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Modeling residual porosity in thick components consolidated by spark plasma sintering

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A constitutive model for densification during spark plasma sintering was adapted and applied to an aluminum–magnesium alloy to determine the effect of increasing sample thickness on residual porosity after sintering. The contributions of electromigration, sintering stresses and external load (on creep, diffusion and yielding) were all taken into consideration, as well as the effect of pressure on increasingly thick components. The results show that the overall description of the spark plasma sintering process agrees with the experimental results.

Keywords: Spark plasma sintering; Aluminum alloys; Sintering; Powder consolidation

Spark plasma sintering (SPS) has, over the past 20 years, come to light as a promising approach for rapid powder consolidation [1,2] and cladding operations [3–5]. This consolidation process involves rapidly heating the powder by electric current along with the simultaneous application of pressure. During compaction, the effective applied pressure within the compact generally decays with increasing thickness [6]. This pressure decay inside the sample is problematic for the fabrication of thicker samples, as it may lead to a gradient of porosity throughout the final microstructure, which would adversely affect the mechanical properties. Hence, prediction and parameter optimization aiming for the removal of any residual porosity in the compact is of paramount importance. The complex nature of the SPS process has led to attempts of modeling the various phenomena occurring during the sintering process [7–10]. Constitutive models have been derived by Olevsky and Froyen [7] describing the effects of electromigration, sintering stress and the external load on diffusion. An attempt is made herein to augment this constitutive model so as to predict the remaining porosity in samples with increasing thicknesses. This will facilitate determining the relationship between thickness and remaining porosity for a given system, and to contribute to the selection of sintering parameters that would allow the elimination of any residual porosity.

Commercial aluminum alloy 5356 powder (composition: 4.5–5.5 wt.% Mg; 0.4 wt.% Fe; 0.25 wt.% Si; 0.1 wt.% Zn; 0.1 wt.% Cu; 0.06–0.2 wt.% Cr, Mn, Ti) was sintered in an ISO-Carb85 graphite die using a Thermal Technology LLC 10-3 spark plasma sintering press. The powder particles were spherical in morphology, having a particle size distribution mean of 28 μm with a standard deviation of 16 μm. The powder was consolidated into pucks of 20 and 38 mm diameter with varying thicknesses. The overall die dimensions were as follows: the height of the smaller die (20 mm) was 40 mm, with a 15 mm wall thickness; and the height of the larger die (38 mm) was 46 mm, with a wall thickness of 17.5 mm. These die cavity sizes then allowed for approximately four times the volume of powder to be placed into the 38 mm diameter die compared to the 20 mm, with a slightly higher wall thickness affecting the thermal load of the sintering cycle. The heating rate was maintained at 100 °C min^{-1}, with a soaking time of 1 min at 500 °C for the 20 mm die and 1 min at 400 °C for the 38 mm die. A mechanical vacuum level of 6.0×10^{-2} torr was maintained prior to and throughout the sintering cycle. Temperature was measured using a C-type thermocouple placed in a hole, drilled to 2 mm from the surface of the sample, in the bottom punch. A preload pressure of 10 MPa by single-action pressing

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was applied and was then ramped to the maximum pressure of 50 MPa during the heating stage, which was maintained throughout the holding temperature. Cross-sections of the pucks were ground and polished using 240, 400, 600, 800 and 1200 grit SiC paper, followed by polishing with 3 and 1 micron diamond suspensions and a 0.05 micron colloidal silica suspension. The residual porosity of the sintered pucks was analyzed using a Nikon light optical microscope equipped with a Clemex Vision System. Reported experimental values were averaged from a minimum of 10 image fields across the sample from a minimum of three samples per condition.

The constitutive model, developed by Olevsky and Froyen [7], includes the effects of the external load on creep and grain boundary diffusion, electromigration and sintering stresses. The axial strain rates observed for each densification phenomenon are shown in Eqs. (1)–(4)for the contributions of the external load on creep and grain boundary diffusion, electromigration and sintering stresses, respectively.

$$\dot{\varepsilon}_{crx} = \left[\left(\frac{3\theta}{2}\right)^{\frac{3}{2}}\left(\frac{3\alpha}{2G}(1-\theta)-\sigma_x\right)/A(1-\theta)^{5/2}\right]^{1/m} \tag{1}$$

$$\dot{\varepsilon}^{load}_{gbx} = \frac{\delta_{gb}D_{gb}}{kT}\frac{\Omega}{G+r_p}\frac{\sigma_x}{G^2} \tag{2}$$

$$\dot{\varepsilon}^{em}_{gbx} = \frac{\delta_{gb}D_{gb}}{kT}\frac{Z^*q_e}{(G+r_p)^2}\frac{U}{l} \tag{3}$$

$$\dot{\varepsilon}^{st}_{gbx} = -\frac{3\delta_{gb}D_{gb}}{kT}\frac{\Omega}{(G+r_p)^2}\frac{\alpha}{G}\left[\frac{1}{r_p}-\frac{1}{2G}\right] \tag{4}$$

where θ is the remaining porosity, $\delta_{gb}D_{gb}$ is the grain boundary diffusion coefficient at a given temperature, Ω is the atomic volume, σ_x is the applied pressure, k is the Boltzmann's constant, T is temperature in kelvin, G is the grain size, which is assumed to be one grain per particle during sintering (i.e. particle size is equal to the grain size), r_p is the pore radius, A is the power-law creep frequency factor, m is the power-law creep exponent, Z^*q_e is the effect charge, U/l is the applied field and α is the surface tension. Values for these parameters can be found in the literature [7]. The overall strain rate observed is the summation of these sintering phenomena shown in Eq. (5).

$$\dot{\varepsilon}_{\text{total}} = \dot{\varepsilon}_{crx} + \dot{\varepsilon}^{em}_{gbx} + \dot{\varepsilon}^{st}_{gbx} + \dot{\varepsilon}^{load}_{gbx} \tag{5}$$

The total strain rate can then be converted to overall densification rate by the following conversion, shown as Eq. (6):

$$\dot{\theta} = (1-\theta)\dot{\varepsilon}_{\text{total}} \tag{6}$$

The overall densification described in Eqs. (1)–(6)does not account for all of the possible effects of applied pressure during densification. Of particular importance to metallic materials is the densification contribution achieved by yielding (assumed to be instantaneous), described by Eq. (7)when the overall density of the compact is less than 90% of the theoretical density (TD) and by Eq. (8)when it is greater than 90% TD [6,11]:

$$\rho_{\text{Yield}} = \left(\frac{(1-\rho_0)\sigma_x}{1.3\sigma_y}+\rho_0^3\right) \quad \rho \leqslant 0.9 \tag{7}$$

$$\rho_{\text{Yield}} = 1-\exp\left(-\frac{3\sigma_x}{2\sigma_y}\right)\rho > 0.9 \tag{8}$$

where ρ_{Yield} is the density achieved due to plastic yielding and ρ_0 is the initial density. As the temperature increases during the ramp, the yield strength of the material will change dramatically. The effect of the temperature on the yield strength σ_y of commercial AA 5356 can be described by the following equation [12] above room temperature, where T is in kelvin:

$$\sigma_{\text{y}} = 20 + \frac{126}{1+10^{-0.0091(525-T)}} \tag{9}$$

Finally, a pressure gradient throughout the sample must be considered when using uniaxial pressing for tall samples, where the applied pressure gradient will change as a function of the total thickness. A rigorous analysis of die-pressing taking into account friction at the die walls, strictly speaking, requires a boundary-value problem formulation. This problem, due to the non-linearity of the constitutive equations, does not allow for an analytical solution and cannot be easily reduced to a set of ordinary differential equations describing the contribution of the applied axial stress to the shrinkage kinetics via plastic yield mass transport mechanism. Therefore, to simplify the problem, we employ an empirical relationship in Eq. (10). In single-action pressing, only one punch moves during pressing, leading to a decrease in effective pressure from the moving punch towards the static punch. The effective pressure σ_{eff} is a function of the thickness x, the diameter of the sample d, the coefficient of friction between the die wall and the powder μ, and the proportionality factor z [6]. In the current study, the friction coefficient was considered constant as a function of temperature, and a value of 0.16 was used for the system, representing Al–graphite [13]:

$$\sigma_{\text{eff}}(x) = \sigma_x \exp\left(-\frac{4\mu z x}{d}\right) \tag{10}$$

The total shrinkage of the compact using the constitutive models developed by Olevsky and Froyen, with the inclusion of the yielding and pressure gradient phenomena, was solved iteratively using MATLAB programming software to determine the remaining porosity as a function of sintered thickness.

Using Eq. (10)to calculate the reduction in effective applied pressure throughout the die, the change in porosity was calculated for samples of various thicknesses. The calculated residual porosity as a function of time for increasing component thicknesses for the 38 mm die is shown in Figure 1. As the thickness of the compact increases, the remaining porosity increases as a result of pressure decay. For this AA5356 alloy, when increasing the thickness of the compact from 5.3 to 28.9 mm, the predicted increase in remaining porosity of the samples rangeed from 5.5 to 6.2%, respectively, as plotted in Figure 2a and b for the 20 and 38 mm die, respectively.

The residual porosity was measured from grayscale thresholding of optical images and plotted as density