



Available online at www.sciencedirect.com





Solar Energy 122 (2015) 126-147

www.elsevier.com/locate/solener

Modeling of a concentrated-solar, falling-particle receiver for ceria reduction

Andrew S. Oles^a, Gregory S. Jackson^{b,*}

^a Department of Mechanical Engineering, University of Maryland, College Park, MD 20742 USA ^b Department of Mechanical Engineering, Colorado School of Mines, Golden, CO 80401 USA

Received 2 February 2015; received in revised form 10 August 2015; accepted 13 August 2015 Available online 12 September 2015

Communicated by: Associate Editor Michael Epstein

Abstract

This paper presents a steady-state model coupling three-dimensional, spectral radiation heat-transfer to a quasi-one-dimensional particle flow model for assessing performance of a directly-irradiated, falling-particle solar receiver with a closed cavity for thermochemical reduction of ceria. A semi-empirical gas-phase flow entrainment model captures the heat and mass exchange between the surrounding gas and the reducing ceria particles. With bulk and surface thermochemistry for the oxide-ion transport and surface reduction kinetics, model results indicate that for particle diameters under 500 µm, surface chemistry controls the rate of ceria reduction in the receiverreactor. For the range of particle inlet temperatures, flow rates, and diameters studied, the degree of ceria reduction correlates well with particle outlet temperature and increases to as high as 6% at maximum outlet temperatures of 1900 K. However, with the relatively low absorptivity of ceria, higher outlet temperatures lower the fraction of solar energy absorbed by the particles from approximately 30% at outlet temperatures of 1500 K to just above 10% at outlets of 1900 K. Most of the heat recovered in the ceria is due to sensible heating, and re-radiation losses can account for as much as 60–75% of the solar energy input due to the required high reduction temperatures and radiation properties of the ceria particles. The predicted low efficiencies show that ceria particle reduction must utilize significant heat recovery and alternative receiver optics other than simple direct radiation to improve the feasibility of solar-driven ceria redox cycles based on falling particle receivers.

© 2015 Elsevier Ltd. All rights reserved.

Keywords: Concentrated solar; Particle receiver; Ceria redox; Reactor modeling

1. Introduction

Concentrated solar power (CSP) plants with central tower receivers are attractive renewable energy systems capable of not only making renewable electricity, but also driving chemical processes, such as fuel production from H_2O and/or CO_2 , that require high-temperature (>1000 K) heat input. While many developed receiver

http://dx.doi.org/10.1016/j.solener.2015.08.009 0038-092X/© 2015 Elsevier Ltd. All rights reserved. designs have lower operating temperatures (<1000 K for commercial plants utilizing molten salt), solid-particle receivers have been proposed as an approach for efficiently achieving higher temperatures (Tan and Chen, 2010). These high receiver temperatures drive not only moreefficient power cycles but also endothermic chemical processes, such as for fuel production and/or integrated long-term storage. This paper explores the design of a central tower receiver that captures solar energy in falling cerium oxide (CeO_{2- δ}) particles through both sensible heating and high-temperature oxide reduction. Reduced

^{*} Corresponding author. Tel.: +1 303 273 3609. E-mail address: gsjackso@mines.edu (G.S. Jackson).

Nomenclature

| 11 | geometric area of a cell face | ε_{λ} | emittance or material emissivity | |
|--------------------------------|--|-------------------------|--|--|
| а | geometric area per particle, m ² | heta | surface site density | |
| C_D | single particle drag coefficient | $	heta_\lambda$ | angle of incident ray | |
| C_S | stream coefficient | λ | wavelength, µm | |
| d | diameter, m | μ | chemical potential, J kmol ⁻¹ | |
| D | species mass diffusivity, $m^2 s^{-1}$ | η | energy efficiency | |
| f_D | diffusion correction factor | ho | mass density, kg m^{-3} | |
| $f_{v,p}$ | particle volume fraction | $ar{ ho}$ | molar density, kmol m ^{-3} | |
| f_{λ_m} | fraction of radiant energy in <i>m</i> th λ -bin | $ ho_\lambda$ | bulk reflectance | |
| F_{i-j} | view factor of cell <i>j</i> for cell <i>i</i> | σ | Boltzmann's constant, $W m^{-2} K$ | |
| g | acceleration due to gravity, $m^2 s^{-1}$ | σ_k | sticking probability for species | |
| h | specific enthalpy, J kg ⁻¹ | $	au_\lambda$ | bulk transmittance | |
| h_T | heat transfer coefficient, $W m^{-2} K^{-1}$ | Г | site density per unit area, kmol | |
| $j_{\rm diff}''$ | diffusion flux, kmol $m^{-2} s^{-1}$ | | | |
| k | reaction rate-constant | Subscriț | pts | |
| k_T | conductivity, $W m^{-1} K^{-1}$ | b | bulk | |
| M | total number of radiation bins | С | curtain | |
| 'n" | reaction rate per unit area, kmol $m^{-2} s^{-1}$ | conv | convective heat transfer | |
| N_p | number density of particles, m^{-3} | eq | equilibrium | |
| Nu | Nusselt number | ext | external wall face or conditions | |
| Р | partial pressure, bar | g | gas | |
| Pr | Prandtl number | i, j | computational cell or face indic | |
| \dot{q}'' | surface heat flux, $W m^{-2}$ | int | internal wall face | |
| $\dot{q}^{\prime\prime\prime}$ | volumetric heat transfer, $W m^{-3}$ | k | species index | |
| \overline{R} | universal gas constant, J kmol ⁻¹ K ⁻¹ | т | radiation bin index | |
| Re | Reynolds number | р | particle | |
| t | time, s | R1, R2 | reaction 1, 2 | |
| t_w | receiver wall thickness, m | rad | radiation heat transfer | |
| Т | temperature, K | red | reduction reaction | |
| ū | mean directional velocity, $m s^{-1}$ | ref | reflected radiation | |
| v | volume per particle, m ³ | S | surface | |
| \overline{W} | molar mass, kg kmol ⁻¹ | sb | sub-surface | |
| X | species mole fraction | sol | solar irradiation | |
| x, y, z | Cartesian coordinates | W | receiver wall | |
| Y | species mass fraction | wind | receiver window | |
| | | λ | wavelength bin | |
| Greek s | symbols | | | |
| α | entrainment constant | Supersc | ripts | |
| β | excess parameter | ex | excess properties | |
| r - | | | | |

| $	heta_{\lambda}$ | angle of incident ray | | | |
|-------------------|---|--|--|--|
| λ | wavelength, μm | | | |
| μ | chemical potential, J kmol ⁻¹ | | | |
| η | energy efficiency | | | |
| ρ | mass density, kg m^{-3} | | | |
| $\bar{\rho}$ | molar density, kmol m^{-3} | | | |
| ρ_{λ} | bulk reflectance | | | |
| σ | Boltzmann's constant, W m ^{-2} K ^{-4} | | | |
| σ_k | sticking probability for species k | | | |
| $	au_{\lambda}$ | bulk transmittance | | | |
| Г | site density per unit area, kmol m^{-2} | | | |
| Subcovinto | | | | |
| h h | bulk | | | |
| C C | curtain | | | |
| conv | convective heat transfer | | | |
| ea | equilibrium | | | |
| ext | external wall face or conditions | | | |
| g | gas | | | |
| 8 i. i | computational cell or face indices | | | |
| int | internal wall face | | | |
| k | species index | | | |
| m | radiation bin index | | | |
| D | particle | | | |
| R1, R2 | reaction 1, 2 | | | |
| rad | radiation heat transfer | | | |
| red | reduction reaction | | | |
| ref | reflected radiation | | | |
| S | surface | | | |
| sb | sub-surface | | | |
| sol | solar irradiation | | | |
| W | receiver wall | | | |
| wind | receiver window | | | |
| λ | wavelength bin | | | |
| Superscripts | | | | |
| ex | excess properties | | | |
| 0 | ideal-state. reference-state | | | |

 $CeO_{2-\delta}$ particles can be reoxidized in a separate reactor by splitting CO₂ and/or H₂O as part of a solar fuel production plant as proposed in several studies (Abanades et al., 2010; Chueh and Haile, 2010; Lapp et al., 2012; Scheffe and Steinfeld, 2012).

Recent research and development on receivers using direct heating of solid particles have demonstrated the effectiveness of sub-mm-diameter particles to directly absorb incident solar radiation (Siegel et al., 2010; Tan and Chen, 2010). Particle receivers have many advantages for solar energy absorption and storage with operating temperatures well above the limits of molten salts and other storage media. Particle receiver designs can mitigate many thermal stress issues associated with fixed storage media if the particles are transported through a simple, open geometry (Kim et al., 2009; Siegel et al., 2010). Some proposed particle receiver configurations utilize absorption of solar heat in tubular reactors, which encapsulate the particle flow and allow for controlled environments (Maag et al., 2009; Martinek et al., 2012), but these arrangements do not provide the rapid heating of receiver designs with direct particle irradiation. Direct particle irradiation can

Download English Version:

https://daneshyari.com/en/article/1549569

Download Persian Version:

https://daneshyari.com/article/1549569

Daneshyari.com