

Available online at www.sciencedirect.com





Procedia CIRP 31 (2015) 299 - 303

15th CIRP Conference on Modelling of Machining Operations

A new procedure to increase the orthogonal cutting machining time simulated

M. Guediche^{1, 2*}, T. Mabrouki^{2, 3}, C. Donnet⁴, J.M. Bergheau¹, H. Hamdi¹

1University of Lyon, CNRS, ENI-Saint-Etienne, LTDS UMR 5513, F-42023-France 2University of Lyon, CNRS, INSA-Lyon, LaMCoS UMR 5259, France 3University of El Manar, ENIT, BP 37, Le Belvedere, 1002, Tunisia 4University of Lyon, CNRS, Université Jean Monnet, LHC UMR 5516, France

* Corresponding author. Tel :+ 33612866588 ; E-mail address: mayssa.guediche@enise.fr

Abstract

Surface integrity is extremely affected by manufacturing processes conditions especially the evolution of cutting tool performance. Many researchers, in steel machining field, focused their works on the elaboration of models predicting tool wear combining both numerical and experimental approaches.

Most of published numerical cutting models simulate the chip formation for a few micro to millisecond time periods. For that, all corresponding experimental tests, needed for the model validation, are usually carried-out in special time conditions which is not reflecting industrial situations. Indeed, the latters are characterized by tool wear whose evolution can affect extremely cutting force levels and the final workpiece integrity.

In this context, the main purpose of the proposed research work is to develop a FEM model, based on the commercial code ABAQUS©, to simulate wear phenomenon of tool insert in the case of orthogonal cutting operation. The present research exposes a lagrangian approach simulating the chip formation in the case of AISI 4140 machining. A strategy that aims to reach high machining time simulated with moderate computational time is presented. It is based on ensuring the thermal continuity of the tool from one calculation to another. A considerable gain of calculation time is achieved comparing to the most common models developed on ABAQUS©.

© 2015 The Authors. Published by Elsevier B.V. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).

Peer-review under responsibility of the International Scientific Committee of the "15th Conference on Modelling of Machining Operations

Keywords: Wear, Simulation, Tool

1. Introduction

Studying tool wear is crucial for designing more performant tools, decreasing machining costs and improving manufactured products quality. For that, many researchers focused on elaborating models predicting tool wear in orthogonal cutting [1,2].

Most of published studies concerning tool wear prediction are based on experimental tests or empirical equations to estimate tool life as a function of cutting conditions. In this case, tool life is provided as a function of several cutting parameters [3,4,5]. More recently, researchers focused on elaborating numerical models to simulate tool wear in machining operations. These approaches resort generally to the Finite Element Method (FEM).

They are based essentially on implementing subroutines to estimate tool wear caused by a specific tool wear mechanism such as abrasion, diffusion and so on, by supposing that one of them is preponderant [6,7].

However, FEM-based softwares are limited in terms of simulated times. In fact, an orthogonal cutting simulation lasts, in most cases few milliseconds, which is not sufficient to reach steady state conditions. In addition, these short times simulated generate high computational times [8].

2212-8271 © 2015 The Authors. Published by Elsevier B.V. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).

Peer-review under responsibility of the International Scientific Committee of the "15th Conference on Modelling of Machining Operations doi:10.1016/j.procir.2015.04.096

Nevertheless, tool wear study requires the simulation of several minutes of machining which involves the use of sophisticated machines such as supercomputers with high processor performance. So, to reach high simulated times in machining operations without resorting to powerful machines with higher costs, researchers developed several methods on different software. Yen et al [9] used the "Konti-cut" module available on DEFORM 2D[©] which consists on eliminating chip and machined workpiece after a certain period of time. Although this method allows simulating six minutes of machining, it has the inconvenient that mechanical and thermal histories of the workpiece are lost.

Salvatore et al [10] proposed also a solution to increase the simulated time on ABAQUS©. It is based on partitioning the chip since it can be considered uninteresting for his study that focuses on tool wear estimation. The simulation is made on a workpiece length more important to reach high process simulated time. However, the model adopted has the inconvenient of not respecting the assumption made on the geometrical model. This assumption consists in considering that the surface to be machined is flat, which remains valid only for small lengths.

That's why, a new approach is presented in this paper to increase machining time simulated in orthogonal cutting. First of all, a Finite Element (FE) multi-part model will be presented based on the commercial code ABAQUS© following a lagrangian approach. It simulates chip formation in the case of AISI 4140 machining with a carbide tool.

Then, a strategy that aims to reach high machining time simulated with moderate computational time is presented. It is based on ensuring the thermal continuity of the tool from one calculation to another. Results will be compared with experimental data found in literature.

2. Numerical approach

2.1. Geometrical model

In order to optimize contact management during simulation, a multi-part model, inspired from MABROUKI proposal [11] is presented. It is composed from four parts (fig.1). PART (1) is the tool made by a tungsten carbide WC ISO-P20 insert. PART (2) is the region of the workpiece that may be removed as chip. The tool-tip passage zone, PART (3), is made of a damageable narrow band. It represents the area where the separation of the material occurs. And finally, PART (4) is the rest of the workpiece.

The mesh is made of CPE4RT elements to achieve temperature-displacement coupled simulations [12].



Fig. 1. Mesh and boundary conditions of the cutting model

2.2. Material behavior

To simulate chip formation, the Johnson-Cook [13] material constitutive law is adopted. Von Mises stress is given by the equation 1.

$$\bar{\sigma} = (A + B\bar{\varepsilon}^n) \left[1 + Cln\left(\frac{\hat{\varepsilon}}{\bar{\varepsilon}_0}\right) \right] \left[1 - \left(\frac{T - T_0}{T_f - T_0}\right)^m \right] \tag{1}$$

For AISI 4140 steel, Johnson-Cook parameters are mentioned in the table 1 [14].

Table 1. Johnson-Cook parameters for AISI 4140

A (MPa)	B (MPa)	n	С	m
1098	1092	0.93	0.014	1.1

2.3. Decreasing computational time

To simulate tool wear, high simulation times (few minutes) need to be reached, which consumes high computational times. In fact, in machining simulations, computational time is divided mainly between calculating strains inside the material and managing contacts between surfaces. It depends also on the formulation adopted. The lagrangian approach adopted in this study is the one consuming the less computational time.

Inspired by previous works [9,10,11], a new approach called "vertical modelling" is proposed in this paper; to increase machining time simulated (Fig.2).

Download English Version:

https://daneshyari.com/en/article/1699652

Download Persian Version:

https://daneshyari.com/article/1699652

Daneshyari.com