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# Predicting glass transition and crystallization temperatures of silicate bioglasses using mixture designs

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#### A R T I C L E I N F O

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#### ABSTRACT

Mixture designs have been applied on bioglasses in the range 42–55%SiO<sub>2</sub>, 13.5–48%CaO, 10–35%Na<sub>2</sub>O, 0–5%P<sub>2</sub>O<sub>5</sub>, and 0–13.5%CaF<sub>2</sub> (mol%). This study focused on glass transition temperature ( $T_g$ ), crystallization temperature ( $T_c$ ) and working range (temperature gap between  $T_g$  and  $T_c$ ). The designs, elaborated from data obtained by Differential Thermal Analysis (DTA), consist of equations connecting the properties with the glass molar composition. Using this powerful mathematical method,  $T_g$ ,  $T_c$  and the working range of bioglasses can be precisely predicted and optimized. We found that a Na, P or F addition decreases  $T_g$ . Crystallization occurs at higher temperature when phosphorus is added in small quantity, due to network polymerization, although further addition induces a decrease of  $T_c$  related to a decrease of the overall strength of the glass network. Fluoride affects crystallization of both manners, depending on the calcium and sodium contents. Last, as a network modifier, Na lowers  $T_c$ . The widest working ranges are obtained for glasses with a large quantity of SiO<sub>2</sub>, CaO, and P<sub>2</sub>O<sub>5</sub> and a medium quantity of CaF<sub>2</sub>, allowing to reach a difference between  $T_c$  and  $T_g$  of up to 260 °C.

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#### 1. Introduction

Since 1969 and the discovery of Bioglass® 45S5 by L.L. Hench [1], bioactive glasses have been developed for medical application, due to their ability to form a hydroxyapatite layer and bond to bone. Shape forming of these materials is widely studied nowadays, giving a great importance to the working range  $T_c$ – $T_g$ . For instance, fabrication of coatings and porous tissue engineered scaffolds requires a viscous flow sintering and no crystallization [2,3]. Indeed, crystallization has been shown to decrease the bioactive properties of bioglasses [4,5]. An a priori mathematical estimation of these two temperatures would then be a real asset for processing such materials.

 $T_g$  and  $T_c$  values depend on several factors, the most important being the glass structure. Phosphosilicate glasses, a common kind of bioglasses, present an amorphous phase separation with small orthosphosphate domains dispersed in a silicate matrix [6]. <sup>29</sup>Si, <sup>31</sup>P and <sup>17</sup>O solid-state NMR spectroscopy confirmed the non existence of Si–O–P bonds in the 45S5 glass [7]. This glass separation induces the observation of two  $T_g$  and two  $T_c$  signatures [8,9]. Nevertheless, depending on the composition, the second  $T_g$  is not always distinguishable, since it could be combined with the first one in a composite glass transition, or hidden by the crystallization peak.

As a network disrupter, sodium is known to decrease both  $T_g$  and  $T_c$  values [10–12]. When added to the nominal glass composition, fluoride

tends to complex preferentially Ca<sup>2+</sup> and Na<sup>+</sup> cations [13–16], and thus lowers the glass transition temperature [8,17]. Molecular Dynamics (MD) calculations suggest that when incorporated, fluorine decreases the overall strength of the glass network, defined by the  $F_{net}$  parameter [14]. It is also worth noting that being thermally activated processes, both  $T_g$  and  $T_c$  are cooling rate, heating rate and sample form dependant [2,9].

About 20 years ago, Andersson described  $T_g$  as a linear function of the Na<sub>2</sub>O content in a six oxide system [11]. Arstila et al. also proposed several equations predicting glass transition and devitrification temperatures, depending on the measurement method [12]. They concluded on the existence of a relation between the working range, the glass composition and the nature of the main phase formed during crystallization. Recently, O'Donnell gathered results from several articles and established a new formula correlating  $T_g$  to bioglass molar composition [17]. His model, elaborated from data fitted thanks to Solver in OpenOffice, allows quite a good  $T_g$  approximation to be obtained, despite results extracted from a different methods (DTA, DSC, dilatometry).

In this paper we propose a different approach for  $T_g$  and  $T_c$  prediction by mixture designs [18]. This mathematical method, recognized for its great potential in mixtures and formulation, allows characteristic temperatures and composition of bioglasses belonging in a predefined domain to be related. Mixture designs have already been demonstrated to be a valuable prediction and optimization method for bioactive properties in a simple system [19]. Designs elaborated in this study focus on a predefined domain belonging to the SiO<sub>2</sub>–CaO–Na<sub>2</sub>O–P<sub>2</sub>O<sub>5</sub>–CaF<sub>2</sub> system. Phosphorus, as bone constituent, is

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#### Table 1

Molar composition of the 100 studied glasses. An \* before a glass name indicates a composition retained as checking glass.

| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$   | $\begin{array}{cccc} - & 6.75 \\ - & 6.75 \\ 2.50 & 6.75 \\ 2.50 & 6.75 \\ 2.50 & 6.75 \\ 2.50 & 6.75 \\ 2.50 & 6.75 \\ 2.50 & 6.75 \\ 5.00 & 6.75 $ |
|--|---|
| G2 55.00 13.50 31.50 - - G52 55.00 28.25 10.00   G3 55.00 35.00 10.00 - - *G53 55.00 20.88 17.38   G4 42.00 23.00 35.00 - - C54 42.00 38.75 10.00   G5 42.00 48.00 10.00 - - *G55 48.50 32.25 10.00   G6 42.00 35.50 22.50 - - *G56 55.00 19.63 16.13   G7 55.00 24.25 20.75 - - G57 55.00 13.50 22.25   G8 53.25 13.50 33.25 - - G58 55.00 25.75 10.00   G9 48.50 41.50 10.00 - - G59 42.00 36.25 10.00 | - 6.75<br>- 6.75<br>2.50 6.75<br>2.50 6.75<br>2.50 6.75<br>2.50 6.75<br>2.50 6.75<br>5.00 6.75<br>5.00 6.75<br>5.00 6.75<br>5.00 6.75<br>5.00 6.75  |
| G3 55.00 35.00 10.00 - - *G53 55.00 20.88 17.38   G4 42.00 23.00 35.00 - - C54 42.00 38.75 10.00   G5 42.00 48.00 10.00 - - *C55 48.50 32.25 10.00   G6 42.00 35.50 22.50 - - *G56 55.00 19.63 16.13   G7 55.00 24.25 20.75 - - G57 55.00 13.50 22.25   G8 53.25 13.50 32.55 - - G58 55.00 25.75 10.00   G9 48.50 41.50 10.00 - - G59 42.00 36.25 10.00  | - 6.75<br>2.50 6.75<br>2.50 6.75<br>2.50 6.75<br>2.50 6.75<br>2.50 6.75<br>5.00 6.75<br>5.00 6.75<br>5.00 6.75<br>5.00 6.75<br>5.00 6.75  |
| G442.0023.0035.00G5442.0038.7510.00G542.0048.0010.00*G5548.5032.2510.00G642.0035.5022.50*G5655.0019.6316.13G755.0024.2520.75G5755.0013.5022.25G853.2513.5033.25G5855.0025.7510.00G948.5041.5010.00G5942.0036.2510.00   | 2.50   6.75     2.50   6.75     2.50   6.75     2.50   6.75     2.50   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75   |
| G542.0048.0010.00*G5548.5032.2510.00G642.0035.5022.50*G5655.0019.6316.13G755.0024.2520.75G5755.0013.5022.25G853.2513.5033.25G5855.0025.7510.00G948.5041.5010.00G5942.0036.2510.00  | 2.50   6.75     2.50   6.75     2.50   6.75     2.50   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75   |
| G642.0035.5022.50*G5655.0019.6316.13G755.0024.2520.75G5755.0013.5022.25G853.2513.5033.25G5855.0025.7510.00G948.5041.5010.00G5942.0036.2510.00  | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$  |
| G7 55.00 24.25 20.75 - - G57 55.00 13.50 22.25   G8 53.25 13.50 33.25 - - G58 55.00 25.75 10.00   G9 48.50 41.50 10.00 - - C59 42.00 36.25 10.00   | 2.50   6.75     2.50   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75   |
| G8   53.25   13.50   33.25   -   -   G58   55.00   25.75   10.00     G9   48.50   41.50   10.00   -   -   G59   42.00   36.25   10.00  | 2.50   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75   |
| G9 48.50 41.50 10.00 G59 42.00 36.25 10.00   | 5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75     5.00   6.75   |
|  | 5.00   6.75     5.00   6.75     5.00   6.75   |
| *G10 46.75 18.25 35.00 G60 48.50 29.75 10.00   | 5.00 6.75<br>5.00 6.75  |
| G11 49.10 26.60 24.30 *G61 55.00 18.38 14.88   | 5.00 6.75   |
| G12 49.00 13.50 35.00 2.50 - G62 55.00 23.25 10.00   | 5.00 0.75   |
| G13 55.00 13.50 29.00 2.50 - G63 55.00 13.50 19.75   | 5.00 6.75   |
| G14 55.00 32.50 10.00 2.50 - *G64 42.00 25.00 23.70  | 2.50 6.80   |
| G15 42.00 20.50 35.00 2.50 - *G65 48.60 13.50 28.60  | 2.50 6.80   |
| G16 42.00 45.50 10.00 2.50 - G66 42.00 13.50 35.00   | 2.50 7.00   |
| G17 42.00 33.00 22.50 2.50 - G67 42.00 26.50 24.20   | - 7.30  |
| *G18 55.00 23.00 19.50 2.50 - *G68 49.10 13.50 30.10   | - 7.30  |
| *G19 52.00 13.50 32.00 2.50 - G69 42.00 13.50 30.50  | 5.00 9.00   |
| G20 48.50 39.00 10.00 2.50 - G70 42.00 13.50 35.00   | - 9.50  |
| *G21 45.50 17.00 35.00 2.50 - *G71 42.00 13.50 31.75   | 2.50 10.25  |
| *G22 48.60 25.10 23.80 2.50 - G72 42.00 13.50 33.00  | - 11.50   |
| G23 46.50 13.50 35.00 5.00 - G73 42.00 24.00 20.50   | - 13.50   |
| G24 55.00 13.50 26.50 5.00 - G74 42.00 34.50 10.00   | - 13.50   |
| G25 55.00 30.00 10.00 5.00 - G75 42.00 13.50 31.00   | - 13.50   |
| G26 42.00 18.00 35.00 5.00 - G76 48.50 28.00 10.00   | - 13.50   |
| G27 42.00 43.00 10.00 5.00 - *G77 48.50 20.75 17.25  | - 13.50   |
| G28 42.00 30.50 22.50 5.00 - G78 48.50 13.50 24.50   | - 13.50   |
| G29 55.00 21.75 18.25 5.00 - G79 55.00 21.50 10.00   | - 13.50   |
| G30 50.75 13.50 30.75 5.00 - G80 55.00 13.50 18.00   | - 13.50   |
| G31 48.50 36.50 10.00 5.00 - G81 55.00 17.50 14.00   | - 13.50   |
| G32 44.25 15.75 35.00 5.00 - *G82 42.00 22.75 19.25  | 2.50 13.50  |
| *G33 48.10 23.60 23.30 5.00 - G83 42.00 13.50 28.50  | 2.50 13.50  |
| *G34 43.50 15.00 35.00 5.00 1.50 G84 42.00 32.00 10.00   | 2.50 13.50  |
| G35 42.00 15.75 35.00 5.00 2.25 G85 48.50 25.50 10.00  | 2.50 13.50  |
| *G36 44.25 13.50 35.00 5.00 2.25 G86 48.50 13.50 22.00   | 2.50 13.50  |
| *G37 44.33 15.83 35.00 2.50 2.33 *G87 48.50 19.50 16.00  | 2.50 13.50  |
| *G38 45.17 16.67 35.00 - 3.17 G88 55.00 19.00 10.00  | 2.50 13.50  |
| *G39 42.00 17.00 35.00 2.50 3.50 *G89 55.00 13.50 15.50  | 2.50 13.50  |
| *G40 45.50 13.50 35.00 2.50 3.50 *G90 55.00 16.25 12.75  | 2.50 13.50  |
| G41 42.00 13.50 35.00 5.00 4.50 G91 42.00 29.50 10.00  | 5.00 13.50  |
| G42 42.00 18.25 35.00 - 4.75 G92 42.00 13.50 26.00   | 5.00 13.50  |
| G43 46.75 13.50 35.00 - 4.75 G93 42.00 21.50 18.00   | 5.00 13.50  |
| *G44 47.65 20.45 21.05 5.00 5.85 G94 48.50 23.00 10.00   | 5.00 13.50  |
| G45 47.90 21.70 21.80 2.50 6.10 *G95 48.50 18.25 14.75   | 5.00 13.50  |
| *G46 42.00 23.50 23.20 5.00 6.30 G96 48.50 13.50 19.50   | 5.00 13.50  |
| *G47 48.10 13.50 27.10 5.00 6.30 G97 55.00 16.50 10.00   | 5.00 13.50  |
| G48 48.15 22.95 22.55 - 6.35 G98 55.00 15.00 11.50   | 5.00 13.50  |
| G49 42.00 41.25 10.00 - 6.75 G99 55.00 13.50 13.00   | 5.00 13.50  |
| G50   48.50   34.75   10.00   -   6.75   *45S5   46.10   26.90   24.40   | 2.60 –  |

an important element in bioglasses and fluoride is known "to prevent and arrest caries" [20,21].

#### 2. Experimental methods

#### 2.1. Mixture designs: D-optimal designs

Preliminary feasibility tests have allowed the studied domain to be limited to the range: 42-55%SiO<sub>2</sub>, 13.5-48%CaO, 10-35%Na<sub>2</sub>O, 0-5%P<sub>2</sub>O<sub>5</sub>, 0-13.5%CaF<sub>2</sub> (mol%). Four constraints from a previous study have been retained: synthesis temperature, vitreous compounds, fast bioactive reaction, and non solubility [19]. Thus, SiO<sub>2</sub>, CaO and Na<sub>2</sub>O limit content values come from this previous paper. Phosphorus and fluoride were added in order to follow the same constraints except for synthesis temperature which has been increased to 1450 °C. In recent studies, authors prepared glasses below 40 mol% silica [16,22,23], but due to apparatus limitations and our preparation method, we limited our compositions to silica contents above this value.

Using five constituents, each content defined by an upper and lower limit, implies the resulting domain representation to be an irregular hyperpolyhedron (i.e. a 4D figure). The study of this extremely complicated volume implies two choices:

- The use of a mixture design dedicated software (JMP 5.1 [24]) in order to extract interesting compositions. The software selection agrees with Scheffé's proposal [25,26], as the 99 extracted points are 20 tops, 40 edges, 29 2D faces, 9 3D faces and the gravity center of the domain (Table 1).
- The selection of a fifth degree postulated model (a priori model), in order to minimize the difference between calculated and experimental temperatures (Eq. 1).

$$\begin{split} \Gamma(C) &= B_1 * X_1 + B_2 * X_2 + B_3 * X_3 + B_4 * X_4 + B_5 * X_5 + B_{12} * X_1 * X_2 + B_{13} * X_1 * X_3 \\ &+ B_{14} * X_1 * X_4 + B_{15} * X_1 * X_5 + B_{23} * X_2 * X_3 + B_{24} * X_2 * X_4 + B_{25} * X_2 * X_5 \\ &+ B_{34} * X_3 * X_4 + B_{35} * X_3 * X_5 + B_{45} * X_4 * X_5 + B_{123} * X_1 * X_2 * X_3 \\ &+ B_{124} * X_1 * X_2 * X_4 + B_{125} * X_1 * X_2 * X_5 + B_{134} * X_1 * X_3 * X_4 + B_{135} * X_1 * X_3 * X_5 \\ &+ B_{145} * X_1 * X_4 * X_5 + B_{234} * X_2 * X_3 * X_4 + B_{235} * X_2 * X_3 * X_5 + B_{245} * X_2 * X_4 * X_5 \\ &+ B_{345} * X_3 * X_4 * X_5 + B_{1234} * X_1 * X_2 * X_3 * X_4 + B_{1235} * X_1 * X_2 * X_3 * X_5 \\ &+ B_{1245} * X_1 * X_2 * X_4 * X_5 + B_{1345} * X_1 * X_3 * X_4 + B_{235} * X_1 * X_2 * X_3 * X_5 \\ &+ B_{1245} * X_1 * X_2 * X_4 * X_5 + B_{1345} * X_1 * X_3 * X_4 * X_5 + B_{2345} * X_2 * X_3 * X_4 * X_5 \\ &+ B_{12345} * X_1 * X_2 * X_3 * X_4 * X_5 + e \end{split}$$

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