Fabrication of ultrafine Nd-Fe-B powder by a modified reduction-diffusion process

JANG $T . S .^{1}$, LEE $D . H .^{1}$, YU $J . H .^{2}$, CHOI $C . J .^{2}$, SEO $W . S .^{3}$, and LEE $Y . H .^{3}$

1) Department of Electronic Materials Engineering, Sunmoon University, Korea

2) Powder Materials Research Center, Korea Institute of Machinery and Materials, Korea

3) Advanced Materials Analysis & Evaluation Center, Korea Institute of Ceramic Engineering and Technology, Korea (Received 2006-08-15)

Abstract: In order to obtain ultrafine Nd-Fe-B powder, a spray-dried precursor was treated by reductiondiffusion (R/D) process. And, unlike the conventional R/D process, calcium reduction that is a crucial step for the formation of Nd₂Fe₁₄B was performed without conglomerating the precursor with Ca powder. By adopting this modified process, it is possible to synthesize the hard magnetic Nd₂Fe₁₄B at the reaction temperature as low as 850 °C. The average size of Nd₂Fe₁₄B particles that are uniformly distributed in the optimally treated powder was << 1 μ m. Most Nd₂Fe₁₄B particles were enclosed with thin layers of Nd-rich phase. Typical magnetic properties of such powder without eliminating impurity CaO were $_iH_c =$ ~5.9 kOe, $B_r = \sim 5.5$ kG, and $(BH)_{max} = \sim 6$ MGOe.

Key words: NdFeB powder; spray drying; reduction-diffusion process; Nd₂Fe₁₄B; magnetic powder

1. Introduction

Currently, most Nd-Fe-B magnetic powders for bonded or sintered magnets are prepared by crushing Nd-Fe-B melt-spun flakes or ingots that are subsequently annealed or HDDR treated, which needs additional energy and increases production cost because of using highpurity metals as starting materials. On the other hand, it is possible to obtain the Nd-Fe-B powder inexpensively, without the pulverizing sequence, by employing reduction-diffusion (R/ D) process $\begin{bmatrix} 1-2 \end{bmatrix}$ in which cheaper raw materials are used. In the reduction-diffusion process, Nd-oxides are usually reduced by Ca in the presence of Fe or Fe-oxide and hard magnetic Nd₂Fe₁₄B is formed simultaneously by solid-state diffusion. It has been shown that the size of final Nd-Fe-B product of the R/D process depends on the size of starting materials 3-4]. We have also successfully prepared fine Nd-Fe-B powder (~ 1 μ m) by adopting the spray-drying as an initial stage of the R/D process [5-7]. However, it is still not easy to obtain the powder consisting of finely distributed Nd₂Fe₁₄B and possessing reasonable coercivity.

As an attempt to prepare such fine powder, the calcium reduction that is a crucial step for the formation of $Nd_2Fe_{14}B$ in the R/D process was tried without conglomerating a sprayed-dried precursor with Ca powder in this study. And effect of this process modification on phase formation, morphologies, microstructures, and properties of Nd-Fe-B powder was investigated.

2. Experimental

 $Nd(NO_3)_6 \cdot H_2O$, $Fe(NO_3)_3 \cdot 9H_2O$, and H_3BO_3 were dissolved into deionized water, adding neodymium hydrate 10% more for the compensation of Nd loss during reactions, to make spray-drying solutions for the target composition of $Nd_{15}Fe_{77}B_8$. Procedures of spray drying, debinding, milling, and hydrogen reduc-

tion in the R/D process were described in detail in Refs. [5-6]. The H₂-reduced precursor was well mixed with Ca powder (Ca : powder = 2:1), and then the mixed powder itself, not as a conventional compact, was reduced for 3 h at 850-1100 °C under Ar atmosphere. The reacted powder was subsequently washed in distilled water and dried in a vacuum. Characterization of the powder was performed by using Cu Ka Xray diffraction, scanning electron microscopy, transmission electron microscopy, and thermomagnetic analysis. Magnetic properties were measured with a VSM with a maximum applied field of 15 kOe.

3. Results and discussion

As shown in Fig. 1, the calcium-reduced powders were all composed of $Nd_2Fe_{14}B$ and CaO regardless of the reduction temperature. It tells us that hard magnetic $Nd_2Fe_{14}B$ can be readily formed through a solid-state reaction even though the Ca reduction is carried out in a mixed powder state, i.e., as the hydrogen-reduced precursor is not consolidated, but just mixed with Ca powder. It is also found that this reduction method has an advantage of lowering the reduction temperature as the $Nd_2Fe_{14}B$ was fully obtained even at 850 °C.

All calcium-reduced powders, as typically shown in Fig. 2(a), were spherical clusters with the particle size 1 μ m more or less al-



Fig.1. XRD patterns of Nd-Fe-B powder calcium reduced in the powder state for 3 h at 850, 900, 1000, and 1100 °C. (Ca:powder = 2:1).

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though the particles tended to grow as the reduction temperature increased. In fact, they were much smaller than those obtained by conventional Ca reduction[6]. When the powder in Fig. 2(a) was washed in water and dried in vacuum, most spherical particles in the powder became much smaller than 1 μ m as shown in Fig. 2(b). Moreover, long rod-type particles that were not found in the calcium-reduced state were often found after washing in water. It indicated that a certain change in shape or phase of the particles occurred during washing [7-8]. In fact, the thermo-magnetic analysis revealed that Nd₂Fe₁₄B was partially decomposed to soft magnetic Nd₂Fe₁₇B, due to the thermal energy generated by severe exothermic reaction occurred in washing[8]. EDX results revealed that both the spherical and the rod-type particles were Nd₂Fe₁₄ B. Such rod-type particles were also found in the Nd-rich Nd-Fe-B alloy 9].

As shown in Fig. 3, $Nd_2Fe_{14}B$ particles in the above mentioned powders were enclosed



Fig.2. SEM images of Nd-Fe-B powder calcium reduced in the powder state for 3 h at 1000 \mathcal{C} (a) and subsequently washed in distilled water (b).

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