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# Propagation properties of the pulsed hollow Gaussian beam through a circular aperture



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#### ARTICLE INFO

### ABSTRACT

temporal shape changing.

Article history: Received 24 July 2014 Received in revised form 5 October 2014 Accepted 12 October 2014 Available online 22 October 2014 Keywords:

Reywords: Pulsed hollow Gaussian beam Diffraction effect Spatiotemporal characteristics

# 1. Introduction

Diffraction is one of the fundamental problems of the propagation of light. The diffraction theory of monochromatic light has been developed in great detail. Recent developments in optics resulted in the generation of ultrashort pulses with extremely broad spectra. Significant efforts have been devoted to investigate their propagation properties. However, most of the studies of pulsed beam propagation have considered only the fundamental Gaussian mode. Two different assumptions are typically made in these studies, i.e., diffraction length is assumed to be constant (constant diffraction length) [1–4], or the waist width is assumed to be constant (constant waist width) [5–8]. Because of the mathematical difficulty in dealing with the propagation of ultrashort pulsed beams with constant waist width, usually numerical results or approximate propagation expressions are found in the past studies. Beyond these, there are few studies focused on the diffraction of pulsed beam from the hard edges [9–11].

In 2003, a convenient theoretical model named hollow Gaussian beam (HGB) was introduced to describe dark-hollow beams [12]. After that, considerable attention has been focused on investigating hollow Gaussian beams [13–19]. Xu et al. [20] introduced a model of isodiffracting hollow Gaussian pulsed beams and discussed the influence of beam order on on-axis temporal profiles.

In this paper, we concentrate on the propagation of pulsed hollow Gaussian beam with constant waist width through a hard

http://dx.doi.org/10.1016/j.optcom.2014.10.026 0030-4018/© 2014 Elsevier B.V. All rights reserved. aperture. In Section 2, based on the angular spectrum representation and the method of stationary phase, an analytical propagation expression in the far-field is derived without any approximation. Numerical calculation results and comparative investigations are provided in Section 3. Finally, the results obtained in this paper are summarized in Section 4.

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#### 2. Analytical expression of pulsed HGB in the far-field

Based on the angular spectrum representation of the Maxwell equations and the method of stationary

phase, this paper presents the far-field analytical expression of a pulsed hollow Gaussian beam with

constant waist width diffracted by the circular aperture, and the result can be simplified for the case of

the paraxial propagation of pulsed Gaussian beam in the free space. Based on the analytical result, the

influences of truncation parameter on the transverse intensity distribution of the pulsed beam are

analyzed. Comparisons of normalized temporal intensity between the pulsed Gaussian beam and the

fourth order pulsed hollow Gaussian beam are presented. We find that the spatial mode can induce the

The monochromatic components of the pulse electromagnetic field in vacuum satisfy the Helmholtz equation

$$(\nabla^2 + k^2) E(\mathbf{r}, \omega) = 0, \tag{1}$$

where  $\nabla^2$  is the Laplace operator;  $\mathbf{k} = \omega/c$  is the wave number with c being the light speed in vacuum;  $\mathbf{r} = x\mathbf{i} + y\mathbf{j} + z\mathbf{k}$ ,  $\mathbf{i}$ ,  $\mathbf{j}$ , and  $\mathbf{k}$  are the unit vectors in the x-, y- and z-directions, respectively;  $E(\mathbf{r}, \omega)$  is the Fourier transform of optical field  $E(\mathbf{r}, t)$ . Thus,  $E(\mathbf{r}, t)$  can be obtained from  $E(\mathbf{r}, \omega)$ 

$$E(\mathbf{r}, t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} E(\mathbf{r}, \omega) \exp(i\omega t) d\omega.$$
(2)

From the angular spectrum theory,  $E(\mathbf{r}, \omega)$  can be expressed as

$$E(\mathbf{r}, \omega) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} A(k_x, k_y, \omega) \exp[-i(k_x x + k_y y + \sqrt{k^2 - k_x^2 - k_y^2} z)] dk_x dk_y,$$
(3)

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where  $A(k_x, k_y, \omega)$  is the angular spectrum. It can be obtained from the initial optical field  $E(\mathbf{r}_0, \omega)$ :

$$A(k_x, k_y, \omega) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} E(r_0, \omega) \exp(ik_x x_0 + ik_y y_0) dx_0 dy_0.$$
(4)

In the Cartesian coordinate system, a pulsed HGB propagates toward the half-space z > 0. The *z*-axis is adopted to be the propagation axis. A circular aperture with radius *R* is assumed to be located at the source plane z = 0. The pulsed HGB just behind the circular aperture is expressed as

$$E(\mathbf{r}_{0},\,\omega) = \left(\frac{\rho_{0}^{2}}{W_{0}^{2}}\right)^{n} \exp\left(-\frac{\rho_{0}^{2}}{W_{0}^{2}}\right) \operatorname{circ}\left(\frac{\rho_{0}}{R}\right) f(\omega),\tag{5}$$

where  $\rho_0 = (x_0^2 + y_0^2)^{1/2}$ , *n* is the beam order of HGB,  $W_0$  is the beam waist radius of the beam which is independent of frequency,  $f(\omega)$  is the spectrum of the initial pulse,  $circ(\cdot)$  denotes the aperture function and is given by

$$circ(\rho_0/R) = 1$$
 for  $0 < \rho_0 < R$ ;  $circ(\rho_0/R) = 0$  for  $\rho_0 > R$ . (6)

To obtain the analytical expression of the field, the aperture function can be expanded into the sum of complex Gaussian functions:

$$\operatorname{circ}\left(\frac{\rho_0}{R}\right) = \sum_{m=1}^{M} B_m \exp\left(-\frac{C_m \rho_0^2}{R^2}\right),\tag{7}$$

where the expansion coefficients  $B_m$  and  $C_m$  can be determined by optimization computation. Wen et al. [21] obtained a set of coefficients, containing only ten terms of coefficients, to match the original aperture function of Eq. (6). It shows that a good agreement between a ten-term Gaussian beam solution and the results of numerical integration throughout the beam field was achieved, and the discrepancies existed only in the extreme near field. In the following calculations, we will take M = 10. Let us consider the propagation of an electromagnetic wave with Gaussian temporal modulation at z = 0

$$f(t) = \exp\left(-\frac{t^2}{T^2} + i\omega_0 t\right),\tag{8}$$

SO

$$f(\omega) = \frac{T}{\sqrt{2}} \exp\left[-\frac{T^2(\omega - \omega_0)^2}{4}\right],\tag{9}$$

where  $\omega_0$  is carrier frequency, 2T is the width of pulse (full width at  $e^{-1}$  of the maximum intensity).  $T_0 = 2\pi/\omega_0$  is an optical cycle corresponding to  $\omega_0$ .

Inserting Eq. (5) into Eq. (4) and performing the integral, we can obtain

$$A(k_x, k_y, \omega) = \sum_{m}^{M} \frac{W_0^2 T n!}{2\sqrt{2}} \frac{B_m}{(1 + C_m/C_0)^{n+1}} \exp\left[-\frac{(k_x^2 + k_y^2)W_0^2}{4(1 + C_m/C_0)}\right] \\ \times L_n \left[\frac{(k_x^2 + k_y^2)W_0^2}{4(1 + C_m/C_0)}\right] \exp\left[-\frac{T^2(\omega - \omega_0)^2}{4}\right],$$
(10)

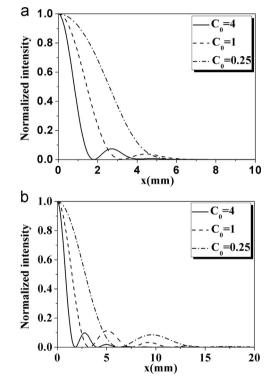
where  $C_0 = R^2/W_0^2$  is the truncation parameter,  $L_n(\cdot)$  denotes Laguerre polynomial with the order *n*. In the far field, the condition  $kr \to \infty$  is fulfilled. Inserting Eq. (10) into Eq. (3) and performing

the integral by the method of stationary phase, it can be obtained

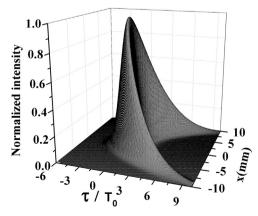
$$E(\mathbf{r},\omega) = \sum_{m}^{M} \frac{ikW_{0}^{2}Tzn!}{2\sqrt{2}r^{2}} \frac{B_{m}}{(1+C_{m}/C_{0})^{n+1}} e^{-ikr} \exp\left[-\frac{(x^{2}+y^{2})k^{2}W_{0}^{2}}{4r^{2}(1+C_{m}/C_{0})}\right] \times L_{n}\left[\frac{(x^{2}+y^{2})k^{2}W_{0}^{2}}{4r^{2}(1+C_{m}/C_{0})}\right] \exp\left[-\frac{T^{2}(\omega-\omega_{0})^{2}}{4}\right],$$
(11)

where  $r = (x^2 + y^2 + z^2)^{1/2}$ . In order to get the analytical expression of  $E(\mathbf{r}, t)$ , we expand the Laguerre polynomial as follows:

$$L_{n}\left[\frac{(x^{2} + y^{2})k^{2}W_{0}^{2}}{4r^{2}(1 + C_{m}/C_{0})}\right]$$
  
=  $\sum_{L=0}^{n} (-1)^{L}\left[\frac{(x^{2} + y^{2})k^{2}W_{0}^{2}}{4r^{2}(1 + C_{m}/C_{0})}\right]^{L}\frac{n!}{(L!)^{2}(n - L)!}.$  (12)



**Fig. 1.** Normalized transverse intensity distributions of pulsed HGB at z = 15 m. (a) n = 3,  $T = 2T_0$ ; (b) n = 3,  $T = 20T_0$ .



**Fig. 2.** Normalized space-time intensity distribution. The parameters are: z = 10 m,  $T = 2T_0$ , n = 3,  $C_0 = 0.25$ .

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