#### Journal of Alloys and Compounds 658 (2016) 603-607

Contents lists available at ScienceDirect

# Journal of Alloys and Compounds

journal homepage: http://www.elsevier.com/locate/jalcom

## A new thermodynamic parameter to predict formation of solid solution or intermetallic phases in high entropy alloys

### O.N. Senkov<sup>\*</sup>, D.B. Miracle

Air Force Research Laboratory, Materials and Manufacturing Directiorate, Wright-Patterson AFB, OH 45433, USA

#### ARTICLE INFO

Article history: Received 29 September 2015 Received in revised form 28 October 2015 Accepted 29 October 2015 Available online 2 November 2015

Keywords: High entropy alloy Phase selection Equilibrium phases

#### ABSTRACT

A simple thermodynamic criterion is proposed to predict the presence or absence of equilibrium intermetallic phases in a high entropy alloy at a given temperature T. The criterion was verified using 45 currently available HEAs, for which equilibrium phases and respective annealing temperature are reported. The present model shows good correlation with experiment and gives an improved ability to predict formation of solid solution and intermetallic phases compared to earlier models.

© 2015 Elsevier B.V. All rights reserved.

#### 1. Introduction

Since the first reports of high entropy alloys (HEAs), a number of attempts have been made to predict phase formation in these alloys, in particular to predict compositions, which would favor formation of solid solution phases. The formation of disordered solid solution phases in HEAs was initially suggested to be governed by high entropy of mixing of alloying elements in these phases [1,2]:

$$\Delta S_{\rm mix} = -R \sum c_i \ln c_i \tag{1}$$

Here R is the gas constant and  $c_i$  is the atomic fraction of element *i*. Indeed, the high value of  $\Delta S_{mix}$  may reduce the Gibbs free energy,  $\Delta G_{mix}$ , of the solid solution (SS) below that of competing intermetallic (IM) phases. However, in spite of having high  $\Delta S_{mix}$  values, many HEAs are multi-phase and can also contain IM phases. For example, Otto et al. [3] studied the effects of entropy and enthalpy on phase formation in 5-component equimolar alloys. They started from a single-phase solid solution CoCrFeMnNi HEA [4] and made 5 other alloys by substituting Co, Cr, Fe or Ni, one element at a time, with, respectively, Ti, Mo or V, V and Cu. Although  $\Delta S_{mix}$  was the same, the modified alloys contained multiple SS and/or IM phases. Thermodynamic analysis showed that formation of multiple phases was consistent with minimization of the total Gibbs free energy,

\* Corresponding author. E-mail address: oleg.senkov.ctr@us.af.mil (O.N. Senkov). which includes both entropy and enthalpy contributions. It was concluded that  $\Delta S_{mix}$  stabilizes single-phase SS microstructures in rare cases. In many cases, the entropy effect is insufficient to counteract the driving forces that favor formation of secondary phases based on strongly interacting component pairs.

Several additional semi-empirical criteria for predicting solid solution phase formation in HEAs were introduced recently [5–9]. Similar to Hume-Rothery rules for binary substitutional solid solutions [10], these criteria focus on the differences of the atomic sizes ( $\delta r$ ), electronegativities ( $\delta \chi$ ), and valence electron concentrations (VEC) of the alloying elements. Additionally, the enthalpy of mixing ( $\Delta H_{mix}$ ) and a parameter  $\Omega$  were also used to develop criteria for the stability of SS, IM and/or amorphous phases in ascast HEAs [11].

Zhang et al. [5] were the first who identified the importance of  $\delta r$  and  $\Delta H_{mix}$  in the formation of SS, IM, SS + IM, or even amorphous phases, in as-cast HEAs. These parameters are calculated using the following equations:

$$\delta r = \sqrt{\sum c_i (1 - r_i/\bar{r})^2} \cdot 100\%$$
<sup>(2)</sup>

$$\Delta H_{mix} = \sum_{i < j} 4H_{ij}c_ic_j \tag{3}$$

Here  $r_i$  and  $c_i$  are atomic radius and atomic fraction of element i;  $\overline{r} = \sum c_i r_i$  is the average atomic radius; and  $H_{ij}$  is an enthalpy of mixing of elements i and j, which values are calculated by using







Miedema's model as given in Ref. [12].

Statistical analysis of existing experimental data for HEAs produced by casting revealed that SS phases can be present if  $\delta r < 6.2\%$  and -12 kJ/mol  $< \Delta H_{mix} < 5$  kj/mol, while IM phases can be present in HEAs for which  $\delta r > 3\%$  and  $\Delta H_{mix} < 0$  kJ/mol [5,13]. HEAs with  $\delta r > 6.2\%$  and -40 kJ/mol  $< \Delta H_{mix} < -12$  kJ/mol can contain amorphous phases. The  $\Delta H_{mix}$  range for IM HEAs overlaps with the  $\Delta H_{mix}$  ranges for SS and amorphous HEAs. Therefore, the  $\Delta H_{mix}$  parameter cannot be used for the separation of SS and IM HEAs, but it can be used to predict whether SS or amorphous phase would form. Such selectivity of  $\Delta H_{mix}$  can be easily understood because  $\Delta H_{mix}$  is a characteristic of disordered phases, to which SS and amorphous phases belong, while the enthalpy of formation  $\Delta H_{IM}$  should be used for IM phases, which is different from  $\Delta H_{mix}$ .

Trying to separate SS and IM phase fields, Yang and Zhang [6] proposed a parameter  $\Omega$ , which contains both  $\Delta S_{mix}$ , and  $\Delta H_{mix}$ , and is calculated as:

$$\Omega = T_m \Delta S_{mix} / |\Delta H_{mix}| \tag{4}$$

Here  $T_m = \sum c_i T_{mi}$  and  $T_{mi}$  is the melting point of element *i*. Only SS phases are found in as-cast HEAs for which  $\Omega \ge 1.1$  and  $\delta r < 3.6\%$ . SS and IM HEAs share the space of  $3.6\% \le \delta r < 6.6\%$  and  $1.1 \le \Omega \le 10$ , while at  $\Omega > 10$  only SS HEAs are identified. Most of the IM alloys have  $\delta r \ge 6.6\%$  and  $1 \le \Omega \le 2$ , and metallic glasses have  $\delta r \ge 5\%$  and  $\Omega \le 2$  [6].

These empirical criteria for phase selection were developed and tested using as-cast HEAs, which often contain non-equilibrium phases. Wang et al. [14] have recently evaluated these criteria to predict formation of equilibrium SS or IM phases in well homogenized and annealed HEAs. Using a limited number of data (27 alloys) available in the literature at that time, Wang et al. [14] found that the  $\Delta H_{mix}$  and  $\delta r$  ranges for HEAs with only SS phases after annealing narrowed significantly. Annealed HEAs with FCC and BCC solid solutions had  $\Delta H_{mix} > -7.5$  kJ/mol and  $\delta r < 3.3\%$ , while as-cast SS HEAs had  $\Delta H_{mix} > -12.5$  kJ/mol and  $\delta r < 6.2\%$ . Annealed HEAs with intermetallic compounds appeared at  $\Delta H_{mix} < -7.5$  kJ/mol and  $\delta r > 3.3\%$ . However, three Al-containing HEAs that were identified as BCC structures had  $\Delta H_{mix}$  between -17 and -10 kJ/ mol and  $\delta r$  between 5 and 6%, which are typical for IM HEAs. They suggested that the Al-containing HEAs probably have a B2 phase. However,  $\Delta H_{mix}$  and  $\delta r$  are characteristics of the alloy composition only and are not affected by alloy processing. Therefore, narrowing the  $\Delta H_{mix} - \delta r$  range for the SS HEAs after annealing may indicate that IM phases formed after annealing in other HEAs, which were solid solutions after casting, or this can just be due to much smaller number of the assessed alloys.

While the effect of  $\delta r$  on the formation of SS or IM phases can be understood from Hume-Rothery rules, the influence of  $\Delta H_{mix}$  and/ or  $\varOmega$  values on the phase selection is not so clear. The authors who derived these criteria [5,6,11,15] state that phase selection among different phases is determined by the *competition* between  $\Delta H_{mix}$ and T $\Delta S_{mix}$ . However this statement is thermodynamically incorrect, because these terms are not in competition, but rather work together to reduce the Gibbs free energy of the SS phase.

Troparevsky et al. [16] (2015) proposed a model that, through the use of high-throughput computation of the enthalpies of formation of binary compounds, seemed to predict single-phase SS equiatomic HEAs. The stability of the competing SS and IM phases was analyzed by comparing the contributions to the Gibbs free energy from only mixing entropy  $(-T\Delta S_{mix})$  for SS alloys and from only the enthalpy of formation  $(\Delta H_{ij}^{IM})$  for the ordered binary compounds. Thus they assumed that  $\Delta H_{mix} = 0$  and  $\Delta S_{IM} = 0$ , which is generally incorrect as  $\Delta H_{mix}$  can be very negative in some cases and  $\Delta S_{IM}$  can be comparable with  $\Delta S_{mix}$  in ordered structures in which the number of alloying elements is higher than the number of sublattices. Troparevsky et al. also assumed that an HEA will have a single SS phase at a temperature T if  $\Delta H_{ii}^{IM}$  values for any binary system present in the alloy are above  $-T\Delta S_{mix}^{9}$ . According to their model, among the currently developed non-refractory HEAs only those consisting of Co, Cr, Fe, Mn and/or Ni are truly singlephase solid solutions, while other alloys should form multiple phases during annealing at  $T_{cr} = 0.55 T_m$ . The conclusion may be correct for equiatomic alloys, however, many non-equiatomic HEAs containing other elements than listed above also retain their singlephase SS structure after annealing (see Table 1). Using their approach, Troparevsky et al. provided a list of new HEAs, which should be single-phase solid solutions, to guide experimental searches. In addition to the combinations of 5 elements listed above, these alloys can also contain such elements as Ir, Os, Rh, Pd, Ru, Pt, - all are very expensive.

#### 1.1. A simple thermodynamic criterion for SS or IM phase formation

In this paper we propose a new approach for the phase selection, which takes into account both enthalpy and entropy terms of the competing phases. The main assumption in this approach is that  $\Delta H_{mix}$  and  $\Delta H_{IM}$  are related. Both terms can be calculated by summing bond energies between first-neighbor atom pairs and thus some relationship between these terms should exist. The entropy of formation,  $\Delta S_{IM}$ , of binary and/or ternary compounds is close to zero. However, it can be high in multi-component compounds that have more constituents than sublattices and/or have a large solubility range, although  $\Delta S_{IM}$  should not be higher than  $\Delta S_{\text{mix}}.$  For example, using the sublattice model for configurational entropy [17], it can be shown that  $\Delta S_{IM}$  of  $(A,B)_1(C,D,E)_3$  compound is 0.997R, where R is the gas constant. This is more than 60% of  $\Delta S_{mix}$  of a 5-component equiatomic SS HEA. As the first approximation, we assume linear relationships between  $\Delta H_{IM}$  and  $\Delta H_{mix}$ , and between  $\Delta S_{IM}$  and  $\Delta S_{mix}$  for HEAs with negative values of  $\Delta H_{mix}$ :

$$\Delta H_{\rm IM} = \kappa_1 \cdot \Delta H_{\rm mix} \text{ and } \Delta S_{\rm IM} = \kappa_2 \cdot \Delta S_{\rm mix} \tag{5}$$

where  $\kappa_1 > 1$  and  $0 \le \kappa_2 < 1$ . The thermodynamic condition for the formation of a SS phase at a temperature T is:

$$\Delta H_{\rm mix} - T\Delta S_{\rm mix} < \Delta H_{\rm IM} - T\Delta S_{\rm IM} \tag{6}$$

Combining Eqs. (5) and (6) results:

$$\kappa_1 = \frac{\Delta H_{IM}}{\Delta H_{mix}} < -\frac{T\Delta S_{mix}}{\Delta H_{mix}} (1 - \kappa_2) + 1 \equiv \kappa_1^{cr}(T)$$
(7)

Equation (7) indicates that a SS phase with given  $\Delta S_{mix}$  and  $\Delta H_{mix}$  values ( $\Delta H_{mix} < 0$ ) is thermodynamically preferable at a temperature T, if the  $\Delta H_{IM}/\Delta H_{mix}$  ratio (i.e.  $\kappa_1$ ) for any competing IM phase is below the critical value  $\kappa_1^{cr}(T) = T\Delta S_{mix}/|\Delta H_{mix}|(1 - \kappa_2) + 1$ . It can be seen that  $\kappa_1^{cr}$  increases with a decrease in  $|\Delta H_{mix}|$  and an increase in the level of ordering of an intermetallic phase. Thus the condition for suppression of IM phases at a temperature T is:

$$\kappa_1^{Cr}(T) > \Delta H_{\rm IM} / \Delta H_{\rm mix} \tag{8}$$

Table 1 shows 45 HEAs, including 27 alloys analyzed by Wang et al. [14], for which information about phase contents in the annealed condition, as well as the annealing temperature, is available. We calculated  $\delta r$ ,  $\Delta H_{mix}$ ,  $\Delta H_{IM}$ ,  $\Omega(T_A)$ ,  $\kappa_1^{cr}(T_m)$  and  $\kappa_1^{cr}(T_A)$  parameters for these alloys ( $T_A$  is the absolute annealing temperature) and compared how well these parameters can predict phases at a given annealing temperature.  $\Delta H_{IM}$  values were calculated

Download English Version:

https://daneshyari.com/en/article/1607470

Download Persian Version:

https://daneshyari.com/article/1607470

Daneshyari.com