

Experimental studies on the effect of using phase change material in salinity-gradient solar pond

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Abstract

Performance of adding phase change material (PCM) to small salinity-gradient solar pond was studied experimentally. Two ponds with an area of 3.4 m² and depth of 1 m were chosen. Horizontal cylindrical capsules containing Paraffin Wax as PCM were used in one of the pond's lower convective zone. The capsules were made of black iron whose thermal conductivity was about 80 W/m °C and its height and diameter were 0.5 m and 75 mm respectively. The study was covered within period of summer for 6 weeks. An internal heat exchanger was used in the lower convective zone of pond. The hourly as well as daily variation of temperatures of the storage zone, surface zone, ambient, inlet and outlet of the internal heat exchanger have been measured and analyzed for ponds. It was shown the assisted PCM pond decreases the temperature difference between night and day. In addition, the pond had more thermal stability over environmental condition and more thermal and salinity stability on heat extraction. Hence the maximum temperature of the pond, outlet water temperature of heat exchanger, and, accordingly, the thermal efficiency decreased by using PCM. However, the heat exchanger outlet water temperature and, accordingly, the thermal efficiency, can be constant by increasing the length of the heat exchanger pipe. Therefore, based on this study, in such applications which one needs lower temperature difference and more uniform temperature, or where applications need a specific temperature range or controlled maximum temperature, PCM with a suitable melting point might be beneficial.

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1. Introduction

High cost of solar system is due to low thermodynamic efficiency and cost of separated solar storage systems. Therefore, it is essential to design the solar thermal devices, which can collect and store solar energy simultaneously. Solar pond can be a typical example of such solar thermal

devices among various solar energy systems (Ranjan and Kaushik, 2014).

Kalecsinsky was a pioneer in the research on the solar pond (see Tundee et al., 2010). In the study, the solar-heated natural salt-water lake was considered. The lake showed temperatures as high as 70 °C at a depth of 1.32 m in the summer season. The minimal temperature was 26 °C during early spring. Following this study, the idea of solar energy collection was further developed using artificially created salinity-gradient solar ponds (SGSP) (Tundee et al., 2010), which were large bodies of water

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Nomenclature

A	heat transfer surface area of the heat exchanger (m^2)	PE	Polyethylene
A_i	internal surface area of the heat exchanger (m^2)	R_{FI}	resistance due to fouling on the heat transfer fluid (HTF) side ($^\circ\text{C}/\text{W}$)
A_o	external surface area of the heat exchanger (m^2)	R_{fi}	fouling factors at inner surfaces ($\text{m}^2\text{ }^\circ\text{C}/\text{W}$)
A_{sp}	area of the solar pond (m^2)	R_{FO}	resistance due to fouling on the solar pond side ($^\circ\text{C}/\text{W}$)
C	heat capacity rate per unit area of pond for heat transfer of fluid in the gradient-layer ($\text{W}/\text{m}^2\text{ }^\circ\text{C}$)	R_{fo}	fouling factors at outer surfaces ($\text{m}^2\text{ }^\circ\text{C}/\text{W}$)
C_p	Specific heat capacity of fluid ($\text{J}/\text{kg }^\circ\text{C}$)	R_p	heat transfer resistance from the brine in the solar pond to the wall tube ($^\circ\text{C}/\text{W}$)
d_i	external diameter of the pipe (m)	R_{tube}	thermal resistance of the wall tube ($^\circ\text{C}/\text{W}$)
d_o	internal diameter of the pipe (m)	R_{water}	heat transfer resistance from the wall tube to the HTF ($^\circ\text{C}/\text{W}$)
G	solar radiation at the surface of the pond (W/m^2)	r_i	external radius of the pipe (m)
h_o	external convective heat transfer coefficient ($\text{W}/\text{m}^2\text{ }^\circ\text{C}$)	r_o	internal radius of the pipe (m)
h_i	internal convective heat transfer coefficient ($\text{W}/\text{m}^2\text{ }^\circ\text{C}$)	$R_{overall}^*$	the independent of length overall resistance ($^\circ\text{C}/\text{W}$)
H	average global solar radiation incident on the surface of the pond (W/m^2)	$R_{overall}$	overall resistance ($^\circ\text{C}/\text{W}$)
k_t	thermal conductivity of the wall tube ($\text{W}/\text{m }^\circ\text{C}$)	T_a	ambient temperature ($^\circ\text{C}$)
L	total lengths of the heat exchanger pipe (m)	T_o	outlet temperature of the internal heat exchanger ($^\circ\text{C}$)
L_o	total outside lengths of the heat exchanger pipe (m)	T_i	inlet temperature of the internal heat exchanger ($^\circ\text{C}$)
L_i	total inside lengths of the heat exchanger pipe (m)		
L^{*l}	new total lengths of the heat exchanger pipe of hypothetical designed solar pond with PCM which has an equal efficiency to the similar pond without PCM (m)	Abbreviation	
\dot{m}	mass flow rate (kg/s)	HTF	heat transfer fluid
NaCl	sodium chloride	IHE	internal heat exchanger
\dot{Q}	rate of heat extraction from the LCZ per unit area of the solar pond (W/m^2)	JSUT	Jundi Shapour University of Technology
U	overall heat transfer coefficient based on external surface area ($\text{W}/\text{m}^2\text{ }^\circ\text{C}$)	LCZ	lower convective zone
Greek symbols		LHTES	latent heat thermal energy storage
Θ	non-dimensional temperature	LMTD	logarithmic mean temperature difference
η	thermal efficiency of the pond	NCZ	none-convective zone
η^{*l}	thermal efficiency of the hypothetical designed solar pond with PCM	PCM	phase change material
δ_{total}	total uncertainty	P_{LMLT}	pond with less maximum LCZ temperature
$\delta_{instrument}$	measuring instrument accuracy	P_{HMLT}	pond with higher maximum LCZ temperature
δ_{sensor}	sensor accuracy	SHTES	sensible heat thermal energy storage
		SGSP	salt gradient solar ponds
		TES	thermal energy storage
		UCZ	upper convective zone
		Subscripts	
		PLMLT	pond with less maximum LCZ temperature
		PHMLT	pond with higher maximum LCZ temperature
		pwp	pond with PCM
		pop	pond without PCM
		$*l$	new hypothetical parameter
		$*$	new predicted parameter

acting as solar collectors and heat storage (Dehghan et al., 2013). Researches on solar ponds have been conducted in a number of countries. In the last 50 years, solar ponds have been successfully built and operated in Europe, USA, Australia and developing countries, mostly on experimental

basis (Ranjan and Kaushik, 2014). A typical solar pond consists of three regions: the upper convective zone (UCZ), the non-convective zone (NCZ) and the lower convective zone (LCZ) as shown in Fig. 1. The UCZ is a relatively thin layer that consists almost of fresh water. The NCZ is below the

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