



# Low-temperature sintering and microwave dielectric properties of $\text{Al}_2\text{TeO}_6\text{--TeO}_2$ ceramics



Isao Kagomiya<sup>a,\*</sup>, Yuichiro Kodama<sup>a</sup>, Yukihiro Shimizu<sup>a</sup>, Ken-ichi Kakimoto<sup>a</sup>, Hitoshi Ohsato<sup>a</sup>, Yasuharu Miyauchi<sup>b</sup>

<sup>a</sup> Materials Science and Engineering, Nagoya Institute of Technology, Gokiso-cho, Showa-ku, Nagoya 466-8555, Japan

<sup>b</sup> Systems, Acoustics, Waves Business Group TDK-EPC Corporation, 2-15-7, Higashiowada, Ichikawa-shi, Chiba 272-8558, Japan

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## ABSTRACT

We propose  $\text{Al}_2\text{TeO}_6\text{--TeO}_2$  ceramics as a candidate for use as low-temperature co-fired ceramics (LTCC). We investigated microwave dielectric properties and low-temperature sintering conditions for  $\text{Al}_2\text{TeO}_6\text{--TeO}_2$  ceramics. The calcined  $\text{Al}_2\text{TeO}_6$  powders were sintered at 900 °C for 2–10 h with 30–50 wt% additive  $\text{TeO}_2$ . X-ray powder diffraction patterns showed that the sintered samples were  $\text{Al}_2\text{TeO}_6\text{--TeO}_2$  composite with no other phase. The apparent density was improved with the additive  $\text{TeO}_2$  content of up to 45 wt%. The dielectric constant ( $\epsilon_r$ ) increased by adding  $\text{TeO}_2$  content from 35 to 45 wt%, although the quality factor ( $Q \cdot f$ ) decreased. During sintering at 900 °C, the  $\epsilon_r$  of the  $\text{Al}_2\text{TeO}_6\text{--TeO}_2$  decreased slightly, whereas the  $Q \cdot f$  increased gradually. The observed microstructures showed that the longer sintering time makes fewer pores in  $\text{Al}_2\text{TeO}_6\text{--TeO}_2$  ceramics. Sintering at 900 °C for a long time contributes to densification, but it simultaneously causes  $\text{TeO}_2$  evaporation. To prevent  $\text{TeO}_2$  evaporation, we investigated the effects of annealing at 750 °C after sintering at 900 °C. Apparent densities or  $\epsilon_r$  for the annealed samples were higher than those of the non-annealed samples. The  $Q \cdot f$  improved with increasing annealing duration time, suggesting that sintering proceeded well during annealing with slower  $\text{TeO}_2$  evaporation at 750 °C. The results show that annealing at 750 °C is effective to facilitate sintering and to control  $\text{TeO}_2$  evaporation.

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## 1. Introduction

Recently, low-temperature co-fired ceramics (LTCC) have attracted attention for the development of next-generation miniaturized microwave/millimeterwave communication devices [1–10]. Using the LTCC, co-firing of dielectric ceramics with internal electrodes is possible, where silver is usually used for the electrode. Because the melting point of silver is approximately 961 °C in air [11], the sintering temperature for the dielectric ceramics must be lower than 961 °C. However, until now, almost all micro/millimeter-wave dielectric ceramics require sintering temperatures higher than 1000 °C to obtain a higher quality factor ( $Q \cdot f$ ), resulting from good densification and crystallinity [2,12–16]. Higher  $Q \cdot f$  is an important factor for higher-frequency telecommuting applications such as filters and resonators [2]. This study was conducted to develop new dielectric ceramics

with a high quality factor, even though the sintering temperature of the ceramics is lower than 961 °C of the silver melting point.

We have proposed that ceramics based on  $\text{Al}_2\text{TeO}_6$  are candidate compounds for the LTCC because they contain Te oxide, which is characterized by its low melting point. For example, the melting point of  $\text{TeO}_2$  is approximately 730 °C [17]. Some studies have been reported that the Te based binaries such as  $\text{TiO}_2\text{--TeO}_2$ ,  $\text{Bi}_2\text{O}_3\text{--TeO}_2$ , and  $\text{CuO--TeO}_2$  can be densified by sintering at temperatures lower than 900 °C [3–6,10]. Additionally, the Al based oxides tend to show lower dielectric constant [2,13,15,16]. Lower dielectric constant in addition to lower dielectric loss is also important for miniaturization of the higher-frequency telecommuting devices [2]. Su et al. have described that the  $\text{Al}_2\text{TeO}_6$  possesses both of low-dielectric constant ( $\epsilon_r$ ) and dielectric loss ( $\tan \delta$ ) in the frequency range of 1 kHz–1 MHz [18]. The  $\epsilon_r$  and the  $\tan \delta$  at 1 MHz have been reported as 9.4 and 0.03, respectively. That fact implies that the  $\text{Al}_2\text{TeO}_6$  is also characterized by low-dielectric constant and dielectric loss in the microwave frequency range. However, no reports in the relevant literature describe studies of microwave dielectric properties in the  $\text{Al}_2\text{TeO}_6$ .

\* Corresponding author. Tel./fax: +81 52 735 7368.

E-mail address: [kagomiya@nitech.ac.jp](mailto:kagomiya@nitech.ac.jp) (I. Kagomiya).

Given that perspective, we tried earlier to prepare  $\text{Al}_2\text{TeO}_6$  ceramic samples as a pilot study, but it was difficult to obtain dense ceramics, when the sample was sintered at temperatures below  $960^\circ\text{C}$ . Not sintered sample, but the pressed sample was used to investigate the dielectric properties in the frequency range of 1 kHz–1 MHz in the literature [18]. It also presumes that preparing the sintered  $\text{Al}_2\text{TeO}_6$  is difficult, because dielectric properties are usually investigated by using a sintered sample. Particularly, densification is more significant for the quality factor in the microwave frequency range. To overcome the difficulty, this study was undertaken to prepare dense  $\text{Al}_2\text{TeO}_6$  ceramics by adding  $\text{TeO}_2$  with the lower melting point. We investigated the low-sintering condition and crystallinity of  $\text{Al}_2\text{TeO}_6$ – $\text{TeO}_2$  ceramics. Then we investigated the microwave dielectric properties of the prepared samples and discussed relation between the sintering conditions and the microwave dielectric properties.

## 2. Experimental procedures

$\text{Al}_2\text{O}_3$  (purity: 99.99%) and  $\text{TeO}_2$  (purity: 99.9%) were weighed as the mole ratio of 1:1. They were ball-milled for 24 h in ethanol solvent using alumina balls with 5 mm  $\phi$  diameter. After drying, the mixed powders were calcined in air at  $550$ – $650^\circ\text{C}$  for 10 h. The calcined  $\text{Al}_2\text{O}_3$ – $\text{TeO}_2$  powders were mixed with additional  $\text{TeO}_2$  of 30–50 wt% and were again ball-milled for 24 h. The powders were molded into pellets with uniaxial pressure of approximately 7.8 MPa. Then cold isostatic pressing (CIP) of the molded samples was conducted under pressure of 200 MPa. The obtained pellets were sintered at  $900^\circ\text{C}$  for 2–10 h in air. Some pellets were annealed at  $750^\circ\text{C}$  for 24 h after sintering at  $900^\circ\text{C}$  for 2 h.

The crystalline phase of the prepared sample was characterized at room temperature using X-ray powder diffraction (XRPD; X'pert MPD Pro; PANalytical B.V.) with  $\text{Cu K}\alpha$  radiation, where the conditions of XRPD voltage and current were respectively 45 kV and 40 mA. The apparent densities of the prepared samples were measured using Archimedes' method. The microstructure images of the prepared samples were investigated using a scanning electron microscope (SEM; JSM-6330F; JEOL Inc.). Differential thermal analysis (DTA) and thermogravimetry (TG) were conducted at temperatures of  $20$ – $900^\circ\text{C}$  with a rate of  $10^\circ\text{C}/\text{min}$  to investigate the weight change and the melting point of  $\text{TeO}_2$  in the samples.

The microwave dielectric properties of the prepared samples were investigated using the Hakki and Coleman method [2,19], for which a pellet sample was positioned between two copper plates. The microwave signal from the sample was investigated using a network analyzer (8720ES; Agilent Technologies Inc.). The dielectric constant ( $\epsilon_r$ ) and the quality factor ( $Q \cdot f$ ) were calculated using the  $TE_{011}$  resonant mode investigated at room temperature [2,19]. The temperature coefficient of the resonator frequency ( $\tau_f$ ) was investigated at temperatures of  $20$ – $80^\circ\text{C}$ .

## 3. Results and discussion

### 3.1. Calcination condition to synthesize $\text{Al}_2\text{TeO}_6$

XRPD patterns of the  $\text{Al}_2\text{O}_3$ – $\text{TeO}_2$  powders calcined at  $550$ – $650^\circ\text{C}$  for 10 h are presented in Fig. 1. When the calcination temperature was  $550^\circ\text{C}$ , reflections corresponding to  $\text{Al}_2\text{O}_3$  and

tetragonal  $\text{TeO}_2$  were observed. At the calcination temperature of  $600^\circ\text{C}$ , reflections corresponding to  $\text{Al}_2\text{TeO}_6$  appeared in addition to the  $\text{Al}_2\text{O}_3$  and the  $\text{TeO}_2$  reflections. With higher calcination temperatures, the reflection intensities of the  $\text{TeO}_2$  and the  $\text{Al}_2\text{O}_3$  decreased, whereas the  $\text{Al}_2\text{TeO}_6$  reflection intensities increased. When the calcination temperature was  $620^\circ\text{C}$ , only  $\text{Al}_2\text{TeO}_6$  reflections were observed, indicating that single phase of  $\text{Al}_2\text{TeO}_6$  is obtainable at this calcination temperature. The reported TGA has showed an endothermal peak related to the formation of  $\text{Al}_2\text{TeO}_6$  at  $620^\circ\text{C}$  [18], which is good agreement with this XRPD result. We confirmed that a broad XRPD peak was observed around  $2\theta = 25^\circ$ , coming from the presence of  $\text{TeO}_2$  glass, when the  $\text{Al}_2\text{O}_3$ – $\text{TeO}_2$  powders were sintered at  $650^\circ\text{C}$ . Consequently, we concluded that  $620^\circ\text{C}$  is an appropriate condition for the calcination temperature for  $\text{Al}_2\text{TeO}_6$ .

### 3.2. Sintering condition to prepare dense $\text{Al}_2\text{TeO}_6$ – $\text{TeO}_2$ ceramic samples

XRPD patterns of the sintered  $\text{Al}_2\text{TeO}_6$ – $\text{TeO}_2$  samples are portrayed in Fig. 2, where the samples were prepared by sintering the calcined  $\text{Al}_2\text{TeO}_6$  powders with additive 30–50 wt%  $\text{TeO}_2$  at  $900^\circ\text{C}$  for 2 h. The calcined temperature was  $620^\circ\text{C}$ , as described above. The observed reflections of the sintered samples can be indexed by two phases:  $\text{Al}_2\text{TeO}_6$  and tetragonal  $\text{TeO}_2$ . With increasing additive  $\text{TeO}_2$  contents, the  $\text{TeO}_2$  reflection intensities increased slightly.

XRPD patterns of the  $\text{Al}_2\text{TeO}_6$  with additive 40 wt%  $\text{TeO}_2$  sintered at  $900^\circ\text{C}$  for 2–10 h are depicted in Fig. 3. Reflections corresponding to  $\text{Al}_2\text{TeO}_6$  and tetragonal  $\text{TeO}_2$  were observed. With longer sintering duration time, the reflection intensities of the  $\text{TeO}_2$  decreased gradually, suggesting that the  $\text{TeO}_2$  is evaporated during sintering at  $900^\circ\text{C}$ .

TG and DTA of the  $\text{Al}_2\text{TeO}_6$  with additive 40 wt%  $\text{TeO}_2$  are presented in Fig. 4. In the DTA, the endothermic peak was observed at  $707^\circ\text{C}$ , at which point the sample weight began to decrease. The results demonstrate that  $\text{TeO}_2$  contained in the sample begins to melt at  $707^\circ\text{C}$ .

The relations between apparent densities and the sample preparation conditions ((1) additive  $\text{TeO}_2$  amount and (2) sintering duration time) are presented in Fig. 5. It is difficult to estimate the relative densities in the  $\text{Al}_2\text{TeO}_6$ – $\text{TeO}_2$  composite series because  $\text{TeO}_2$  is evaporated during sintering. In the case of the additive 30 wt%  $\text{TeO}_2$ , the apparent density was the lowest among the samples in the case of additive  $\text{TeO}_2$  of 30–50 wt%, when the sintering duration time was 2 h. With increasing the additive  $\text{TeO}_2$  from 30 wt% to 45 wt%, the apparent density increased. The

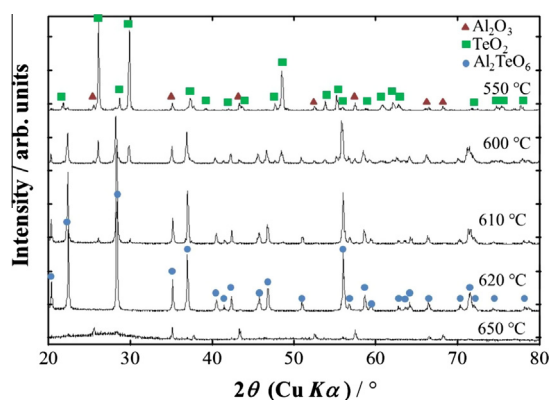


Fig. 1. XRPD patterns of the  $\text{Al}_2\text{O}_3$ – $\text{TeO}_2$  calcined for 10 h at  $550$ – $650^\circ\text{C}$ .

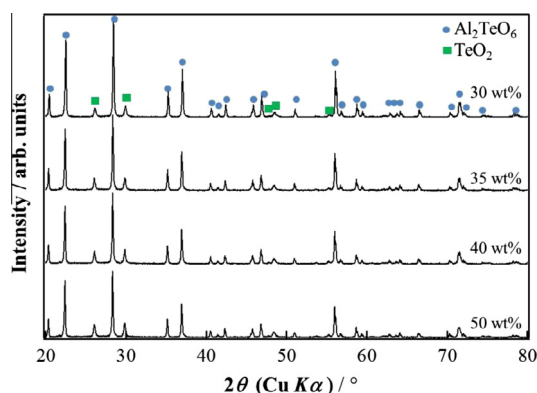


Fig. 2. XRPD patterns of the  $\text{Al}_2\text{TeO}_6$  sintered for 2 h with additive  $\text{TeO}_2$  of 30–50 wt% at  $900^\circ\text{C}$ .

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