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Thermal analysis and performance optimization of a solar hot water plant with economic evaluation

Young-Deuk Kim^a, Kyaw Thu^a, Hitasha Kaur Bhatia^b, Charanjit Singh Bhatia^c, Kim Choon Ng^{b,*}

^a Water Desalination and Reuse Center, 4700 King Abdullah University of Science and Technology, Thuwal 23955-6900, Saudi Arabia
 ^b Department of Mechanical Engineering, National University of Singapore, 9 Engineering Drive 1, Singapore 117576, Singapore
 ^c Department of Electrical and Computer Engineering, National University of Singapore, 9 Engineering Drive 1, Singapore 117576, Singapore

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Abstract

The main objective of this study is to optimize the long-term performance of an existing active-indirect solar hot water plant (SHWP), which supplies hot water at 65 °C for use in a flight kitchen, using a micro genetic algorithm in conjunction with a relatively detailed model of each component in the plant and solar radiation model based on the measured data. The performance of SHWP at Changi International Airport Services (CIASs), Singapore, is studied for better payback period using the monthly average hourly diffuse and beam radiations and ambient temperature data. The data input for solar radiation model is obtained from the Singapore Meteorological Service (SMS), and these data have been compared with long-term average data of NASA (surface meteorology and solar energy or SSE). The comparison shows a good agreement between the predicted and measured hourly-averaged, horizontal global radiation.

The SHWP at CIAS, which comprises 1200 m² of evacuated-tube collectors, 50 m³ water storage tanks and a gas-fired auxiliary boiler, is first analyzed using a baseline configuration, i.e., (i) the local solar insolation input, (ii) a coolant flow rate through the headers of collector based on ASHRAE standards, (iii) a thermal load demand pattern amounting to 100 m³/day, and (iv) the augmentation of water temperature by auxiliary when the supply temperature from solar tank drops below the set point. A comparison between the baseline configuration and the measured performance of CIAS plant gives reasonably good validation of the simulation code. Optimization is further carried out for the following parameters, namely; (i) total collector area of the plant, (ii) storage volume, and (iii) three daily thermal demands. These studies are performed for both the CIAS plant and a slightly modified plant where the hot water supply to the load is adjusted constant at times when the water temperature from tank may exceed the set temperature. It is found that the latter configuration has better thermal and economic performances over the conventional design.

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Keywords: Solar hot water plant; Solar radiation analysis; Economic evaluation; Optimization

1. Introduction

Solar hot water (SHW) systems are recognized as the most cost-effective way for generating hot water for domestic, agricultural, commercial, and industrial applications. It is environmental friendly and economic viable investment

because it reduces the burning of fossil fuels and thus, reduces the emission of pollutants and greenhouse gases. A SHW system can be used in most climate conditions as they harness the solar energy to useful heating. However, system costs vary considerably depending on geographic location, water usage, and utility rates. To assure maximum cost benefit, therefore, the appropriate sizing of each component in the system and operating conditions are important parameters need to be accounted for.

^{*} Corresponding author. Tel.: +65 6516 2214; fax: +65 6516 1459. *E-mail address:* mpengkc@nus.edu.sg (K.C. Ng).

Nomenclature			
A	area (m²)	H_{d}	monthly average daily diffuse irradiation on a
$A_{\rm a}$	aperture area per collector (m ²)		horizontal plane (J/m ²)
$A_{\rm c}$	total collector area (m ²)	$H_{ m h}$	monthly average daily global irradiation on a
A_{ch}	channel cross-sectional area, $bL_{\rm w}$ (m ²)		horizontal plane (J/m ²)
$A_{\rm cs}$	cross sectional area of the tank (m ²)	i	interest rate (%)
$A_{ m eff}$	effective area of plate, $L_{\rm h}L_{\rm w}$ (m ²)	i'	effective interest rate (%)
$A_{ m HX}$	total heat transfer area of the plate heat exchan-	i''	effective interest rate for fuel (%)
11.1	ger (m ²)	I_{b}	monthly average hourly beam irradiation on a
$A_{\rm i}$	anisotropy index	Ö	horizontal plane (J/m ²)
A_1	lateral area of control volume (m ²)	$I_{ m d}$	monthly average hourly diffuse irradiation on a
b	mean flow channel gap, $p-t$ (m)	u	horizontal plane (J/m ²)
c_1	global heat loss coefficient (W/m ² °C)	$I_{ m h}$	monthly average hourly global irradiation on a
c_2	temperature dependence of global heat loss	11	horizontal plane (J/m ²)
2	coefficient $(W/m^2 {}^{\circ}C^2)$	I_{o}	monthly average hourly extraterrestrial irradia-
c_3	effective thermal capacity (kJ/m ² °C)	O	tion on a horizontal plane (J/m ²)
$c_{\rm p}$	mean specific heat capacity (kJ/kg °C)	$I_{ m T}$	monthly average hourly global irradiation on a
$C_{\mathbf{B}}$	boiler cost coefficient (S\$)	-1	tilted plane (J/m ²)
$C_{\rm c}$	fluid heat capacity rate in primary circuit (W/	j	inflation rate (%)
	°C)	$k_{ m w}$	thermal conductivity of water (W/m °C)
$C_{ m C}$	collector cost coefficient (S\$/m²)	$k_{\rm p}$	thermal conductivity of plate (W/m °C)
C_{D}	collector area dependent cost (S\$/m²)	K_{T}	monthly average daily clearness index
C_{F}	fuel cost coefficient (S\$/kW h)	$K_{0\mathrm{b}}$	beam radiation incidence angle modifier
$C_{\rm h}$	fluid heat capacity rate in secondary circuit (W/	$K_{ heta ext{d}}$	diffuse radiation incidence angle modifier
O _{II}	°C)	$L_{ m h}$	effective plate length (m)
C_{I}	collector area independent cost (S\$)	LMTD	
$C_{\rm IC}$	instrumentation and control cost coefficient (S\$/	$L_{ m w}$	effective plate width (m)
	m^2)	$\dot{m}_{ m ch}$	mass flow rate per channel, $\dot{m}_{\rm p}/N_{\rm ch}$ (kg/s)
$C_{ m HX}$	heat exchanger cost coefficient (S\$/m²)	$\dot{m}_{ m l}$	desired load mass flow rate (kg/s)
C_{max}	maximum heat capacity rate (W/°C)	$\dot{m}_{ m p}$	mass flow rate in primary circuit, A_cG (kg/s)
C_{\min}	minimum heat capacity rate (W/°C)	$\dot{m}_{ m r}$	makeup water mass flow rate (kg/s)
C_{PS}	pump and support structure cost coefficient (S\$/	$\dot{m}_{ m s}$	mass flow rate in secondary circuit, A_cG (kg/s)
-15	m^2)	$\dot{m}_{ m t}$	mass flow rate from storage to load (kg/s)
$C_{ m RF}$	capital recovery factor $(1/y)$	n	life cycle of plant (years)
$C_{\rm S}$	total cost of plant (S\$)	$N_{ m c}$	number of collectors
C_{T}	storage tank cost coefficient (S\$/m³)	$N_{ m ch}$	number of channels per pass, $(N_{\rm pl}-1)/(2N_{\rm pass})$
C^*	dimensionless heat capacity rate ratio	N_{pass}	total number of passes
D_{e}	channel equivalent diameter, $2b/\phi$ (m)	$N_{ m pl}$	total number of plates, $A_{\rm HX}/A_{\rm eff} + 2$
e	fuel inflation rate (%)	$N_{ m ht}$	number of heat transfer plates, $N_{\rm pl} - 2$
f	modulating factor	Nu	Nusselt number, hD_e/k_w
F	control function	p	plate pitch (m)
F(X)	objective function (years)	Pr	Prandtl number, $\mu C_p/k_w$
G	mass flow rate per unit area of collector (kg/	$q_{ m a}$	auxiliary energy required (W)
	m^2s)	$Q_{ m a}$	auxiliary energy required over a year (J)
G_{b}	monthly average hourly beam irradiance on a	\widetilde{Q}_1	desired hot water load over a year (J)
- 0	tilted plane (W/m ²)	$\widetilde{Q}_{ m r}$	solar energy incident on the collector over a year
$G_{ m ch}$	mass flux velocity, $\dot{m}_{\rm ch}/A_{\rm ch}$ (kg/m ² s)	21	(J)
$G_{\rm d}$	monthly average hourly diffuse irradiance on a	$q_{ m s}$	load met by solar energy (W)
- u	tilted plane (W/m^2)	$Q_{ m s}$	load met by solar energy over a year (J)
$G_{ m T}$	monthly average hourly global irradiance on a	$q_{ m u}$	solar useful heat gain rate (W)
	tilted plane (W/m ²)	$Q_{ m u}$	solar useful heat gain rate over a year (J)
h	heat transfer coefficient (W/m ² °C)	$R_{\rm b}$	ratio of beam radiation on a tilted plane to that
H/D	height to diameter ratio of storage tank	5	on the horizontal plane
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