glass packing density can be calculated from the following Eqs. (2)–(3) [7]

$$V_t = \frac{\rho}{M} \sum_i x_i V_i \tag{2}$$

where  $V_i$  is given by,

$$V_i = \frac{4\pi N_A}{3} \left( x r_M^3 + y r_O^3 \right) \tag{3}$$

where  $N_A$  is Avogadro's number, and where  $r_M$  and  $r_O$  are the ionic radii of the cation and anion of the oxide  $M_xO_y$ , respectively. The uncertainties in molar volume and packing density were acquired from experiments repeated three times of densities. The estimated error in these results was about  $\pm 0.200 \text{ cm}^3 \cdot \text{mol}^{-1}$  and  $\pm 0.003 \times 10^{-6} \text{ m}^3$ , respectively (shown in Table 1).

#### 2.3. Ultrasonic measurements and determination of elastic moduli

To measure the ultrasonic velocity in the glass samples, an ultrasonic flaw detector, SONATEST Sitescan 230, was used. The ultrasonic wave was generated from a ceramic transducer with a resonant frequency at 4 MHz and acting as a transmitter–receiver at the same time. The ultrasonic wave velocity ( $\nu$ ) can be calculated using the following Eq. (4) [5]:

$$\nu = \frac{2x}{\Delta t} \quad \left(cm \cdot s^{-1}\right) \tag{4}$$

Table 1

Glass composition, density ( $\rho$ ), molar volume ( $V_a$ ) and packing density ( $V_t$ ) of the glass samples.

where x is the sample thickness (cm) and $\Delta t$ is the time interval (s). The
measurements were repeated three times to check the reproducibility
of the data. The estimated error in the velocity measurements was
$\pm 23 \text{ m} \cdot \text{s}^{-1}$ for the longitudinal velocity and $\pm 11 \text{ m} \cdot \text{s}^{-1}$ for the
shear velocity. The elastic strain produced by a small stress can be de-
scribed by two independent elastic constants, $C_{11}$ and $C_{44}$ [27]. Elastic
moduli were calculated using the following standard relations $(5)-(10)$

Longitudinal modulus  $C_{11} = L = \rho v_L^2$ , (5)

Shear modulus 
$$C_{44} = G = \rho v_s^2$$
, (6)

Bulk modulus 
$$K = L - \frac{4}{3}G$$
, (7)

Young's modulus 
$$E = (1 + \sigma)2G$$
, (8)

Poisson's ratio 
$$\sigma = \frac{L-2G}{2(L-G)}$$
, (9)

Microhardness 
$$H = \frac{(1-2\sigma)E}{6(1+\sigma)}$$
, (10)

Debye temperature calculated from Eq. (11) [28]

$$\theta_D = \left(\frac{h}{k_B}\right) \left(\frac{32N_A}{4\pi V_a}\right)^{1/3} v_m,\tag{11}$$

where  $v_L$  and  $v_S$  are longitudinal and transverse velocities, respectively. *h* is Planck's constant,  $k_B$  is Boltzmann's constant,  $N_A$  is Avogadro's number, *z* is the number of atoms in the chemical formula and  $v_m$  is the mean ultrasonic velocity defined by the relationship (12) [29].

$$\nu_m = \left[\frac{3\nu_L^3 \nu_S^3}{\nu_L^3 + \nu_S^3}\right]^{1/3}$$
(12)

Softening temperature  $T_s$  is related to the ultrasonic velocity of shear waves  $v_s$  by Eq. (13) [4]

$$T_s = \frac{v_s M}{C^2 Z} \tag{13}$$

where *Z* is the number of atoms in the chemical formula and *C* is the constant of proportionality and equals 507.4  $m \cdot s^{-1} \cdot K^{1/2}$ . The

Sample no.	SiO2	B <sub>2</sub> O <sub>2</sub>	TiO <sub>2</sub>	BaO	Bi2O2	0	Va	$V_{t} \times 10^{-6}$
	(mol%)	(mol%)	(mol%)	(mol%)	(mol%)	$(g \cdot cm^{-3})$	$(\text{cm}^3 \cdot \text{mol}^{-1})$	(m <sup>3</sup> )
SO	70	30	0	0	0	2.548	24.704	0.485
S1-TiO <sub>2</sub>	70	30	1	0	0	2.547	24.287	0.498
S2-TiO <sub>2</sub>	70	30	2	0	0	2.572	23.821	0.512
S3-TiO <sub>2</sub>	70	30	3	0	0	2.594	23.390	0.526
S4-TiO <sub>2</sub>	70	30	4	0	0	2.614	22.985	0.540
S5-TiO <sub>2</sub>	70	30	5	0	0	2.634	22.585	0.555
S1—BaO	70	30	0	1	0	2.582	24.933	0.485
S2—BaO	70	30	0	2	0	2.600	25.023	0.488
S3—BaO	70	30	0	3	0	2.630	25.189	0.489
S4—BaO	70	30	0	4	0	2.647	25.381	0.489
S5—BaO	70	30	0	5	0	2.671	25.503	0.491
S1-Bi <sub>2</sub> O <sub>3</sub>	70	30	0	0	1	2.676	24.132	0.501
S2-Bi <sub>2</sub> O <sub>3</sub>	70	30	0	0	2	2.800	23.645	0.516
S3-Bi <sub>2</sub> O <sub>3</sub>	70	30	0	0	3	2.947	23.020	0.535
S4-Bi <sub>2</sub> O <sub>3</sub>	70	30	0	0	4	3.021	22.996	0.540
S5-Bi <sub>2</sub> O <sub>3</sub>	70	30	0	0	5	3.123	22.767	0.551
The uncertainty						$\pm 0.015$	$\pm 0.200$	$\pm 0.003$

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