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# Numerical analysis of oscillatory Couette flow of a rarefied gas on the basis of the linearized Boltzmann equation

ABSTRACT

discussed.

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#### A R T I C L E I N F O

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#### 1. Introduction

The flow of a rarefied gas has been investigated extensively for more than five decades, and the behavior of various fundamental flows has been clarified [1]. The results of these studies are successfully applied to vacuum and micro engineering and have made an important contribution to modern technologies. The oscillatory Couette flow, i.e., the flow of a gas between two parallel plates caused by the reciprocating motion of the plates, which is one of the most fundamental time-dependent flows, plays an important role in macro sensors, and thus has drawn the attention of numerous engineers and scientists [2–5]. Extensive computations based on the DSMC method have been conducted in Refs. [3,4], and the physical discussion is given in Ref. [3].

In the present study, we perform a direct numerical analysis of the oscillatory Couette flow based on the linearized Boltzmann equation for a hard sphere molecular gas. The goals of the present paper are to present a standard solution of this linear problem and to present more detailed data than that provided by the DSMC result, which would be useful in practical applications in engineering. Quite recently, Sharipov and Kalempa [5] conducted a similar study based on the linearized BGKW model of the

Boltzmann equation. The result of the present study and that of

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2. Problem and basic equation

Ref. [5] are compared.

The unsteady motion of a rarefied gas between two parallel plates, one of which is oscillating in its plane,

is studied based on the linearized Boltzmann equation for a hard sphere molecular gas. The detailed

numerical solution for a wide range of gas rarefaction and oscillatory frequency is presented. The

transition of the solution from low to high frequencies under various degrees of gas rarefaction is

Consider a rarefied gas between two parallel plates placed at  $X_1 = 0$  and  $X_1 = L$  having a common temperature  $T_0$ , where  $X_i$  is the space rectangular coordinates. The plate at  $X_1 = 0$  undergoes an inplane reciprocating motion with the velocity (0,  $V_w \cos \omega t$ , 0) (t: time). We investigate the time-dependent periodic behavior of the gas based on kinetic theory. We perform the analysis under the following assumptions: (i) the gas behavior is governed by the Boltzmann equation for a hard sphere molecular gas, (ii) the gas molecules make diffuse reflection on the boundaries, and (iii) the speed of the plate is much smaller than the sonic speed, and the

equation and the boundary condition may be linearized. The basic equation is the linearized Boltzmann equation

$$\frac{1}{k}\frac{\partial\phi}{\partial\hat{t}} + \zeta_1\frac{\partial\phi}{\partial\mathbf{x}_1} = \frac{1}{k}\mathscr{L}(\phi),\tag{1}$$

where  $\hat{t} = t/\bar{v}_c^{-1}$ ,  $x_i = X_i/L$ , and  $\zeta_i$  are the nondimensional time, space coordinates, and the molecular velocity, respectively,  $\rho_0(2RT_0)^{-3/2}E(1+\phi)$  is the velocity distribution function,  $E = \pi^{-3/2} \exp(-\zeta_i^2)$ , R is the specific gas constant,  $\rho_0$  is the mean density of the gas,  $k = (\sqrt{\pi}/2)$  Kn (where Kn =  $\ell/L$  is the Knudsen number),  $\bar{\nu}_c$ 



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and  $\ell [= (8RT_0/\pi)^{1/2} \overline{\nu}_c^{-1}]$  are the mean collision frequency and the mean free path of the gas in the equilibrium state at rest, respectively, with density  $\rho_0$  and temperature  $T_0$ . Finally,  $\mathscr{L}(\varphi)$  is the linearized collision integral (see Ref. [1]).

The boundary condition is the diffuse reflection condition

$$\phi = 2\zeta_2 u_w \cos \Omega \hat{t} - 2\sqrt{\pi} \int_{\zeta_1 < 0} \zeta_1 \phi E d\zeta_1 d\zeta_2 d\zeta_3 \ (x_1 = 0, \zeta_1 > 0), \quad (2)$$

$$\phi = 2\sqrt{\pi} \int_{\zeta_1 > 0} \zeta_1 \phi E d\zeta_1 d\zeta_2 d\zeta_3 \quad (x_1 = 1, \zeta_1 < 0), \tag{3}$$

where  $u_w = V_w/(2RT_0)^{1/2}$  and  $\Omega = \omega/\overline{\nu}_c$  is the nondimensional frequency of the oscillation.

In this problem, we can seek a solution in the following form:  $\phi(x_1, \zeta_i, \hat{t}) = (\zeta_2/\zeta_\rho)\Phi(x_1, \zeta_1, \zeta_\rho, \hat{t})$ , where  $\zeta_\rho = (\zeta_2^2 + \zeta_3^2)^{1/2}$ . Furthermore, since we are interested in the periodic behavior in time, we set  $\Phi$  as  $\Phi(x_1, \zeta_1, \zeta_\rho, \hat{t}) = \text{Re}[\exp(-i\Omega \hat{t})\Psi(x_1, \zeta_1, \zeta_\rho)]$ , where  $i = \sqrt{-1}$  and Re[\*] denotes the real part of \*. Substituting these expressions into Eqs. (1)–(3), we obtain the boundary value problem of the spatially one-dimensional Boltzmann equation, which is characterized by two parameters, namely, k and  $\Omega$ .

#### 3. Numerical analysis

The boundary value problem stated above is solved numerically using a finite difference method. The collision integral is evaluated with the aid of the numerical kernel method devised in Ref. [6]. The solution method is well established, and there is only one difficulty to be considered. In the present problem, the distribution function  $\Psi$  tends to vary rapidly in  $\zeta_1$  as  $\Omega/k$  increases, and thus the numerical analysis becomes difficult for a large  $\Omega/k$ . To avoid this difficulty, we deal with  $\Psi - \Psi_{\#}$ , instead of directly dealing with  $\Psi$ , where  $\Psi_{\#}$  is a known function that is similar to the solution of the collisionless Boltzmann equation. Since the remainder  $\Psi-\Psi_{\#}$  is considerably smooth, we can perform an accurate numerical analysis for considerably large values of  $\Omega/k$ . A similar technique is used in Ref. [5].

#### 4. Large Knudsen number and frequency

Before presenting the numerical results, we present a brief summary of the solution for large k and  $\Omega$  following Refs. [3–5].

If we ignore the collision term of the Boltzmann equation (1), the solution is easily obtained, e.g., the shear stress P and the heat flow Q are given by,

$$P = 2\pi^{-1/2} J_1(-i\Omega x_1/k), \quad Q = \pi^{-1/2} [J_2(-i\Omega x_1/k) - J_0(-i\Omega x_1/k)/2], \tag{8}$$

The macroscopic quantities of the gas, i.e., the flow velocity  $v_i$ , the stress tensor  $p_{ij}$ , and the heat flow  $q_i$ , are given as follows:

$$v_2/(2RT_0)^{1/2}u_w = \operatorname{Re}\left[\exp\left(-i\Omega \hat{t}\right)U(x_1)\right], \quad v_1 = v_3 = 0, \quad (4)$$

$$p_{21}/p_0 u_w = \operatorname{Re}\left[\exp\left(-i\Omega \hat{t}\right)P(x_1)\right], \quad p_{32} = p_{13} = 0,$$
 (5)

$$p_{11} = p_{22} = p_{33} = p_0, \tag{6}$$

$$q_2/p_0(2RT_0)^{1/2}u_w = \operatorname{Re}\left[\exp\left(-i\Omega\hat{t}\right)Q(x_1)\right], \ q_1 = q_3 = 0,$$
 (7)

where U, P, and Q are complex valued functions of  $x_1$  and are given by the moments of  $\Psi$ , and  $p_0 = R\rho_0 T_0$ . The other macroscopic quantities, i.e., the density  $\rho$ , the temperature *T*, and the pressure *p*, are found to be constant, i.e.,  $\rho = \rho_0$ ,  $T = T_0$ , and  $p = p_0$ .

where  $J_n$  is defined by  $J_n(z) = \int_0^\infty \zeta_1^n \exp(-\zeta_1^2 - z/\zeta_1) d\zeta_1$ . From the latter equation, we find  $Q(0) = Q(\infty) = 0$  and |Q| has a simple peak at  $x_1 = 1.12k/\Omega$ . There are three typical cases in which the solution is given by Eq. (8). (i) When  $k \to \infty$ , keeping  $\Omega$  finite (or  $\Omega/k \to 0$ ), the solution reduces to the time-independent free molecular solution. Then,  $P = \text{const} = 2\pi^{-1/2}J_1(0) = \pi^{-1/2}$ . (ii) When  $\Omega \to \infty$ , keeping  $\Omega/k$  finite, the solution is given by Eq. (8) with finite  $\Omega/k$ . Note that this solution has a characteristic length of  $Lk/\Omega \sim (2RT_0)^{1/2}/\omega$ , which is different from the characteristic length  $(\nu/\omega)^{1/2}$  of the Stokes layer, where  $\nu$  is the kinematic viscosity of the gas. (iii) When  $\Omega \to \infty$ , keeping k finite (or  $\Omega/k \to \infty$ ), the thickness of the layer expressed by Eq. (8) shrinks indefinitely.

#### 5. Results and discussion

First, we show the profile of the macroscopic variables of the gas. As shown in Eqs. (4)–(7), the flow velocity  $v_2$ , the shear stress  $p_{21}$ , and the heat flow  $q_2$  are expressed using the complex valued



**Fig. 1.** The profile of the macroscopic variables I: k = 0.1. (a) Flow velocity  $v_2$ , (b) shear stress  $p_{21}$ , and (c) heat flow  $q_2$ , where  $U = |U| \exp(i\varphi_U)$ ,  $P = |P| \exp(i\varphi_P)$ ,  $Q = |Q| \exp(i\varphi_Q)$  [see Eqs. (4)–(7)]. —: amplitude, - - -: phase, - - - -. time-independent Couette flow [7].

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