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Investigation on the preparation and properties of monodispersed Al₂O₃–ZrO₂ nanopowder *via* Co-precipitation method



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1. Introduction

Due to the high reactivity, good homogeneity and sinterability. the synthesis of ceramic powders with narrow size distribution is currently of considerable interest. For example, compared to their conventional micron-crystalline counterpart, nano zirconia based ceramics has been attracted much attentions because of their good properties, superplastic behavior [1-4]. Therefore, there is a strong tendency for hard-aggregate formation during drying and calcination by liquid phase synthesis like chemical precipitation [5-8]and sol-gel processes [9]. Weakly agglomerated nanopowders can be obtained by hydrothermal synthesis. However, it is hard to control and reproduce [10,11]. Although gas phase methods are effective approaches to produce high quality agglomerate-free nanopowders, the disadvantages are involving in expensive equipment, complex operation process and requiring significant time and energy to produce relatively small amounts of material [12–15]. Co-precipitation is a process of simplicity, universality, low cost and easy to realize the industrialization if the hard-

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ABSTRACT

With Al₂O₃ as inhibitor (which can be etched after calcination), monodispersed Al₂O₃–ZrO₂ nanopowder was successful prepared by co-precipitation method. The as-prepared powders were characterized by acoustic particle sizer (APS), SEM, TEM and XRD, respectively. Crystalline and non-agglomerated nanometric Al₂O₃–ZrO₂ powders with very small crystallite size (~7 nm) and narrow size distribution can be obtained. The relative yield was effected dramatically by pH and the ratio of M_{AHC}: M_{Zr}. Green bodies have an ultrafine uniform microstructure without apparent macropore through 200 MPa CIP treatment. The relative density of the grains can be reached to ~98.2% by sintering at 1050 °C for 4 h, with an average grain size ~39 nm.

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aggregate can be avoided. Actually, hard-aggregate is consisting of many of single particles through sintering during calcination process. Typically, the addition of proper inhibitor is an effective way to suppress the process of calcination. Then, monodispersed powders can be obtained by etching the inhibitor. Till now, Al₂O₃ is often used as good inhibitor because it is inert, economic and can be easily removed.

In this study, co-precipitation technology by using Al₂O₃ as inhibitor is introduced for monodispersed Al₂O₃–ZrO₂ preparation. Zr⁴⁺ cations can be dissolved in carbonate solution forming a complex [Zr(CO₃)_x(OH)^{4-x}]^{x-} (x = 0–4, which depends on the pH) solution when addition of metal cation M (M = Ni²⁺, Y³⁺, Al³⁺, etc) was existed to form precipitate [16]. Due to a uniform mixing in atom level of Zr and Al and formation of a kind of amorphous Al₂O₃ covered ZrO₂ structure, monodispersed Al₂O₃–ZrO₂ can be obtained in theory. The synthetic schematic diagram was shown in Fig. 1.

2. Experimental section

2.1. Sample preparation

Raw materials used in this experiment include ZrOCl₂…8H₂O





Fig. 1. Schematic diagram of preparation of monodispersed Al₂O₃-ZrO₂.

(analytical-reagent grade), Al(NO₃)₃···9H₂O (Kermel Chemical Reagents Co., LTD, Tianjin) and NH₄HCO₃ (AHC). The pH was adjusted by ethanediamine (2 mol/L) and nitric acid (0.2 mol/L). Nominally, 97 mol% ZrOCl₂···8H₂O and (3.5–5.0) × 97 mol% AHC were dissolved, respectively, and 97 mol% Al(NO₃)₃···9H₂O were dissolved together in deionized water. Then addition of zirconium slowly to AHC solution with a magnetic stirrer till clear solution was obtained. The final concentration of zirconium in all processes was 0.1 mol/L. Precipitates emerged when Al³⁺ mixed solution was added to zirconium complex solution dropwise. The resultant suspension was filtered and washed for four times with deionized water and three times with ethanol. After drying at 80 °C overnight in air, the obtained precursors were calcined at 700–1200 °C for 2 h Fig. 2 presents a schematic flow diagram of the synthesis process.

Precursors used for yield calculation were synthesized at ~1250 °C for 2 h and the obtained powder compact bodies calcined at 700 °C for 10 h. The 1 and 15 mm thick samples in diameter were prepared by uniaxial pressing at 15 MPa, then calcined in air at a rate of 10 °C/min at various temperature for etching test. The concentration of NaOH corrosive liquid was 2 mol/L, and etch time and temperature were set as 2 h and 95 °C, respectively. The etched bulk samples were rinsed by deionized water and dried to constant weight for weighting. The etched powder samples were rinsed by deionized water till pH reach 7.0, and ethanol washed twice times and then dried at 80 °C. Putting the powders through a 60 mesh sieve, then uniaxial pressing at 4 MPa for molding and densifying



Fig. 2. A co-precipitation procedure for producing monodispersed $\mbox{Al}_2\mbox{O}_3\mbox{-}Zr\mbox{O}_2$ nanopowder.

by cold isostatic pressing (CIP) at 200 MPa, after that sintered in air at a rate of 5 °C/min for sintering samples preparation (High-Temperature Furnace P330, Nabertherm, Germany). There is no need to determine the accurate etching rate of Al_2O_3 in our present experiment. Hence, the mass changes of calcined samples in etching test were determined just by analytical balance.

2.2. Samples characterization

Phase identification and average crystalline size calculation were measured by using X-ray diffractometry (XRD, X'pert PRO, PANalytical, Holland). The density of the sintered samples was calculated by the Archimedes method. The theoretical densities of the $Al_{0.12}Zr_{0.88}O_{1.94}$ crystal structure (chemical formula $Al_{0.12}Zr_{0.88}O_{1.94}$ was obtained from XRF data, not provided here) were calculated according to Eq. (1):

$$\rho_{XRD} = \frac{4 \cdot \left[x \cdot M_Y + y \cdot M_{Al} + (1 - x - y) \cdot M_{Zr} + \left(2 - \frac{x + y}{2} \right) \cdot M_O \right]}{a^3 \cdot N_{Av}}$$
(1)

where M is atomic weight (g/mol), x and y are the dopant mole fraction, respectively. *a* is the unit cell lattice parameter (Å) and N_{Av} is Avogadro's constant. The thermal behaviors of the precursor powders were analyzed by differential scanning calorimetry (DSC)/ thermogravimetry (TG) in the temperature range between 40 and 1300 °C in air using a 10 °C/min ramp (DTA/TG, Netzsch 449 Thermal Analyzer, NETZSCH, Germany). Transmission electron microscopy (TEM, JEM-2010HR, JEOL, Japan) and scanning electron microscopy (FE-SEM field-emission type, XL30FEG, Philips, Holland) were used to observe the morphology and calculate size of obtained powders and bulk samples. Particle size distribution analysis of the powders was performed with acoustic particle size analyzer (APS-100, Matec Instruments Company, USA).

3. Results and discussion

3.1. Influence of pH and mole ratio on relative yield (RY)

The ratio of the ammonium bicarbonate to zirconium (M_{AHC} : M_{Zr}) is fixed at 4.5. The pH was adjusted slowly with nitric acid along with the addition of Al³⁺. The RY of ZrO₂–Al₂O₃ significantly depends on pH, as can be seen in Fig. 3a. The RY is increasing with pH changing from 6.5 to 7.0, then decreasing (pH 7.0–8.0). Clear solution turns to turbid when pH below 7.5 or above 8.7 without Al³⁺ addition due to generation of Zr(OH)₄. Meanwhile, flocculent precipitate emerged when Al³⁺ addition at pH excess 8.0 due to Al(OH)₃ formation, which was detrimental to complex of [Zr(CO₃)_x(OH)^{4-x}]^{x-} and Al³⁺ (leading to insufficient or excessive of Al³⁺). Fast dissolution was observed when Zr⁴⁺ was added to (NH₄)₂CO₃ and AHC mixed solution (M_{mix} : $M_{Zr} = 4.5$) at various ratio (5:1–1:5). However, less than 65% of RY was observed at all

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